

CHARACTERIZATION OF GROUND WATER FLOW IN THE LOWER BOISE RIVER BASIN

Prepared by

Christian R. Petrich

Idaho Water Resources Research Institute
University of Idaho

Scott M. Urban

Idaho Department of Water Resources

Prepared for and in cooperation with the

Idaho Department of Water Resources

1301 North Orchard
Boise, Idaho 83706-2237



FEBRUARY 2004

**IDAHO WATER RESOURCES RESEARCH INSTITUTE
RESEARCH REPORT**

IWRRI-2004-01



ACKNOWLEDGEMENTS

The work described in this report was conducted as part of the Treasure Valley Hydrologic Project (TVHP). Participants in the TVHP include the Idaho Department of Water Resources (IDWR), the Idaho Water Resources Research Institute (IWRRI), University of Idaho (UI), United Water Idaho, Inc. (UWID), Boise State University (BSU), U.S. Geological Survey (USGS), U.S. Bureau of Reclamation (USBR), Idaho Water Resources Board (IWRB), Ada and Canyon Counties, and the cities of Boise, Nampa, Caldwell, Meridian, Kuna, and Eagle. The project was funded by the U.S. Environmental Protection Agency, the Idaho State Legislature, UWID, and the IWRB. In addition, substantial in-kind services were provided by UWID, the USGS, and the USBR.

The authors wish to acknowledge the following contributions to this report:

- Helen Harrington and Shane Bendixsen (IDWR) prepared hydrographs of water level data from Treasure Valley wells.
- Linda Davis and Genna Ashley-Poulson provided GIS support and assistance.
- Diana Hegland provided proofreading and editing assistance.
- The citizens of the Treasure Valley, who helped pay for this effort.

This report was reviewed by:

- Hal Anderson (IDWR)
- Paul Castelin (IDWR)
- Garth Newton (IDWR)
- Dr. David Tuthill (IDWR)
- Ed Squires (Hydro Logic, Inc.)

EXECUTIVE SUMMARY

The Treasure Valley Hydrologic Project (TVHP) was a multi-year study to develop a better understanding of ground water resources in the lower Boise River basin (Treasure Valley) of southwestern Idaho. This report presents, as part of the TVHP, a summary of hydrologic conditions in the Treasure Valley aquifer system. The report describes (1) Treasure Valley aquifer characteristics, (2) multi-level ground water monitoring wells installed as part of the TVHP, (3) results from water level measurements, and (5) aquifer inflows and outflows. The report concludes with a description of ground water flow in Treasure Valley aquifers. This conceptual model of ground water flow forms the basis for a series of numerical simulations (Petrich, 2004a; Petrich, 2004b) conducted as part of the TVHP.

The Treasure Valley aquifer system resides in a complex series of interbedded, tilted, faulted, and eroded sediments extending to depths of over 6,000 feet (Wood and Clemens, in press). These sedimentary aquifers contain shallow, local flow systems (with ground water residence times ranging from days to tens of years), and a deep, regional flow system (with residence times ranging from hundreds to tens of thousands of years). Only a few wells extend beyond a depth of 1,200 feet.

Water levels indicate general ground water movement in a westerly to southwesterly direction. Individual hydrographs indicate relatively stable water levels in many areas. Some areas, such as southeast Boise and an area south of Lake Lowell, have experienced water level declines of approximately 30 and 65 feet, respectively. A number of wells in other areas (primarily in the eastern portion of the valley) have also experienced water level declines over the last several years. These declines have generally been less than 10 feet.

The largest component of recharge to shallow aquifers is seepage from the canal system and infiltration associated with irrigated agriculture. Recharge to the deeper aquifer occurs in the eastern portion of the valley and along the Boise Front. Ground water discharge to rivers, drains, and canals represents the dominant form of discharge from the Treasure Valley aquifer system. The primary form of natural discharge from the deeper aquifers is thought to be regional upwelling in the southern and western portions of the basin, with ultimate discharge to the Boise River and/or Snake River.

Ground water residence times in the deeper, regional aquifer system were found to increase with depth and with distance along a regional east-to-west-trending flow path. Residence time estimates ranged from thousands to tens of thousands of years.

Relatively long residence times in the regional flow system (over 20,000 years) imply that (1) regional aquifers are marginally transmissive, (2) recharge rates to the deeper regional aquifers are limited, and/or (3) regional aquifers are discharge-limited. Although there are abundant silt and clay layers with low hydraulic conductivity, productive sand layers are present throughout central portions of the valley. These sand zones are tapped by many

irrigation and municipal wells. Recharge to the deeper, regional system is limited, but generally has been sufficient for current rates of withdrawal. Thick lacustrine clays at the distal end of the valley likely inhibit upward (discharge) flow, limiting the amount of water that can flow through the system.

TABLE OF CONTENTS

| | |
|--|-----|
| Acknowledgements | ii |
| Executive Summary..... | iii |
| 1. Introduction | 1 |
| 1.1. Project Background | 1 |
| 1.2. Report Scope..... | 1 |
| 1.3. Previous Investigations | 2 |
| 2. Description of Project Area | 4 |
| 2.1. Project Area | 4 |
| 2.2. Population..... | 5 |
| 2.3. Climate..... | 6 |
| 2.4. Land Use | 8 |
| 2.5. Irrigation | 8 |
| 3. Aquifer Description | 13 |
| 3.1. Introduction..... | 13 |
| 3.2. Geologic Setting | 13 |
| 3.3. Stratigraphic Profile..... | 14 |
| 3.4. Aquifer Description | 21 |
| 3.5. Water Chemistry | 23 |
| 3.6. Ground Water Flow Systems..... | 24 |
| 3.7. Hydraulic Properties | 25 |
| 3.8. Geothermal System..... | 29 |
| 4. Dedicated TVHP Monitoring Wells | 31 |
| 5. Ground Water Levels | 36 |
| 5.1. Introduction..... | 36 |
| 5.2. Mass Ground Water Level Measurements | 36 |
| 5.2.1. Data Collection | 38 |
| 5.2.2. Potentiometric Surface Maps..... | 38 |
| 5.2.3. Seasonal Water Level Changes..... | 41 |
| 5.3. Periodic Ground Water Level Monitoring..... | 42 |
| 5.3.1. Well Network Description | 42 |
| 5.3.2. Hydrographs..... | 43 |
| 6. Aquifer Inflows and Outflows..... | 46 |
| 6.1. Introduction..... | 46 |
| 6.2. 1996 Water Budget | 46 |
| 7. Treasure Valley Ground Water Flow Characteristics | 49 |
| 8. References | 54 |
| Appendix A. Conversion Factors | 59 |

| | | |
|-------------|--|-----|
| Appendix B. | Aquifer Test Data..... | 60 |
| Appendix C. | Construction Details for Dedicated, Multi-Level Piezometers..... | 83 |
| Appendix D. | Construction and Measurement Details for Mass Measurement Wells..... | 84 |
| Appendix E. | Potentiometric Surface Maps..... | 106 |
| Appendix F. | Hydrographs..... | 117 |
| Appendix G. | Selected Hydrographs Showing Changes | 139 |

LIST OF FIGURES

| | |
|---|----|
| Figure 2-1: Map showing the Boise River basin, lower Boise River sub-basin, and Treasure Valley Hydrologic Project | 4 |
| Figure 2-2: Treasure Valley area. | 5 |
| Figure 2-3: Treasure Valley population growth for the period 1970-2000 (solid lines) and projected growth for the period 2000-2020 (dashed lines). | 6 |
| Figure 2-4: Monthly average temperatures. | 6 |
| Figure 2-5: Annual precipitation at the Boise Airport between 1940 and 2001. | 7 |
| Figure 2-6: Boise River basin precipitation at selected sites. | 7 |
| Figure 2-7: Treasure Valley land use. | 8 |
| Figure 2-8: Changes in Treasure Valley irrigated lands between 1938–1939 and 2000 (IDWR data). | 9 |
| Figure 2-9: Major and intermediate canals in the Treasure Valley (IDWR data). | 10 |
| Figure 2-10: Treasure Valley irrigation district boundaries (IDWR data). | 11 |
| Figure 2-11: Treasure Valley flood and sprinkler irrigation in 1994 (IDWR data). | 12 |
| Figure 3-1: Cross-section of the WSRP. | 15 |
| Figure 3-2: Upper Miocene basalt surface. | 16 |
| Figure 3-3: Surficial geology map. | 20 |
| Figure 3-4: Subdivisions of Idaho Group sediments. | 22 |
| Figure 3-5: Transmissivity estimates for wells completed between 0 and 300 feet below ground surface. | 26 |
| Figure 3-6: Transmissivity estimates for wells completed below 300 feet below ground surface. | 27 |
| Figure 3-7: Locations of selected single and multiple well aquifer tests. | 28 |
| Figure 4-1: TVHP monitoring well locations. | 31 |
| Figure 4-2: Hydrograph for TVHP #1. | 32 |
| Figure 4-3: Hydrograph for TVHP #2. | 33 |
| Figure 4-4: Hydrograph for TVHP #3. | 34 |
| Figure 4-5: Hydrograph for TVHP #4. | 35 |
| Figure 5-1: Potentiometric surface, spring 1996, shallow zone (240 wells). | 39 |
| Figure 5-2: Potentiometric surface, spring 1996, intermediate zone (49 wells). | 39 |

| | |
|--|-----|
| Figure 5-3: Potentiometric surface, spring 1996, deep zone (45 wells). | 40 |
| Figure 5-4: Spring and fall 1996 change map..... | 41 |
| Figure 5-5: Locations of hydrograph wells..... | 42 |
| Figure 5-6: Locations of wells showing substantial water level changes..... | 45 |
| Figure E-1: Spring 1996, shallow zone (240 wells). | 106 |
| Figure E-2: Spring 1996, intermediate zone (49 wells)..... | 107 |
| Figure E-3: Spring 1996, deep zone (45 wells). | 107 |
| Figure E-4: Fall 1996, shallow zone (235 wells)..... | 108 |
| Figure E-5: Fall 1996, intermediate zone (49 wells). | 108 |
| Figure E-6: Fall 1996, deep zone (35 wells)..... | 109 |
| Figure E-7: Spring 1998, shallow zone (259 wells). | 109 |
| Figure E-8: Spring 1998, intermediate zone (50 wells)..... | 110 |
| Figure E-9: Spring 1998, deep zone (38 wells). | 110 |
| Figure E-10: Fall 1998, shallow zone (245 wells)..... | 111 |
| Figure E-11: Fall 1998, intermediate zone (44 wells). | 111 |
| Figure E-12: Fall 1998, deep zone (29 wells)..... | 112 |
| Figure E-13: Spring 2000, shallow zone (238 wells). | 112 |
| Figure E-14: Spring 2000, intermediate zone (42 wells)..... | 113 |
| Figure E-15: Spring 2000, deep zone (27 wells). | 113 |
| Figure E-16: Fall 2000, shallow zone (16 wells)..... | 114 |
| Figure E-17: Fall 2000, intermediate zone (34 wells). | 114 |
| Figure E-18: Fall 2000, deep zone (26 wells)..... | 115 |
| Figure E-19: Fall 2001, shallow zone (212 wells)..... | 115 |
| Figure E-20: Fall 2001, intermediate zone (35 wells). | 116 |
| Figure E-21: Fall 2001, deep zone (27 wells)..... | 116 |

LIST OF TABLES

| | |
|---|----|
| Table 3-1: Geologic time during the Cenozoic and Mesozoic eras..... | 14 |
| Table 3-2: Stratigraphic names in the WSRP. | 18 |
| Table 4-1: Construction details for TVHP monitoring wells..... | 32 |
| Table 5-1: Numbers of wells measured during each of four mass water level measurements..... | 37 |
| Table 5-2: Model layer thicknesses. | 37 |
| Table 5-3: Approximate number of monitoring wells with increasing or decreasing water levels. | 44 |
| Table 6-1: Summary of recharge and discharge estimates contained in the 1996 water budget..... | 47 |

1. INTRODUCTION

1.1. Project Background

The lower Boise River basin of southwestern Idaho (commonly referred to as the “Treasure Valley”) has experienced significant population growth, local ground water declines, and periodic drought conditions in the last two decades. This led to public concern about the status and future of water resources in the valley. The Treasure Valley Hydrologic Project (TVHP) was formed to address some of these issues and to provide a framework for future water management. The purpose of the TVHP was to develop a better understanding of ground water resources in the Treasure Valley and to evaluate changes in regional and local ground water conditions (Petrich, 2004c). The project included numerous components, including (1) water level measurements, (2) monitoring well construction, (3) water budget development, and (4) numerical modeling.

1.2. Report Scope

This report presents a summary of hydrologic conditions in the Treasure Valley aquifer system. The report includes descriptions of the (1) Treasure Valley area, (2) Treasure Valley aquifers, (3) multi-level ground water monitoring wells installed as part of the TVHP, (4) ground water levels based on well measurements, and (5) aquifer inflows and outflows. The report concludes with a description of ground water flow in Treasure Valley aquifers. This description of ground water flow forms the basis for a series of numerical simulations (Petrich, 2004a; 2004b).

This report draws, in part, from other reports and papers prepared as part of the TVHP. These include the following:

1. Geologic and Tectonic History of the Western Snake River Plain, Idaho and Oregon (Wood and Clemens, in press)
2. Water Budget for the Treasure Valley Aquifer System for the years 1996 and 2000 (Urban, 2004)
3. Simulation of Ground Water Flow in the Lower Boise River Basin (Petrich, 2004a)
4. Ground Water Recharge and Flow in the Regional Treasure Valley Aquifer System (Hutchings and Petrich, 2002a)
5. Influence of canal seepage on aquifer recharge near the New York Canal (Hutchings and Petrich, 2002b)

6. Domestic, Commercial, Municipal, and Industrial Water Demand Assessment and Forecast in Ada and Canyon Counties, Idaho (Cook et al., 2001)
7. Stratigraphic Studies of the Boise (Idaho) Aquifer System using Borehole Geophysical logs with Emphasis on Facies Identification of Sand Aquifers (Squires and Wood, 2001)
8. Seismic Reflection Project - UPRR 2000 Profile (Liberty and Wood, 2001)
9. Hydrogeology, Geochemistry, and Well Construction of the Treasure Valley Hydrologic Project Monitoring Well #1 (Dittus et al., 1999)
10. 1996 Water Budget for the Treasure Valley Aquifer System (Urban and Petrich, 1998)
11. New York Canal Geologic Cross Section, Seepage Gain/Loss Data, and Ground Water Hydrographs: Compilation and Findings (Carlson and Petrich, 1998)
12. Seismic Reflection Imaging of a Geothermal Aquifer in an Urban Setting (Liberty, 1998)
13. Structure Contour Map of the Top of the Mudstone Facies, Western Snake Supporting Data for Groundwater Conditions and Aquifer Testing of the Tenmile Ridge Area of South Boise, Ada County, Idaho (Dittus et al., 1998)
14. Ground Water Quality Characterization and Initial Trend Analysis for the Treasure Valley Shallow and Deep Hydrologic Subareas (Neely and Crockett, 1998)
15. Structure Contour Map of the Top of the Mudstone Facies, Western Snake River Plain, Idaho (Wood, 1997c)
16. Cross Section of the Treasure Valley in the Boise Area: Notes on the Geology of the Boise, Ontario, Parma, and Notus areas (Beukelman, 1997a; Beukelman, 1997b; Beukelman, 1997c; Beukelman, 1997d)
17. Preliminary Map of the Base of the Sedimentary Section of the Western Snake River Plain (Wood, 1996b)

1.3. Previous Investigations

Numerous previous investigations have focused on geology and hydrology in the Treasure Valley or Western Snake River Plain (WSRP). Lindgren (1898) provided early geologic descriptions of the Boise River Valley. Mabey (1982), Malde (1991), Wood and Anderson (1981), and Wood and Clemens (in press) described the geological setting. Othberg (1994), Othberg and Stanford (1992), Wood and Anderson (1981), Malde (1991), Clemens (1993), Wood (1994), and Wood and Clemens (in press) described valley stratigraphy. Several authors have described aquifer characteristics, including Dion (1972), Ralston and Chapman (1970), Wood and

Anderson (1981), Squires et al. (1992); and Wood and Clemens (in press). Previous ground water flow models were developed by Lindgren (1982), Newton (1991), and Brockway and Brockway (1999). The work conducted as part of the TVHP builds on these efforts.

2. DESCRIPTION OF PROJECT AREA

2.1. Project Area

The TVHP project area consists of (1) the lower Boise River sub-basin and (2) the area between the lower Boise River sub-basin and the Snake River (Figure 2-1). The lower Boise River sub-basin begins where the Boise River exits the mountains near Lucky Peak Reservoir. From Lucky Peak Dam, the lower Boise River flows about 64 (river) miles northwestward through the Treasure Valley to its confluence with the Snake River. The Boise River drains the central portion of the valley; the Snake River drains the southern portion of the valley. The project area (shown in red) extends south to the Snake River because ground water flows from some portions of the lower Boise River basin south toward the Snake River.

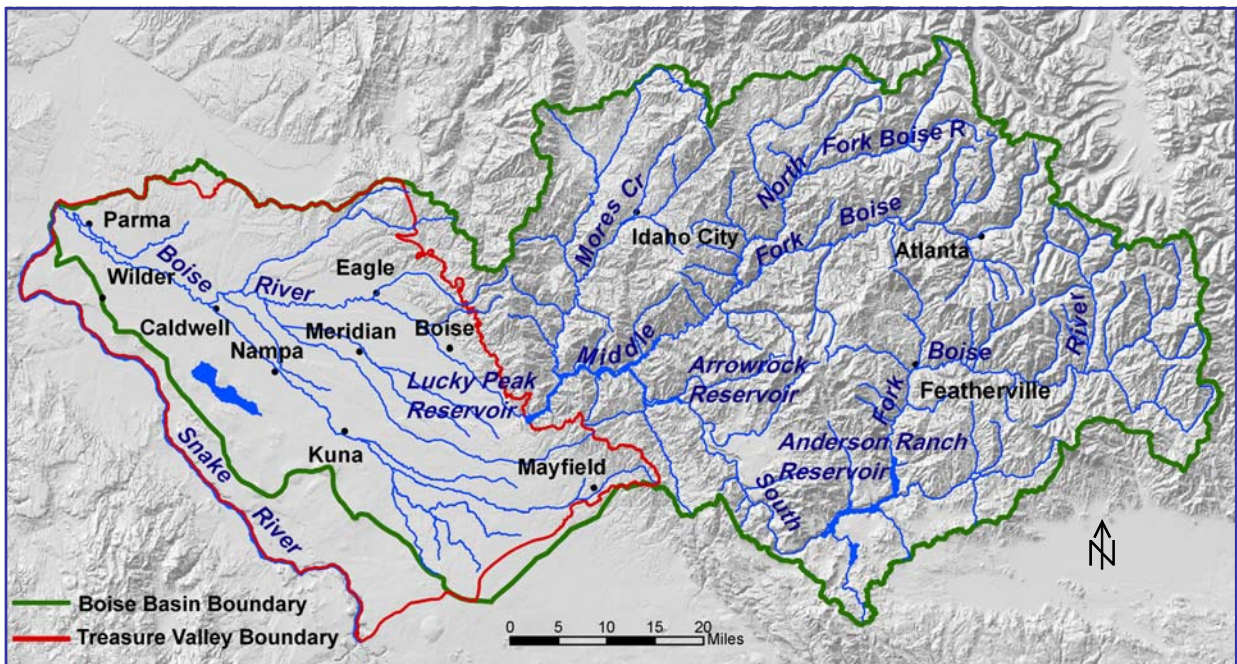


Figure 2-1: Map showing the Boise River basin, lower Boise River sub-basin, and Treasure Valley Hydrologic Project

The entire Boise River basin covers over 4,020 square miles in southwestern Idaho. Elevations in the basin range from a high of 10,174 feet above mean sea level (msl) to a low of 2,185 feet (msl) at the confluence of the Boise and Snake Rivers.

Most of the surface water in the lower Boise River basin originates in the upper Boise River basin. Much of the runoff from high elevation areas is stored in three reservoirs:

Anderson Ranch Reservoir, Arrowrock Reservoir, and Lucky Peak Reservoir (Figure 2-1). The northern portion of the basin drains a large portion of Idaho's south-central mountains. Major surface water bodies in the Treasure Valley include the Boise River, Lake Lowell, and the Snake River (Figure 2-2).

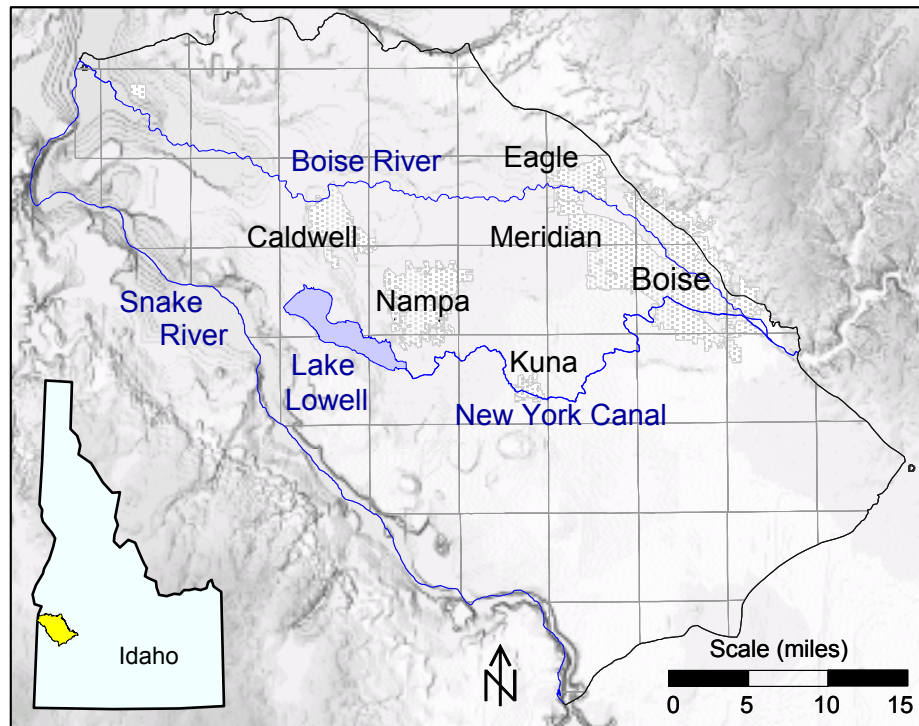


Figure 2-2: Treasure Valley area.

2.2. Population

The Treasure Valley was home to approximately 426,300 people in 2000¹, or about one-third of Idaho's population. Most of the Treasure Valley population is concentrated in the growing cities of Boise, Nampa, Caldwell, and Meridian, as well as a number of smaller communities (Figure 2-2).

Population growth in these areas for the period 1970–2000 is shown in Figure 2-3. The population is projected to grow to approximately 655,000 people by 2020², an increase of over 50% in 20 years.

¹ Source: U. S. Census data, presented by the Community Planning Association of Southwest Idaho (<http://www.compassidaho.org/demo/profiledemocharacteristics.pdf>).

² Source: Community Planning Association of Southwest Idaho (<http://compassidaho.org>)

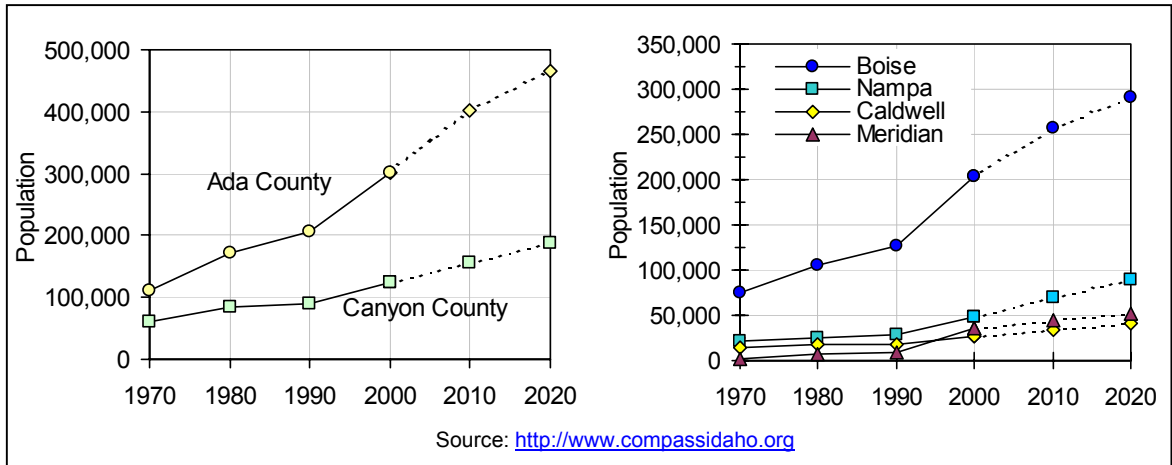


Figure 2-3: Treasure Valley population growth for the period 1970-2000 (solid lines) and projected growth for the period 2000-2020 (dashed lines).

2.3. Climate

The Treasure Valley has a temperate and arid to semi-arid climate. Average high temperatures range from about 90°F in summer to 36°F in winter (Figure 2-4); average low temperatures range from about 20°F in winter to about 56°F in summer. The average precipitation ranges from about 8 to 14 inches throughout most of the valley (Figure 2-5), most of which falls during the colder months (Figure 2-6).

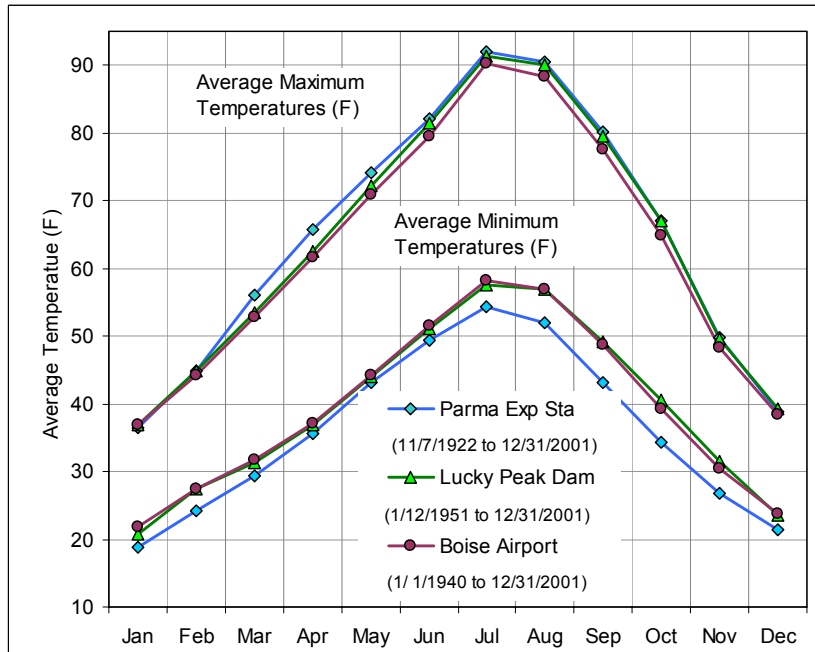
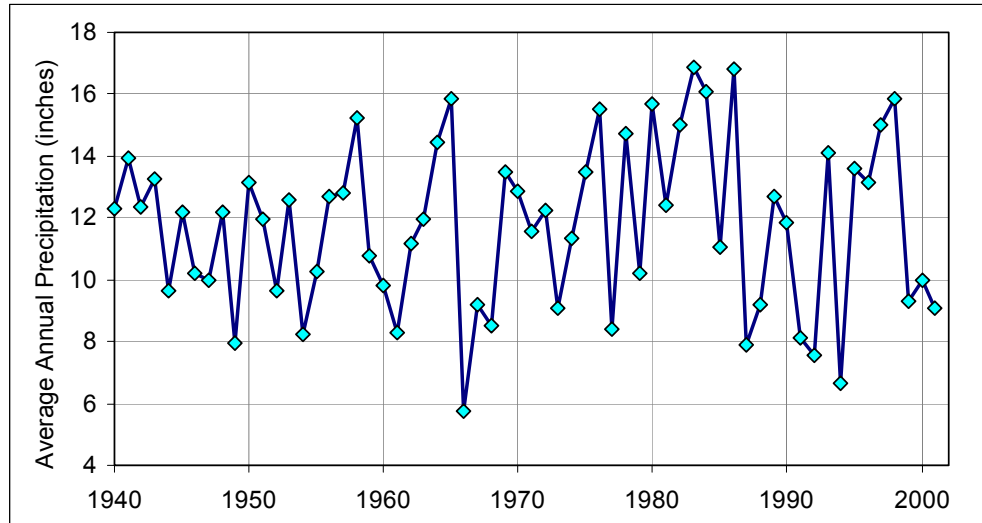
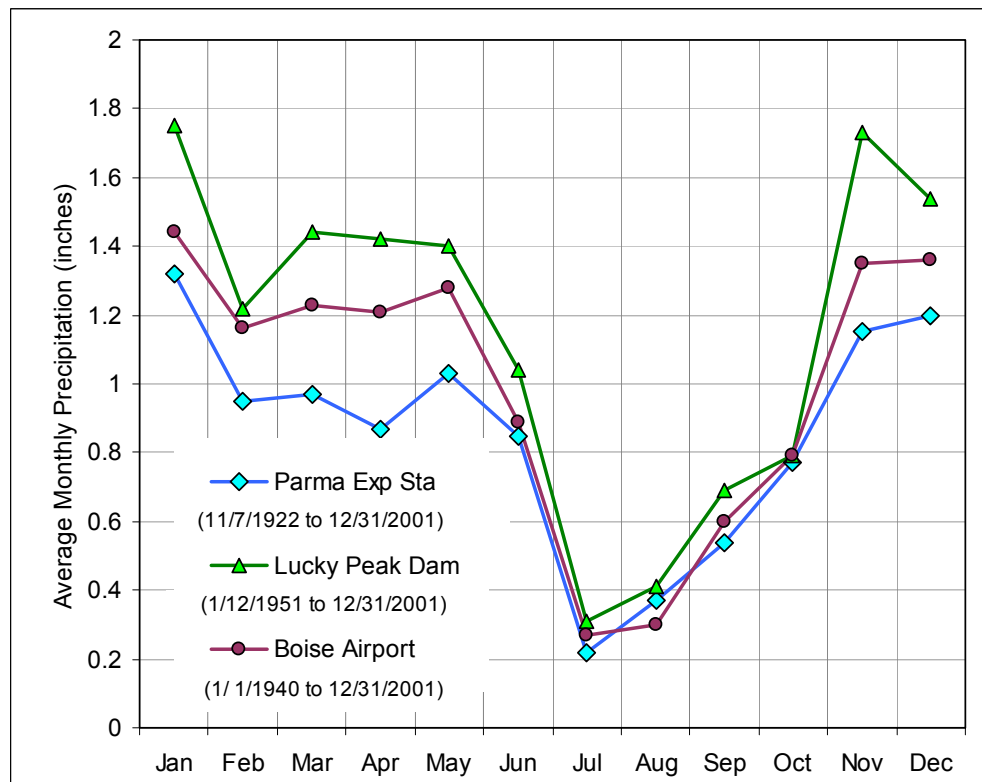


Figure 2-4: Monthly average temperatures.



Source: State Climate Services, Biological and Agricultural Engineering Department, University of Idaho.

Figure 2-5: Annual precipitation at the Boise Airport between 1940 and 2001.



Source: State Climate Services, Biological and Agricultural Engineering Department, University of Idaho.

Figure 2-6: Boise River basin precipitation at selected sites.

2.4. Land Use

Approximately half of the land area in the Treasure Valley (Figure 2-7) is devoted to irrigated agriculture. Major crops grown in the Treasure Valley include alfalfa and alfalfa seed, sugar beets, wheat, beans, silage and seed corn, onions, and potatoes. Residential and commercial uses account for approximately 10% of the land use, and the remaining land is primarily open range and foothills.

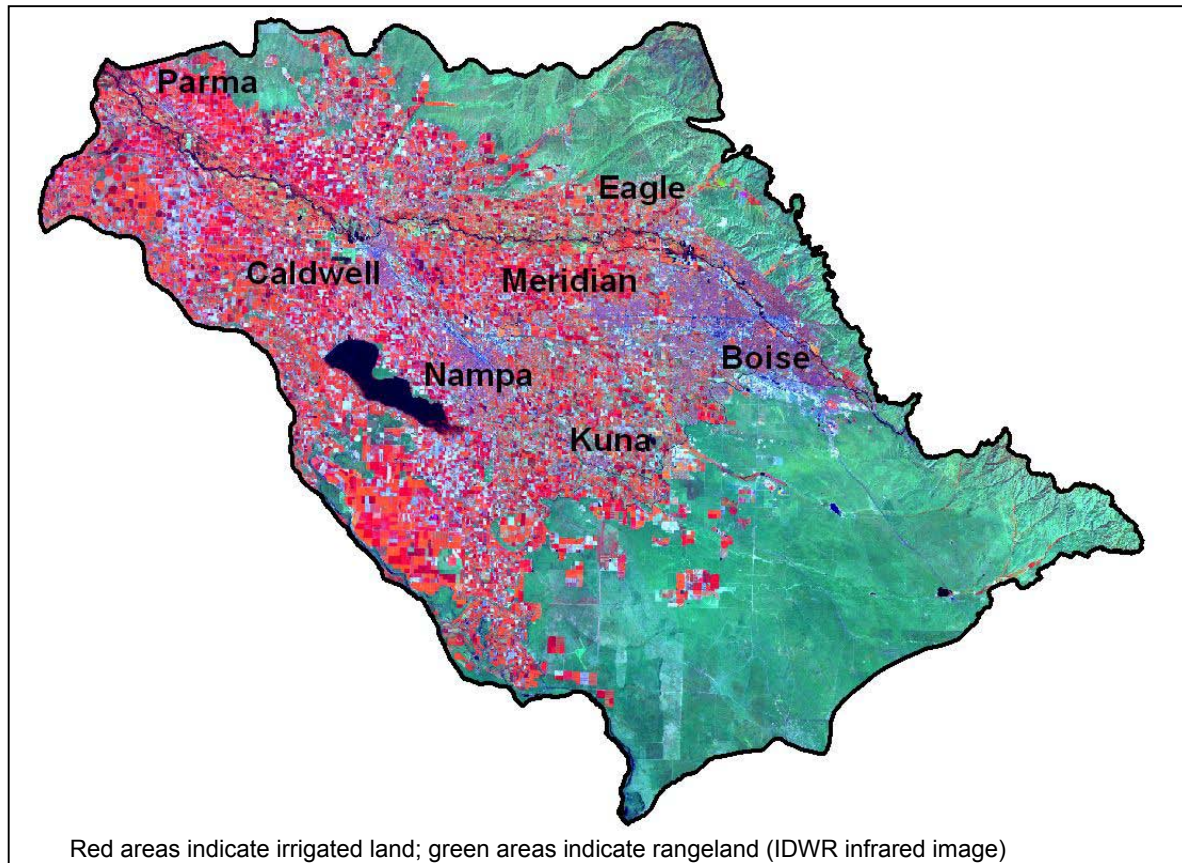


Figure 2-7: Treasure Valley land use.

2.5. Irrigation

Large-scale irrigation in the Treasure Valley began in the late 1800s, and by the 1930s, irrigated lands covered a large portion of the valley (Figure 2-8). The primary application method is flood irrigation, with water diverted from the Boise River. Expansion of irrigated land continued after 1939 (Figure 2-8). Some of the water for expanded irrigation was drawn from the Payette River (through the Black Canyon canal system), and some was obtained from ground water sources. In 1996, approximately 252,000 acres were irrigated with surface water (Urban and Petrich,

1998). An additional estimated 42,300 acres were irrigated with ground water. An increasing amount of irrigated land has been taken out of production in recent decades (Figure 2-8). Most of the loss of irrigated land between 1938–1939 and 2000 can be attributed to urban expansion.

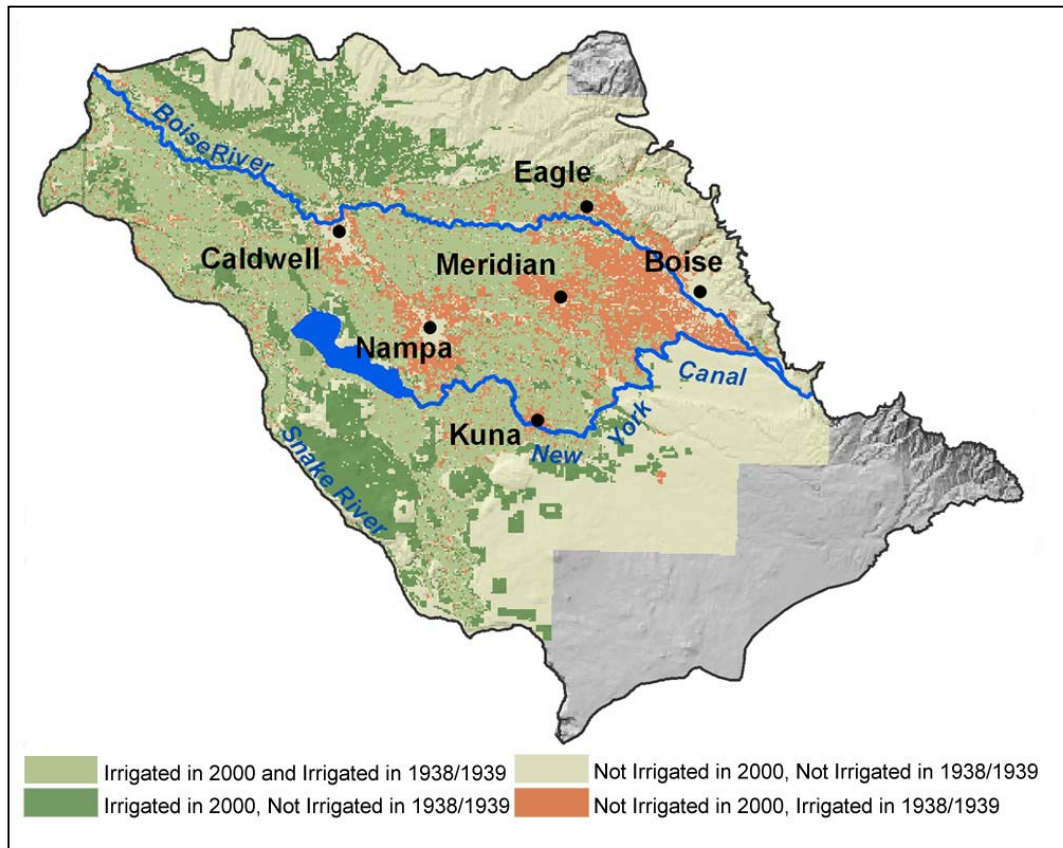


Figure 2-8: Changes in Treasure Valley irrigated lands between 1938–1939 and 2000 (IDWR data).

The region's croplands are irrigated primarily with surface water through an extensive network of reservoirs and canals. The first canals were constructed in the 1860s; there are now over 1,100 miles of major and intermediate canals in the Treasure Valley (Figure 2-9)³. The majority of canals are owned and maintained by canal companies and irrigation districts (Figure 2-10). The Treasure Valley also has an extensive network of drains (and ditch companies that service the drains). These channels serve to drain water (often originating from irrigation practices) from low-lying areas. In some cases the drains are also canals, and shallow ground water discharging to drains is used for additional surface water irrigation.

³ Figure created by IDWR based on canals included in 1:100,000 scale topographic mapping.

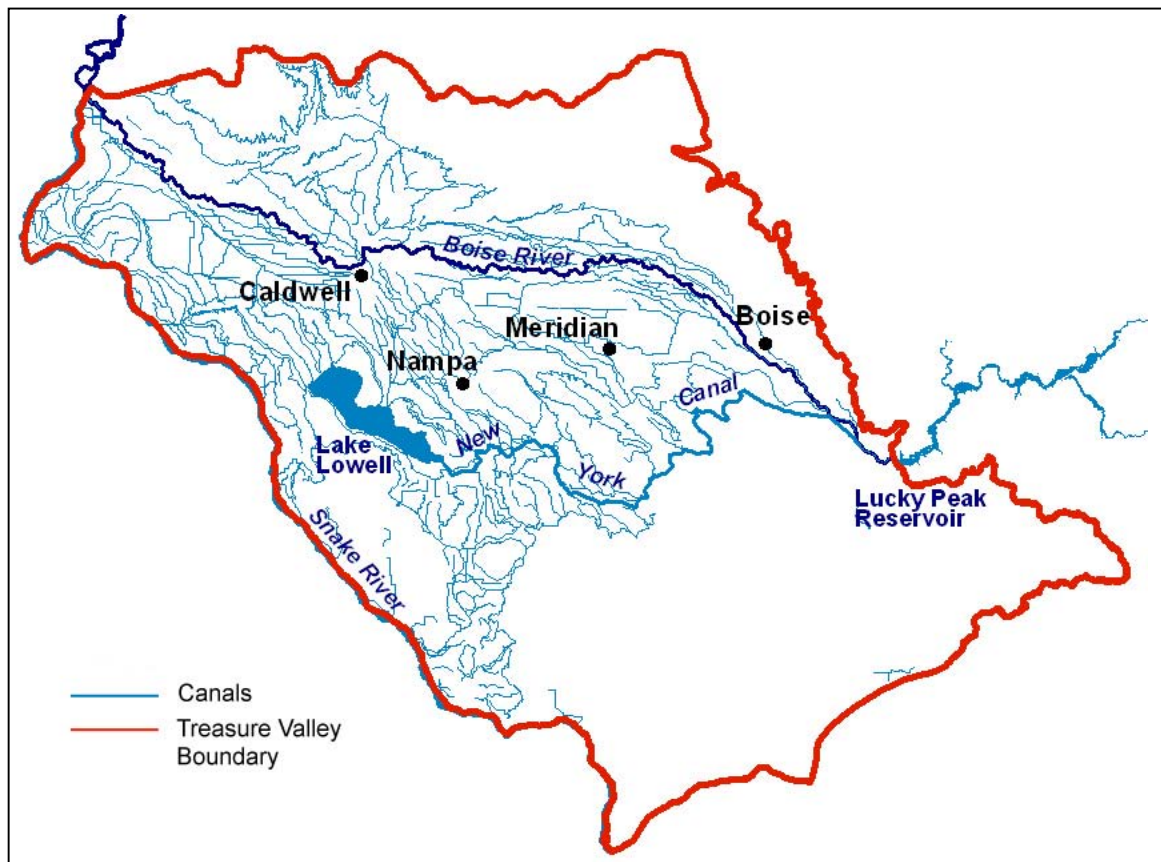


Figure 2-9: Major and intermediate canals in the Treasure Valley (IDWR data).

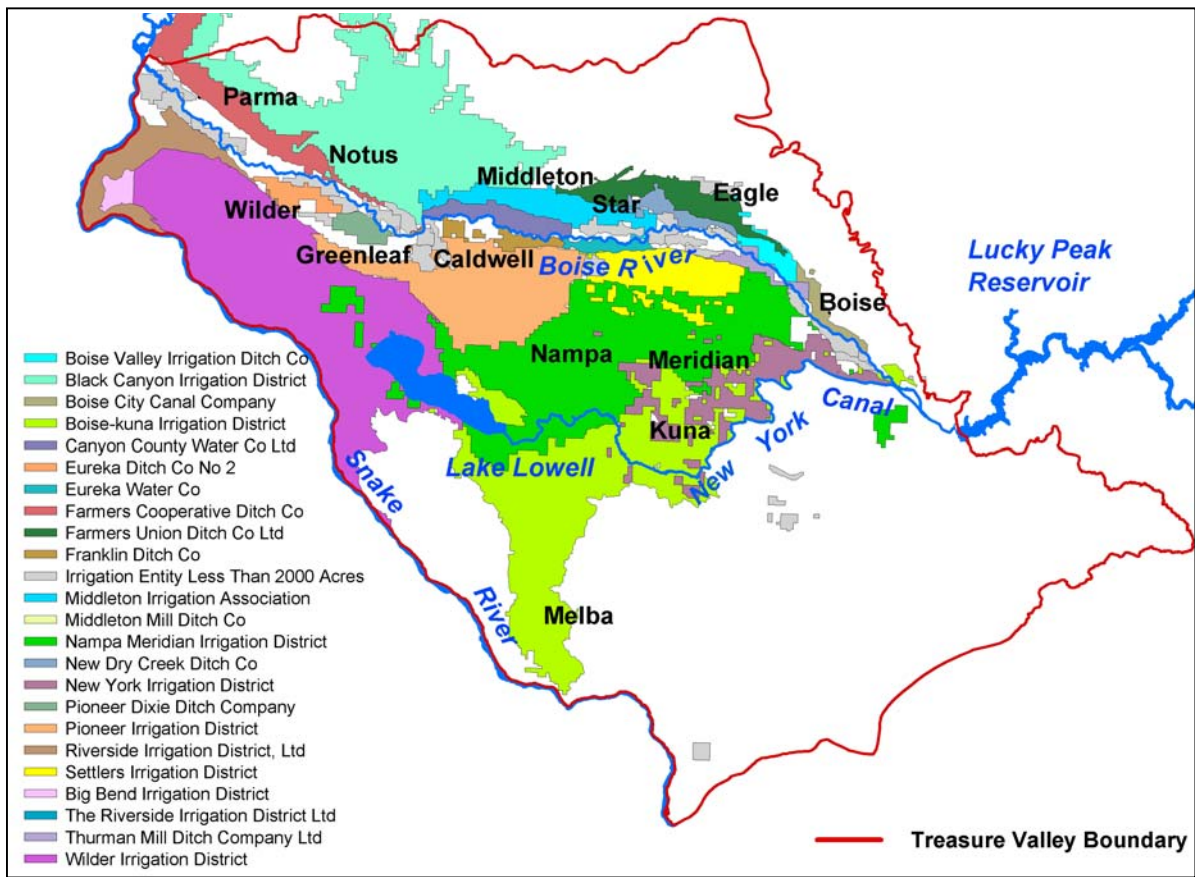


Figure 2-10: Treasure Valley irrigation district boundaries (IDWR data).

Of the estimated 252,000 acres irrigated in 1996 (Figure 2-11), approximately 101,000 acres was irrigated by sprinkler systems (Urban and Petrich, 1998). Of this total, approximately 42,000 acres (42%) are irrigated with ground water and 59,000 acres (58%) are irrigated with surface water. Ground water is used for irrigation in locations where surface water is unavailable or in times of surface water shortages. Irrigation wells were installed during the late 1920s and 1930s to provide supplemental irrigation during times of drought. Additional wells for primary and supplemental irrigation (and domestic uses) have been drilled during the last several decades.

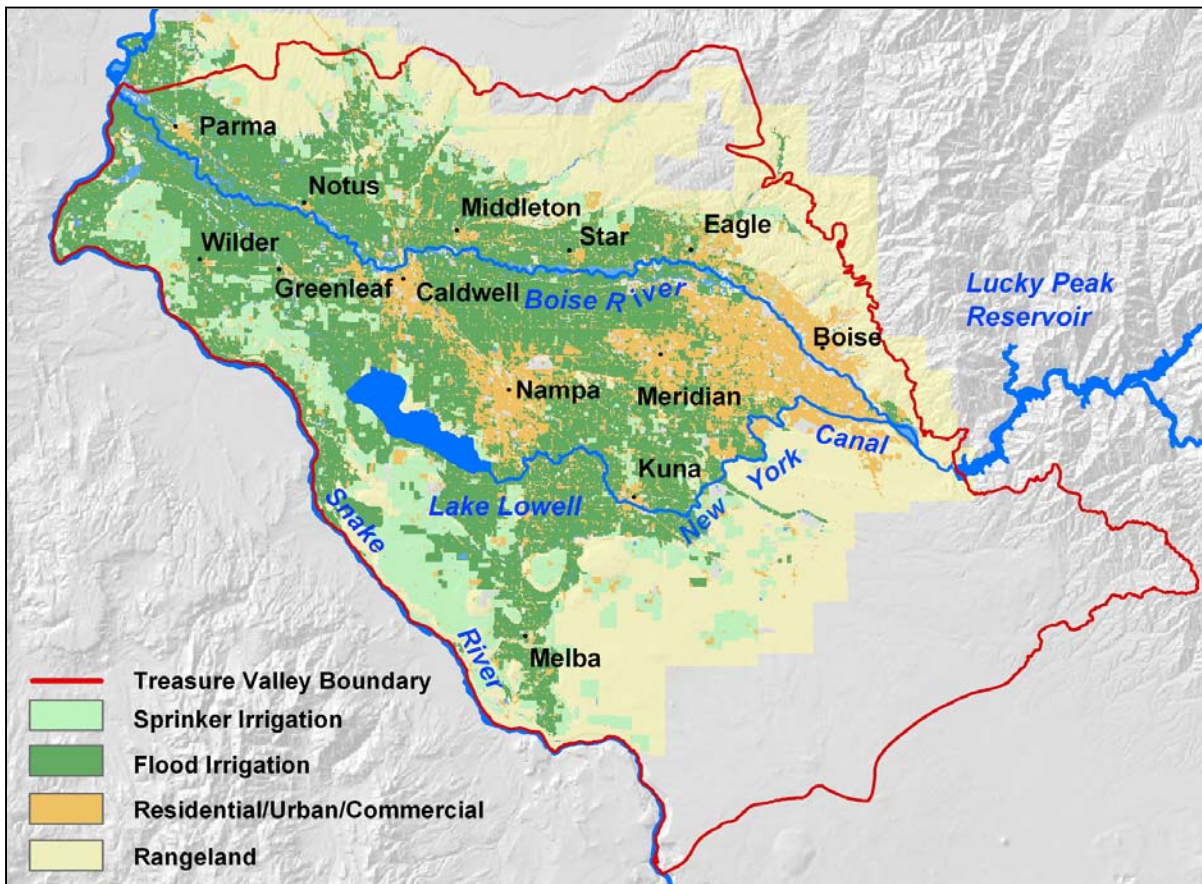


Figure 2-11: Treasure Valley flood and sprinkler irrigation in 1994 (IDWR data).

3. AQUIFER DESCRIPTION

3.1. Introduction

This section provides a description of Treasure Valley aquifer characteristics. Material for this section was drawn from geological investigations conducted prior to and as part of the TVHP. A description of flow characteristics, based on aquifer characteristics, hydraulic heads, hydraulic gradients, and estimates of inflows and outflows, is provided in Section 7.

3.2. Geologic Setting

The lower Boise River sub-basin (Treasure Valley) is located within the northwest-trending topographic depression known as the Western Snake River Plain (WSRP). The WSRP is a Neogene-aged (Table 3-1) continental rift basin (Wood and Clemens, in press), separating Cretaceous granitic mountains of west-central Idaho from the granitic/volcanic Owyhee mountains in southwestern Idaho. The WSRP now has the appearance of a northwest-trending graben associated with continental rifting (Mabey, 1982; Wood and Anderson, 1981). The WSRP extends from around Twin Falls, Idaho, northwestward to Vale, Oregon. The section of the WSRP containing the lower Boise River valley is about 30 miles wide (Figure 2-1 and Figure 2-2).

The WSRP is believed to have been formed by crustal extension (Malde, 1991, p.251). Malde suggests that the basin began forming as early as 17 million years ago (Ma), although Wood and Clemens (in press) suggest that the basin began forming about 11 Ma, with major faulting that occurred between 11 and 9 Ma (Wood and Clemens, in press). Miocene-aged (Table 3-1) rhyolite flows and domes are present along the margins of the WSRP. Rhyolite is present in outcrops in the Boise Foothills near Boise. Geothermal wells in the downtown Boise area draw water from two rhyolite zones separated by arkosic sand and granitic gravels. Deep wells north and west of Boise have not penetrated rhyolite (to the authors' knowledge); for example, the 14,100-foot-deep J.N. James well near Meridian did not encounter rhyolite (S. Wood, pers. comm., 2000). For this reason Wood and Clemens (in press) hypothesize that much of the plain may have been an upland during Miocene silicic volcanism.

The basin dropped, relative to surrounding highlands, by isostatic compensation (Malde, 1991) in response to thick accumulations of volcanics associated with rifting and deposition of overlying sediments (Mabey, 1982). Wood and Clemens (in press), Squires and Wood (2001), and others have described fluvial and lacustrine sediment deposition that occurred in the basin during this time (Section 3.3).

| Era | Period | | Epoch | Approximate Duration (Millions of Years) | Approximate beginning (Millions of Years Ago) |
|----------|------------|-----------|-------------------|---|--|
| Cenozoic | Quaternary | | Holocene (Recent) | Approx. Last 10,000 years | 10,000 years |
| | | | Pleistocene | 2 | 2 |
| | Tertiary | Neogene | Pliocene | 3 | 5 |
| | | | Miocene | 18 | 23 |
| | | Paleogene | Oligocene | 15 | 38 |
| | | | Eocene | 16 | 54 |
| | | | Paleocene | 11 | 65 |
| | | | | | |
| Mesozoic | Cretaceous | | | 71 | 136 |
| | Jurassic | | | 54 | 190 |
| | Triassic | | | 35 | 225 |


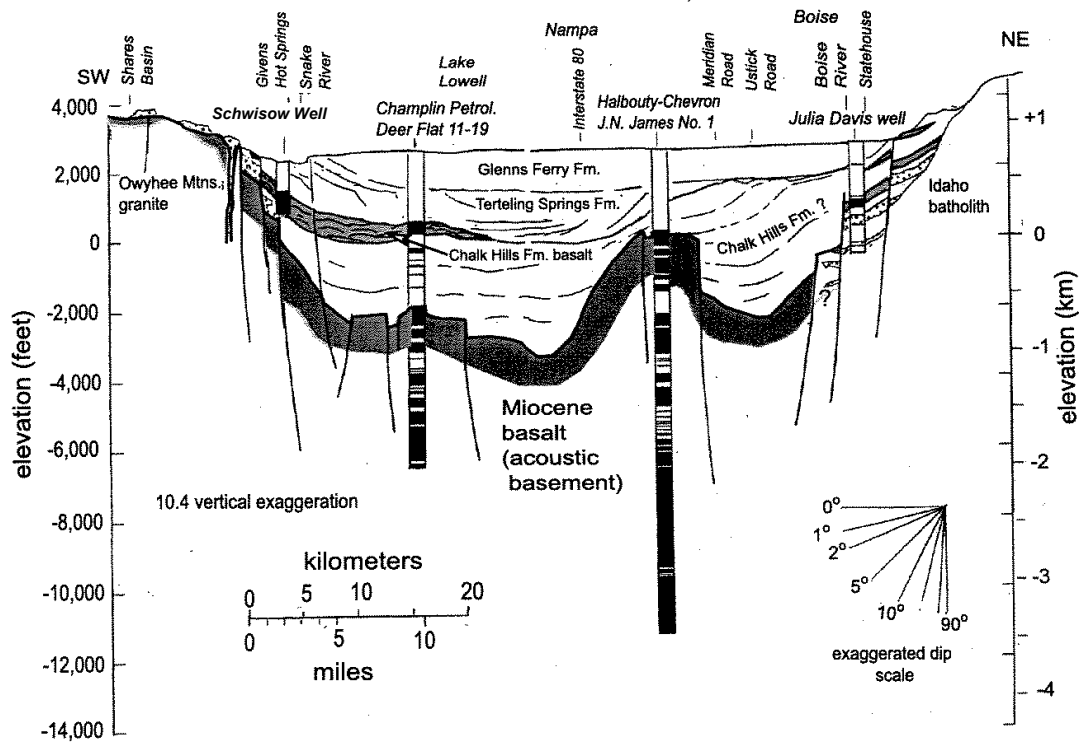
 Shading indicates ages represented in Treasure Valley geology.

Table 3-1: Geologic time during the Cenozoic and Mesozoic eras.

Volcanic activity returned to the WSRP during the late stages of Lake Idaho (see Section 3.3) about 5.5 Ma (Wood and Clemens, in press). Lava erupted from a line or series of volcanic vents referred to as the Kuna–Mountain Home volcanic rift. These Quaternary basalt flows, assigned to the upper Snake River Group (Malde, 1991, p.266; Malde and Powers, 1962), flowed across portions of the ancestral Snake River Valley in an area that is now south of the Boise River (Malde, 1991). The Snake River then changed course, incising at its present location along the southern margin of the basalt flows. More recent eruptions (from Kuna Butte and other local sources along the rift) spilled lava into the Snake River Canyon south of Melba. The Snake River has since incised into this basalt (Malde, 1991, p.267).

3.3. Stratigraphic Profile

The general stratigraphy of the WSRP consists of interbedded layers of sand, silt, and clay overlying Miocene tuffaceous sediments and basalt flows (Figure 3-2). The sediments, ranging up to 6,000 feet in thickness in some locations, distinguish the WSRP from the Eastern Snake River Plain (ESRP), which is primarily Quaternary basalt in its upper section (Wood and Anderson, 1981, p.9).

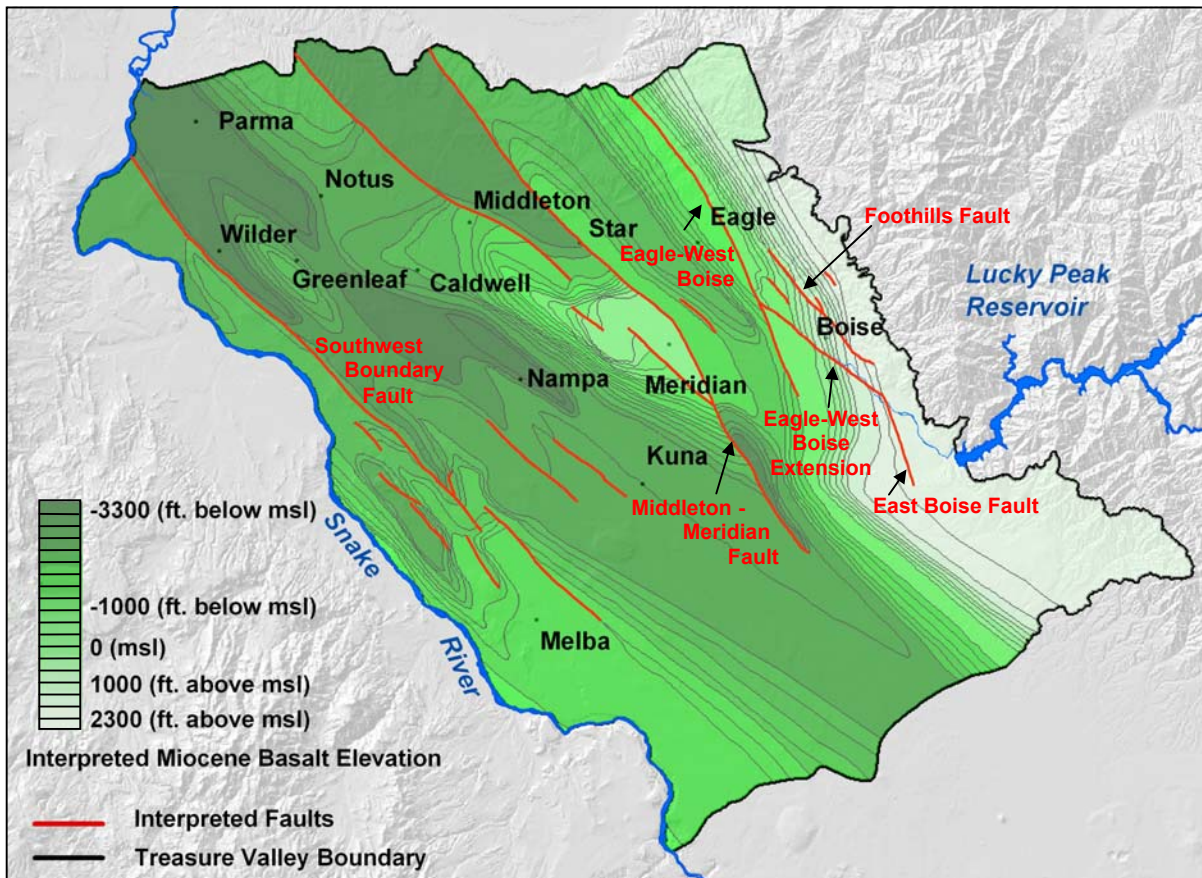


From Wood and Clemens (in press).

Figure 3-1: Cross-section of the WSRP.

The Miocene-aged tuffaceous basalt rests unconformably on granitic rocks of the Idaho Batholith, on late Miocene rhyolite, and/or on basalt of the Miocene Columbia River Group (Wood and Clemens, in press). The basalt assemblage is several hundred feet thick in the Boise area and forms the basement for sediments comprising the Treasure Valley aquifers.

The upper surface of the Miocene basalt forms a highly irregular surface (Figure 3-2), intersected by numerous northwest-southeast trending faults (Figure 3-3). The basalt surface was interpreted by Wood (1996b) based on well data, deep seismic reflection data, subsurface investigations in east Boise (Squires et al., 1992), and shallow seismic data (Liberty, 1996a; Liberty, 1996b).



Based on Wood (1997b) and Squires et al. (1992).

Figure 3-2: Upper Miocene basalt surface.

Faulting has been described by numerous authors (Barrash and Dougherty, 1995; Liberty, 1996a; Liberty, 1996b; Liberty, 1998; Liberty and Wood, 2001; Malde, 1991, p. 259; Othberg and Stanford, 1992; Squires et al., 1993; Squires et al., 1992; Wood, 1994; Wood, 1996b; Wood and Anderson, 1981; Wood and Clemens, in press) on the basis of surface geomorphology, stratigraphic correlations, and seismic reflection surveys and associated interpretations. Displacement along these faults ranges from feet to hundreds of feet. Cumulative fault offsets (up to several hundred feet of displacement) and basinward downwarping account for much of the basin structural relief (Figure 3-3). The East Boise Fault truncates the Boise Fan sediments with 400 to 600 feet of displacement along the fault (Squires et al., 1992). Additional faults are illustrated in Othberg and Stanford (1992).

Other major faults include the Eagle–West Boise Fault, Foothills Fault, Middleton–Meridian Fault, Lake Lowell Fault, and Southwest Boundary Fault (Wood, 1996b). The West Boise–Eagle Fault has about 800 feet of displacement near Chinden Boulevard just west of the Boise Fairgrounds and has been recognized by apparent stratigraphic offsets in wells between Dry Creek and Eagle along Highway 55.

Transmissive sands appear to be rare below a depth of 300 to 400 feet northeast of the fault (R. Dittus, pers. comm., 2003)⁴; productive sands are present at deeper depths southeast of the fault. The clay northeast of the fault is considered to be part of the mudstone facies of the Terteling Springs Formation (Burnham and Wood, 1992). The Foothills Fault also is a recognizable feature along the Boise Foothills near Boise (with an offset of greater than 500 feet in the Boise vicinity), although seismic data in the lower Stewart Gulch area (Wood, written comm., 2003) do not show large displacement along the foothills margin. The Middleton–Meridian Fault (actually seen as four faults distributed over a 1.5-mile-wide area in the Chevron seismic line) has an approximate offset of 1,200 feet (Wood, 1996b). The Lake Lowell Fault is mapped between the southern edge of Lake Lowell and Wilder and has a displacement of about 400 feet. Finally, Wood (1996b) describes about 4,000 feet of subsurface structural relief over a 5 mile area southwest of Marsing, although detailed subsurface studies have not been done in this part of the valley.

A thick sequence of sediments overlies the Miocene volcanics (Figure 3-1). These sediments are categorized into two groups: the older and deeper Idaho Group and younger Snake River Group (Table 3-2). Idaho Group sediments represent a thick series of predominantly lacustrine sediments that include the Chalk Hills, Terteling Springs, and Glenns Ferry Formations (Kimmel, 1982; Wood and Clemens, in press). In general, these sediments range to several thousand feet in thickness and grade finer with depth.

The Idaho Group sediments originated from large lakes in the WSRP during the late Miocene and Pliocene epochs. The base of the sedimentary sequence consists of interbedded arkose, mudstone, and volcanic ash, considered part of the Chalk Hills Formation (Kimmel, 1982). Sediments within the bottom 300 feet are generally coarse sand and pebble gravel originating from the Idaho Batholith and other older volcanics, grading upward into tuffaceous muds, clays, and ash beds (Wood and Clemens, in press). The Chalk Hills sediments are faulted and tilted, dipping 4 to 12 degrees basinward, compared to overlying lacustrine sediments that dip less than 4 degrees (Wood and Clemens, in press). In some areas, an unconformity associated (in part) with the occurrence of gravels separates Chalk Hills sediments from overlying sediments (Squires and Wood, 2001; Wood and Clemens, in press).

A transgressive sequence followed the draining of the Chalk Hills Lake, beginning about 5.5 Ma, resulting in a vast lake referred to as Lake Idaho (Wood and Clemens, in press). At its maximum extent, Lake Idaho reached an elevation of about 3,600 feet (msl) in the Boise Foothills. Most of the exposed sediments in the Boise Foothills appear to have been deposited during this transgressive sequence. These sediments,

⁴ The TVHP #1 well (Figure 4-2) was drilled on the northeast side of this fault to a depth of 1,005 feet, with the lower 600 feet in dominantly clay materials (Dittus et al., 1999); see Section 4.

mapped as the Terteling Springs Formation (Burnham and Wood, 1992; Wood and Clemens, in press), include shoreline sand deposits with oolitic sand lenses, small deltaic deposits, and a mudstone facies associated with lacustrine deposition basinward. The Terteling Springs Formation is indicated by a 400-foot-thick section of near-shore sediments marked by oolitic lenses and extends to an elevation of up to 3,200 feet (msl) in the Boise Foothills (Squires and Wood, 2001).

| Time | Lithostratigraphic Units | | Group |
|---------------------------------------|---|--------------------------------------|-------------------|
| Quaternary | Alluvium | | Snake River Group |
| | Gravel of the Boise Terrace | | |
| | Gravel of the Whitney Terrace | | |
| | Gravel of the Sunrise Terrace | | |
| | Basalt of the Gowen Terrace (0.572 ± 0.210 Ma) | | |
| | Gravel of the Gowen Terrace | | |
| | Basalt of the Fivemile Creek (0.974 ± 0.130 Ma) | | |
| | Gravel of the Fivemile Creek | | |
| ~1.8 Ma | | | |
| Pliocene | Tenmile Gravel | | |
| | East Boise alluvial fan deposits | | |
| | Pierce Gulch Sand | Glenns Ferry Formation | |
| ~5.0 Ma | | | |
| Upper Miocene | Terteling Springs Sand Facies Mudstone Facies | Basalt of Aldape Park (9.4 ± 0.6 Ma) | Idaho Group |
| | Boise Foothill Volcanic Assemblage Basalt of Pickett Pin Canyon Volcaniclastic sediments and tuffs and Barber rhyolite ash Lower basalt flow rocks | | |
| | Rhyolite of Quarry View Park (11.8 ± 0.6 Ma) | | |
| | Rhyolite of Table Rock Road | | Idavada Group |
| | Rhyolite of Cottonwood Creek (11.3 ± 0.6 Ma) | | |
| | ~38 Ma | | |
| Mesozoic & Eocene | Granitic Rocks | | Idaho Batholith |
| Adapted from Squires and Wood (2001). | | | |

Table 3-2: Stratigraphic names in the WSRP.

Malde and Powers (1962) suggested that the lowest occurrence of oolitic shoreline sands marks the base of the Glenns Ferry Formation, which covered a large area from the Snake River at Glenns Ferry to Homedale. More recently, Burnham and Wood (1992) and Wood and Clemens (in press) have defined the lower portion of these sediments as the Terteling Springs Formation.

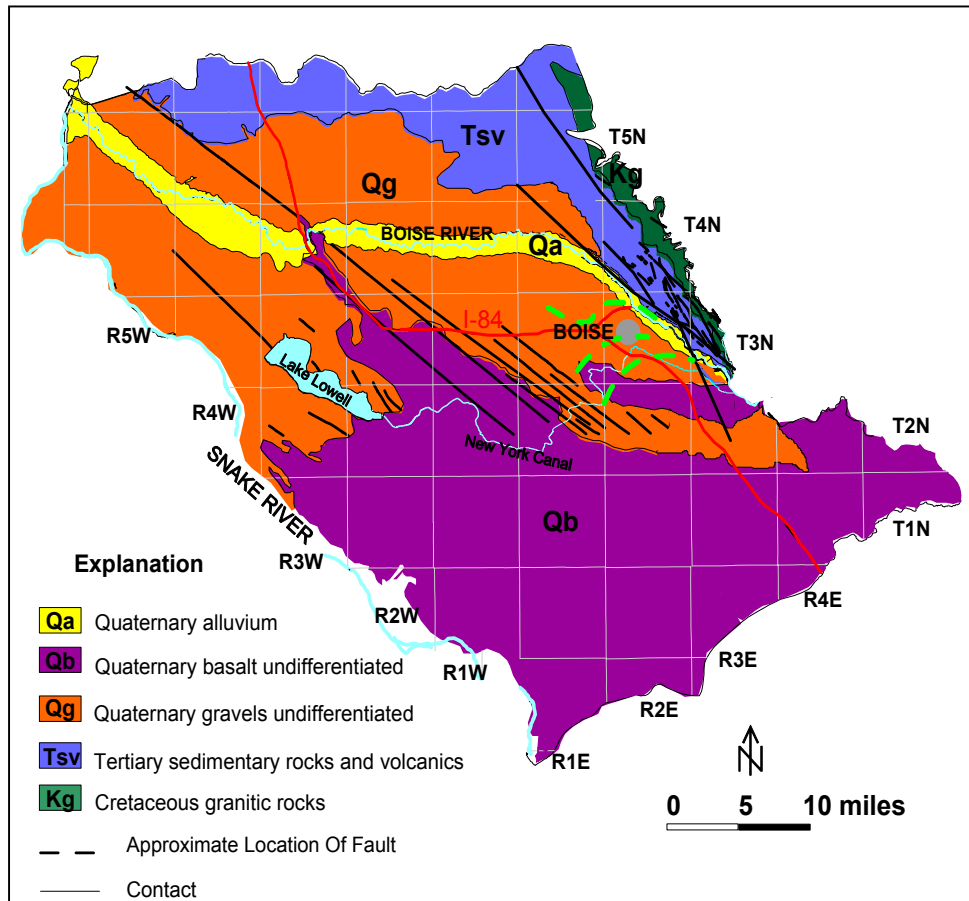
Wood and Clemens (in press) hypothesize that Lake Idaho began to recede about 4 Ma, with the outlet downcutting at a rate of approximately 400 feet per million years. Sediments (originally eroded from uplands and deposited at the basin margins) were further eroded as Lake Idaho water levels dropped. These sediments contributed to filling the receding lake, forming interbedded sand and mud sequences and extensive lacustrine delta systems. Along the Boise Foothills, these sediments are represented by a 200-foot-thick coarse sand unit (Pierce Park Sand) with Gilbert-type foreset bedding. The Pierce Park Sand correlates basinward with the Glens Ferry Formation (Squires et al., 1993; Wood and Clemens, in press), which overlies the Terteling Springs facies. These sediments were spread basinward as the lake system receded from the valley during the Lake Idaho regression (E. Squires, pers. comm., 2003).

Within the general transgressive (Terteling Springs deposits) and regressive (Pierce Park–Glens Ferry deposits) sequence, there is evidence of rising and lowering lake levels. The occurrence of gravel layers in the valley several miles from the basin margins within a general lacustrine sediment sequence is evidence of fluvial deposition, indicating multiple episodes of lowering and raising of lake levels within the transgressive-regressive sequence (Squires and Wood, 2001).

The top of the upper Idaho Group is marked in several parts of the Treasure Valley by a widespread fluvial gravel deposit known as the Tenmile Gravel. Tenmile Gravels contain rounded granitic rocks and felsic porphyries originating from the Idaho Batholith to the north and northeast. The Tenmile Gravels may range up to several hundred feet in thickness along the Tenmile Ridge south of Boise but are less than 50 feet thick in the Nampa-Caldwell area (Wood and Anderson, 1981).

Wood (1994) identified a buried lacustrine delta within the Idaho Group sediments in the Nampa-Caldwell area. The location of the delta in the WSRP suggests that the eastern part of the Boise River basin was delta plain and flood plain at the time of deposition, while the western part was a slack-water (e.g., lake) environment. The delta probably prograded northwestward into a lake basin about 850 feet deep based on high-resolution seismic reflection data and resistivity log interpretations. The delta-plain and delta-front sediments were shown to be mostly fine-grained, well-sorted sand with thin layers of mud (Wood, 1994). The northwest trend of the delta indicates a sediment source to the southeast, such as where the Snake River flows today (Wood, 1994).

The uppermost sediments and basalt covering much of the project area (Figure 3-3) belong to the Pleistocene-age Snake River Group (Othberg and Stanford, 1992). The Snake River Group sediments, consisting primarily of coarse-grained sand and gravels, include Quaternary alluvium, a series of Quaternary terrace gravels and sands, and Pleistocene basalt flows (Wood and Anderson, 1981). The basalt flows cover primarily the southern portion of the project area (Figure 3-3).



From Othberg and Stanford (1992)

Figure 3-3: Surficial geology map.

Several stratigraphic cross-sections were drawn by Beukelman (1997a; 1997b; 1997c; 1997d), Wood (1996a), and Squires and Wood (2001) as part of the TVHP. The cross-sections were based on drillers' logs, geophysical logs, geologic outcrops, and seismic data. Surficial deposits were noted as modern flood plain deposits, Bonneville Flood slackwater fine sediments, Pleistocene gravels, and older tertiary-age sediments.

A transition from brown to underlying blue or gray sediments is noted in many drillers' reports and in the various cross-sections. The color transition is observed throughout central and western portions of the valley (Beukelman, 1997b; Beukelman, 1997c; Beukelman, 1997d; Squires and Wood, 2001), as far west as Parma and Ontario and as far east as Boise (Beukelman, 1997a; Squires et al., 1992). The blue-gray sediments are not found in the upper 1,100 feet of alluvial fan sediments east of Boise (Squires et al., 1992). The blue-gray sediments generally consist of clay and/or silt but also may include interbedded sand or even pea gravels. The upper surface of these sediments, frequently referred to as the "blue clay," can be found at depths ranging from tens of feet to over 800 feet below ground surface.

The origin of the contact between brown and blue-gray sediments is not well understood. The bluish color probably reflects chemically-reducing conditions associated with an oxygen-poor environment. Some of the color may be associated with depositional environment, especially when lacustrine sediments become buried under new deposition. Some of the color may be associated with post depositional conditions, as evidenced by gravels and coarse sands within bluish horizons. Local elevation variations in bluish sediments may reflect erosion of the blue-gray sediments, exposure to oxygen, and/or structural movement.

The use of color changes to identify depositional environments can be misleading. Despite the presence of blue-gray sediments throughout much of the valley, the color-change contact does not appear to represent individual areally-extensive strata. Bluish-colored sediments may change color if exposed to oxygen (or oxygen-rich ground water). Thus, the transition from brown to blue-gray sediments probably reflects a combination of deposition and post-depositional conditions and therefore, is not necessarily indicative of current ground water flow conditions.

Multiple layers of clay are found within the Idaho Group sediments. These clay layers, in aggregate, form aquitards separating shallow aquifers from deeper zones. Although the clay layers are often of substantial thickness, individual clay units are not necessarily continuous over large portions of the project area.

3.4. Aquifer Description

Treasure Valley aquifers also have been described in terms of subdivisions based on general material properties and location within the valley (Squires et al., 1992). This section provides a general description of primary aquifers on the basis of sedimentary characteristics.

The sediments included in these subdivisions may span multiple formations or geologic groups (Section 3.3). For instance, some of the East Boise alluvial fan sediments may be contemporaneous to the upper Chalk Hills Formation (Wood and Clemens, in press); lacustrine sediments in the central portion of the valley may belong to the Chalk Hills, Terteling Springs, and/or Glens Ferry Formations. Distinctions between the specific geologic formations may not necessarily indicate differences in ground water flow characteristics. For instance, lacustrine sediments in the central portion of the valley may have similar ground water flow characteristics, regardless of whether they belong to the Chalk Hills Formation or the Terteling Springs mud facies.

Thus, the Treasure Valley aquifer system consists of a series of sedimentary aquifers within the Idaho Group and Snake River Group sediments. Squires et al. (1992) interpreted five subdivisions (Figure 3-4) within the Idaho Group sediments in the Boise area using geophysical logs, well logs, and aquifer tests. The five subdivisions

are the (1) Boise Fan Sediments, (2) Fan-to-Lake Transition Sediments, (3) Central Boise Lacustrine Sediments, (4) Deep Lacustrine Sands and Alluvial Lake Margin Sands of west Boise, and (5) Lake Margin Sands of northeast Boise.

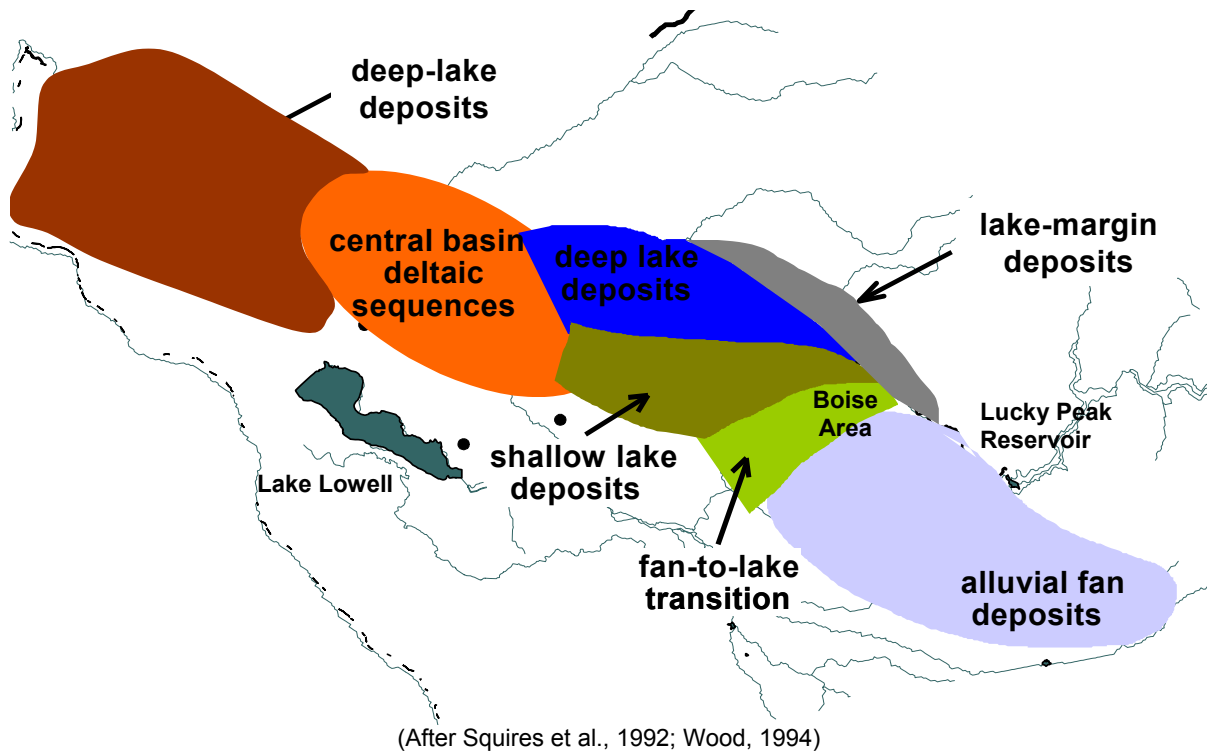


Figure 3-4: Subdivisions of Idaho Group sediments.

The Boise Fan (Squires et al., 1992) covers a large, highly heterogeneous deposit of gravels, sands, and silts, beginning near Lucky Peak Dam and extending about 6 miles to the west-northwest. Predominantly silty sands, the Boise Fan sediments also contain numerous gravel lenses and a few silt lenses. Fan-to-Lake Transition sediments were described as clays and sands of alternating brown and blue colors, indicating interfingered oxidized and reduced materials, respectively. Squires et al. (1992) described the Central Boise Lacustrine sediments as sand, silt, and clay units bearing lacustrine features (e.g., oolites, fine grain sizes). Sediments underlying an area of west Boise were described as deep lacustrine sands and alluvial lake margin sands. Wells in this area encountered 500 feet of nearly horizontal medium- to coarse-grained sands interbedded with silts, sands, and clays, underlain by 500 to 1,000 feet of fine-grained sand layers within thick layers of clay and silt. Seismic data indicated a westerly dip in the lower section of 3 to 7 degrees and 2 to 3 degrees in the upper materials. Finally, Squires et al. (1992) interpreted lake margin sediments containing sands, gravels, and occasional silty zones in the area underlying northeast Boise. The sediments were interpreted as lake margin sediments on the basis of the well-sorted

nature of the sand layers, interbedded fluvial deposits, and their stratigraphic location with respect to adjacent geologic outcroppings of the Boise Foothills.

Wood and Anderson (1981) first suggested that the Glenns Ferry sediments rest on a geological unconformity within the Idaho Group. The lower sediments dip basinward approximately 4 to 7 degrees. The buried unconformity lies 350 to 400 feet beneath central and east Boise and 400 to 500 feet deep in west Boise (Squires et al., 1992). Additional fluvial deposits have been noted within lacustrine sequences (Squires and Wood, 2001), indicating multiple episodes of rising and lowering lake levels.

Sequences of interbedded sand, silt, and clay, such as the upper portion of the Glenns Ferry Formation of the upper Idaho Group in the Nampa–Caldwell area, are the major water-producing aquifers in a large part of Canyon County (Anderson and Wood, 1981).

3.5. Water Chemistry

Despite regional geologic complexity, geochemical analyses conducted as part of the TVHP (Hutchings and Petrich, 2002a) show predictable relationships between ground water chemistry and the unique depositional environments of the principal aquifers. The analyses indicated (1) a strong relationship between concentrations of dissolved constituents and depositionally-defined aquifer units, (2) apparent geochemical evolution along the valley axis, and (3) a general east-to-west increase of ground water residence times.

Geochemical evolution of Treasure Valley ground water appears to be influenced by a solution of both carbonate and silicate minerals. Ground water near the northeastern basin margin has experienced little chemical interaction with aquifer minerals; ground water beyond the northeastern basin margin has experienced substantial interaction with aquifer minerals.

Concentrations of major ions and other dissolved constituents vary consistently with depth among aquifer zones. Specific conductance (and by inference, concentrations of total dissolved solids) is often greater in shallow alluvial aquifers than in some deeper zones. This finding indicates that water in these deeper zones did not enter the ground water regime through the carbon-rich sediments found in Treasure Valley soils.

Residence times of Treasure Valley ground water generally increase with depth and with distance along a regional east-to-west trending flow path (Hutchings and Petrich, 2002a; Hutchings and Petrich, 2002b). Residence times range from years to hundreds of years in shallow aquifers and thousands to tens of thousands of years in deeper, regional aquifers.

Residence times in the shallow system are bracketed, in part, based on tritium concentrations remaining from nuclear testing during the 1950s and 1960s. Tritium is present in shallow aquifers, such as those underlying the New York Canal (Hutchings and Petrich, 2002b). Tritium is virtually non-existent in deeper, regional ground waters, except where well construction has allowed inter-aquifer mixing. This finding indicates that ground water in deeper aquifers entered the flow regime prior to atmospheric nuclear testing during the 1950s and 1960s.

The youngest waters in the deeper, regional flow system entered the subsurface a few thousand years ago and are found along the eastern and northeastern boundary of the basin, adjacent to the Boise Foothills. The oldest waters in the regional flow system entered the subsurface between 20,000 and 40,000 years ago and are now found in the western reaches of the basin near the Snake River. Ground water in the deep deltaic aquifers beneath Boise entered the subsurface between 10,000 and 20,000 years ago.

From the ground water chemistry analyses it becomes clear that contemporary seepage from surface water in the central portion of the valley and/or irrigation water is not the primary source of recharge for most deeper, regional aquifers. Fractured granite aquifers of the Idaho Batholith, surface water in the far eastern portion of the valley, and tributary sedimentary aquifers (underflow) are the most likely sources of recharge to the regional flow system. A conceptual model consisting of (1) recharge in alluvial sediments in southeast Boise and at the base of the mountain front north of Boise, (2) movement of ground water from the recharge areas into the deeper Boise area fluvio-lacustrine aquifers, and (3) movement of ground water from the Boise area aquifers into regional deep-lake aquifers of Nampa and Caldwell is consistent with these chemistry data.

3.6. Ground Water Flow Systems

Ground water for municipal, industrial, rural domestic, and irrigation uses in the Treasure Valley is drawn from Snake River Group and Idaho Group aquifers. Many domestic wells draw water from shallow aquifers, such as those in the Snake River Group deposits. Larger production wells (for municipal and agricultural uses) generally draw water from the deeper Idaho Group sediments. Flow systems providing water to these wells can be markedly different. Distinguishing between shallow and regional ground water flow systems is important for understanding ground water flow characteristics and managing ground water resources.

Local flow systems in shallow aquifers are recharged by infiltration associated with precipitation, irrigation, and channel (e.g., streams or canals) losses. These local flow systems often discharge to local drains or streams. The time from recharge to discharge in shallow flow systems probably ranges from days to hundreds of years. In contrast, regional ground water flow systems extend much deeper than local flow

systems. The Treasure Valley regional flow system begins with downward movement in coarse-grained alluvial fan sediments in the eastern portion of the valley. Some water also enters the regional flow system as underflow from the Boise Foothills in the northeastern part of the valley. The regional flow system is thought to discharge primarily to the Boise and Snake Rivers in the western and southwestern parts of the valley. Residence times (Section 3.5) for some of the water in the regional flow system were estimated to be greater than 20,000 years (Hutchings and Petrich, 2002a).

3.7. Hydraulic Properties⁵

Numerous hydraulic parameter value estimates have been made for Treasure Valley aquifers. Most parameter estimates have been made on the basis of single-well tests. Water production wells are frequently pumped to estimate well yield and specific capacity. Very approximate estimates of transmissivity can sometimes be obtained with specific capacity data (Driscoll, 1986). Permeability estimates have also been made under laboratory conditions at some locations in conjunction with landfill construction (e.g., Seaman's Gulch, Clay Butte, and Pickles Butte). In addition, a few large-scale, multiple-well tests have been conducted in the Treasure Valley.

Specific capacity data obtained from well drillers' reports were used to develop plots of aquifer transmissivity values. These plots, however, should only be viewed on a qualitative basis because of a high degree of uncertainty associated with these data. The uncertainty is high because of variability in test duration, pumping rate, well efficiency, differences in well construction (e.g., different lengths of open intervals), degree of aquifer penetration, and measurement accuracy.

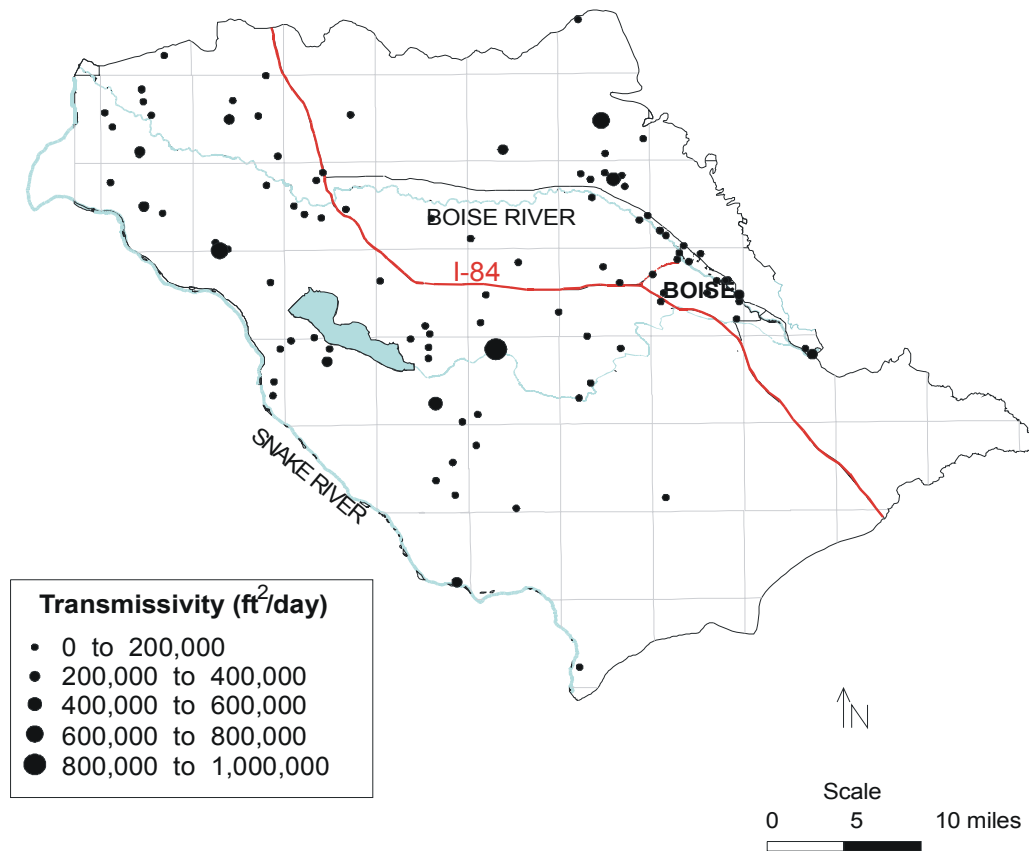
Well pump test data for 197 wells within the valley formed the basis for the specific capacity plots. The specific capacity data were compiled from drillers' report information contained in the IDWR Well_Log database⁶. Specific capacity data were divided into two depth zone categories: a zone from 0 to 300 feet below ground surface and a zone greater than 300 feet depth below ground surface. The data were divided into zones on the basis of open interval depths for wells as listed in the well drillers' reports. Aquifer thickness values were (1) entered in Well_Log on the basis of lithology indicated in the drillers' log or (2) assumed to be the thickness between the water level in the well and the well bottom.

A transmissivity map for the 0 to 300-foot zone (Figure 3-5) suggests that the bulk of transmissivity values calculated for shallow aquifers in the Treasure Valley are less than 200,000 ft²/day. Isolated areas with comparatively high transmissivity values

⁵ Data for this section were compiled and plotted by Rick Carlson, formerly with IWRRI.

⁶ The Well_Log data base is being developed and maintained by IDWR with data from well drillers' reports.

(> 600,000 ft²/day) were noted northeast and southeast of Lake Lowell and just north of the Boise River near Eagle. These high transmissivity values correlate with areas underlain by both gravel and basalt.

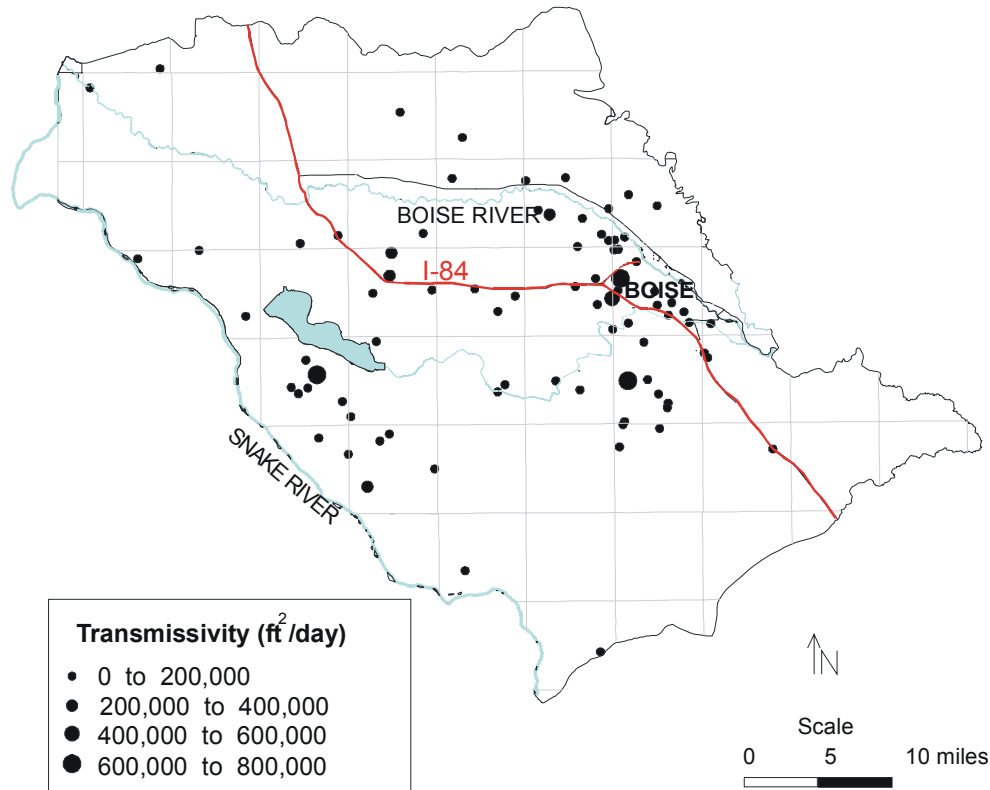


(Based on specific capacity data for wells with screened interval beginning at less than 300 feet below land surface)

Figure 3-5: Transmissivity estimates for wells completed between 0 and 300 feet below ground surface.

The map for the greater-than-300-foot zone (Figure 3-6) suggests that transmissivity values are comparatively greater at depth. The majority of calculated transmissivity values for deep aquifers across the Treasure Valley ranged between 200,000 and 400,000 ft²/day. Isolated areas of higher transmissivity (600,000 to 800,000 ft²/day) were apparent beneath west Boise, about 5 miles south of Boise, and 2 miles south of

Lake Lowell. These areas of high transmissivity are believed to correlate with deep aquifers containing zones of coarser-grained sediments⁷.

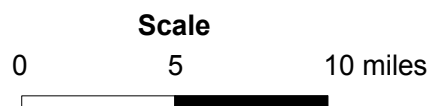
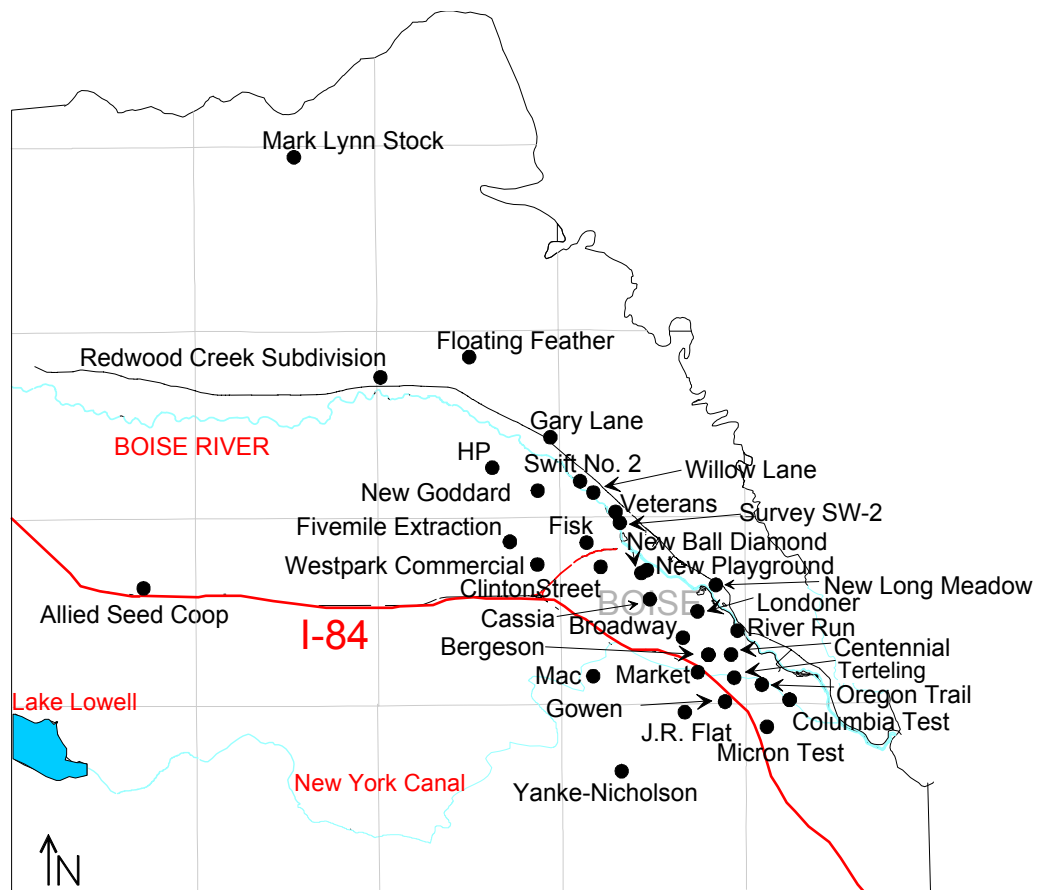


(Based on specific capacity data for wells with screened interval beginning at greater than 300 feet below land surface)

Figure 3-6: Transmissivity estimates for wells completed below 300 feet below ground surface.

In addition, aquifer parameter estimates were compiled from various single- and multi-well aquifer test results. The source of these data includes various reports prepared by public agencies and private consultants. Test locations are shown in Figure 3-7. A table of values is provided in Appendix B. Estimated hydraulic conductivity values ranged from 2.49×10^3 to 1.0×10^5 ft/day.

⁷ These conclusions may be skewed because (1) low-producing wells may not have been completed, and therefore are not included here, and (2) most of the wells used for aquifer tests are designed for production, and therefore are completed in the most productive zones.



- Pumping well location

Figure 3-7: Locations of selected single and multiple well aquifer tests.

3.8. Geothermal System

The “cold water” aquifer system contained in the Snake River and Idaho Groups is underlain by a low-temperature geothermal⁸ aquifer system. Temperatures of the low-temperature geothermal water range from 85° to 175°F along the Boise Front⁹ (Petrich, 2003). The geothermal system provides heating for numerous Boise buildings and residences. In some areas, apparent upwelling from the geothermal system appears to influence potable non-geothermal ground water chemistry, evidenced by elevated concentrations of fluoride and other constituents.

The geothermal water along the Boise Front is associated with the Miocene basalts and underlying rhyolite (Wood and Burnham, 1987, p.121). Geothermal water rises from fractured rhyolite along the northwest-trending fault zone that marks the northeastern boundary of the Snake River Plain. A conceptual geothermal water circulation loop was described by Wood and Burnham (Wood and Burnham, 1987, p.121; Wood and Low, 1988, p.32-33), in which meteoric water from surrounding highlands circulates through deep fractures in the Idaho Batholith. The extent of the rhyolite aquifer into the valley is unknown. The rhyolite is present along the northern and southern margins of the WSRP, but no wells in the central part of the valley have extended into rhyolite (S. Wood, pers. comm., 1996). Potentiometric surface maps based on the 2002 mass measurements in geothermal wells suggest a westerly or southwesterly hydraulic gradient in the Boise Front area (Petrich, 2003).

It is important to differentiate between geothermal water and water that is greater than 85°F found in deeper Idaho Group sediments. Geothermal water from the rhyolite aquifers generally contains greater concentrations of sodium, bicarbonate, sulfate, chloride, fluoride, silica, arsenic, boron, and lithium than the overlying non-geothermal systems (Wood and Low, 1988, p.32). Upper aquifers, even if containing warm water, generally have higher concentrations of calcium and magnesium than the geothermal system. Squires and Wood (1989) note that ground water taken from Tenmile Ridge wells exhibits warm temperatures (70° to 88° F), but does not contain the high fluoride content associated with geothermal water on the north side of the Boise Valley. This lack of chemical similarity suggests that, with the exception of the fault zone area along the Boise Foothills, (1) the hydraulic connection between aquifers in the Idaho Group sediments and the geothermal rhyolite aquifers is limited, or (2) the volume of cold water entering the Idaho Group aquifers is much larger than the volume of geothermal water entering the Idaho Group aquifers.

⁸ “Low-temperature geothermal water” is defined by Idaho Code (I.C. § 42-233) as ground water with a temperature greater than 85°F but less than 212°F.

⁹ Boise Front describes the portion of the Idaho Batholith that forms the northeastern boundary of the lower Boise River basin.

Limited hydraulic interaction between the geothermal rhyolite aquifers and the non-geothermal aquifers in the Idaho Group is attributed to low permeabilities of the materials separating the aquifer zones. Miocene basalt and tuffaceous sediments overlying the rhyolite geothermal aquifer have low permeability because of clay alteration and minerals filling the fractures (Squires and Wood, 1989, S. Wood, pers. comm., 1997)S. Wood, pers. comm., 1997). Low permeability mudstone (which may be more than several hundred feet thick) at the base of the Idaho Group sediments further restricts the vertical permeability and hydraulic connection. However, elevated fluoride and temperature in some non-geothermal aquifers (along the Boise Front and in an area southwest of Nampa) indicates that some upwelling does occur.

4. DEDICATED TVHP MONITORING WELLS

Four multi-completion monitoring wells were constructed as a part of the TVHP (Figure 4-1). The purpose of the wells was to provide water level and chemistry data at different depths and locations within the aquifer system. A summary of screened intervals for the multiple-completion wells is provided in Table 4-1. Appendix A provides construction details and stratigraphic data for each of the wells. Geophysical data for wells TVHP #1, TVHP #2, and TVHP #4 are also provided in Appendix A.

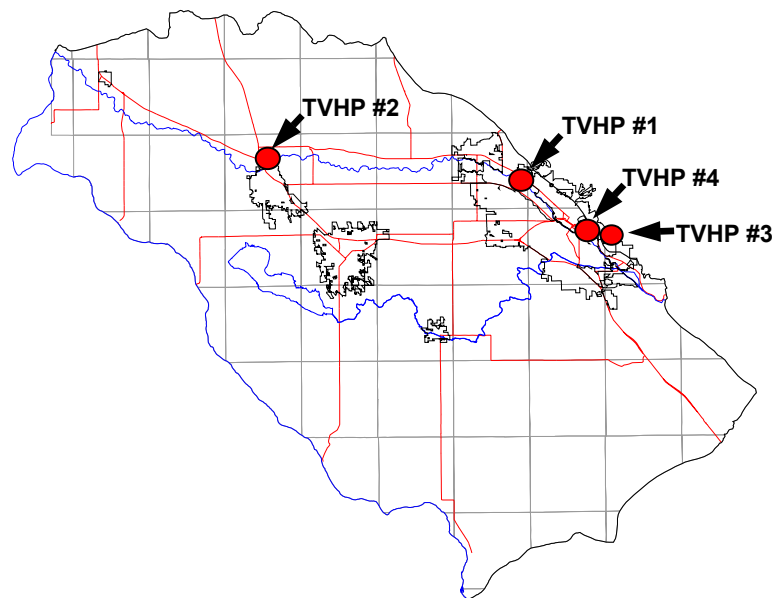


Figure 4-1: TVHP monitoring well locations.

Monitoring well TVHP #1 was drilled and constructed by United Water Idaho, Inc. (UWID) during December 1996. The well was drilled as a deep exploratory test well, and was originally drilled to evaluate potential aquifer units that might be developed for municipal water supply (Dittus and Squires, 1998). The borehole was drilled to a depth of 1,050 feet below ground surface but was subsequently backfilled to 357 feet. Four piezometers were then installed, with completion depths ranging from 170 to 340 feet. Water quality analyses from these piezometers showed the aquifers were not suitable for use as a municipal supply. UWI donated the well to the TVHP for use as a long-term monitoring well, and IDWR purchased an access easement to the well from a private landowner. Water levels (Figure 4-2) indicate an upward hydraulic gradient and apparent influences of nearby withdrawals and/or recharge.

| Well Name | Piezometer | Screened Intervals – Depth below ground surface (feet) |
|----------------------------|------------|--|
| TVHP #1 (Near Eagle) | Zone 1 | 300-310, 330-340 |
| | Zone 2 | 270-290 |
| | Zone 3 | 210-220, 240-250 |
| | Zone 4 | 130-140, 150-170 |
| TVHP #2 (Caldwell) | Zone 1 | 912-922, 932-942 |
| | Zone 2 | 679-689, 699-709 |
| | Zone 3 | 516-536 |
| | Zone 4 | 376-396 |
| | Zone 5 | 238-248 |
| | Zone 6 | 182-192 |
| | Zone 7 | 142-152 |
| | Zone 8 | 110-120 |
| TVHP #3 (Quarry View Park) | 1 | 600-700 |
| | 2 | 813-848 |
| TVHP #4 (Municipal Park) | 1 | 35-55 |
| | 2 | 190-210 |
| | 3 | 300-320 |
| | 4 | 450-470 |
| | 5 | 710-730 |

Table 4-1: Construction details for TVHP monitoring wells.

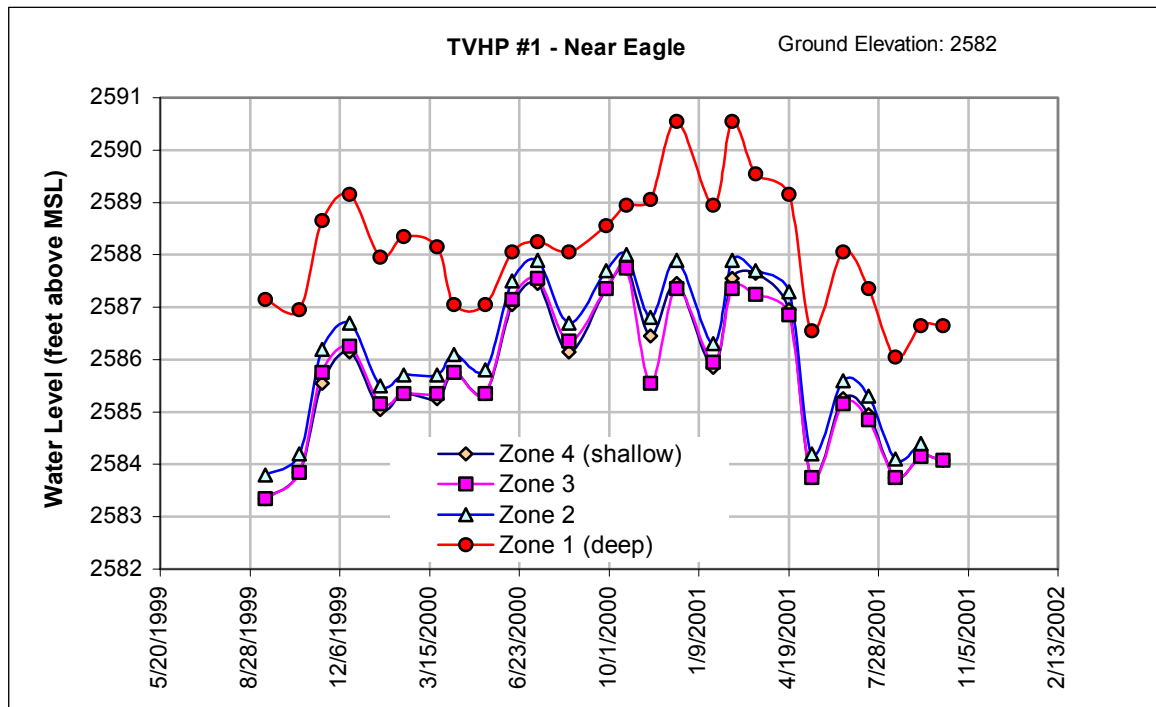


Figure 4-2: Hydrograph for TVHP #1.

Monitoring well TVHP #2 was constructed within the city of Caldwell during 1999. As with TVHP #1, this borehole was drilled for the purpose of seeking an additional source of municipal water. The city of Caldwell and IDWR agreed to share the cost of completing the borehole as a multi-level monitoring well (with in-kind technical support by UWID). Completed with eight piezometers, this well nest has completion depths ranging from 120 to 942 feet. Hydraulic head measurements (Figure 4-3) indicated a strong upward gradient between 725 feet and shallower zones and a moderate upward gradient from 550 feet to shallower zones. The vertical head differences ranged from 35 to 41 feet (upward gradient) between 11/30/99 and 6/20/01, with an average difference of 37 feet. The four uppermost completions (between 122 and 270 feet depth) are relatively consistent, indicating the possibility of a high degree of hydraulic connection between these zones. There appears to be a slight downward gradient from 725 to 1,010 feet. All completions above and including 550 feet show influences of seasonal withdrawals (i.e., summer declines).

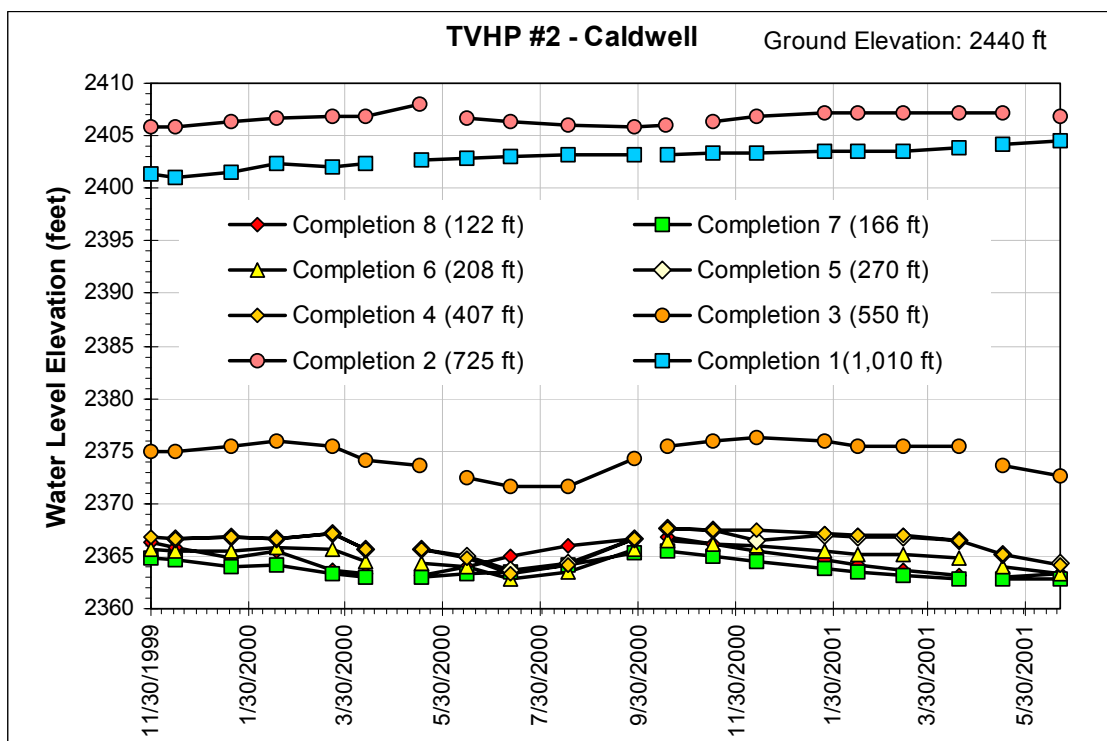


Figure 4-3: Hydrograph for TVHP #2.

Monitoring well TVHP #3 was completed in June 2001. Originally drilled in 1983, the well was used to irrigate the nearby Quarry View Park. The deepest completion produced geothermal water. Production ceased in 1988 to reduce geothermal water use (Scanlan, 2001). The well was then converted to a dual-level monitoring well by the city of Boise and IDWR as part of the TVHP. Water levels in the Quarry View well

were virtually identical between September 2001 and October 2003 (Figure 4-4), indicating close hydraulic connection between screened intervals. Decreased summer water levels indicate nearby irrigation influences.

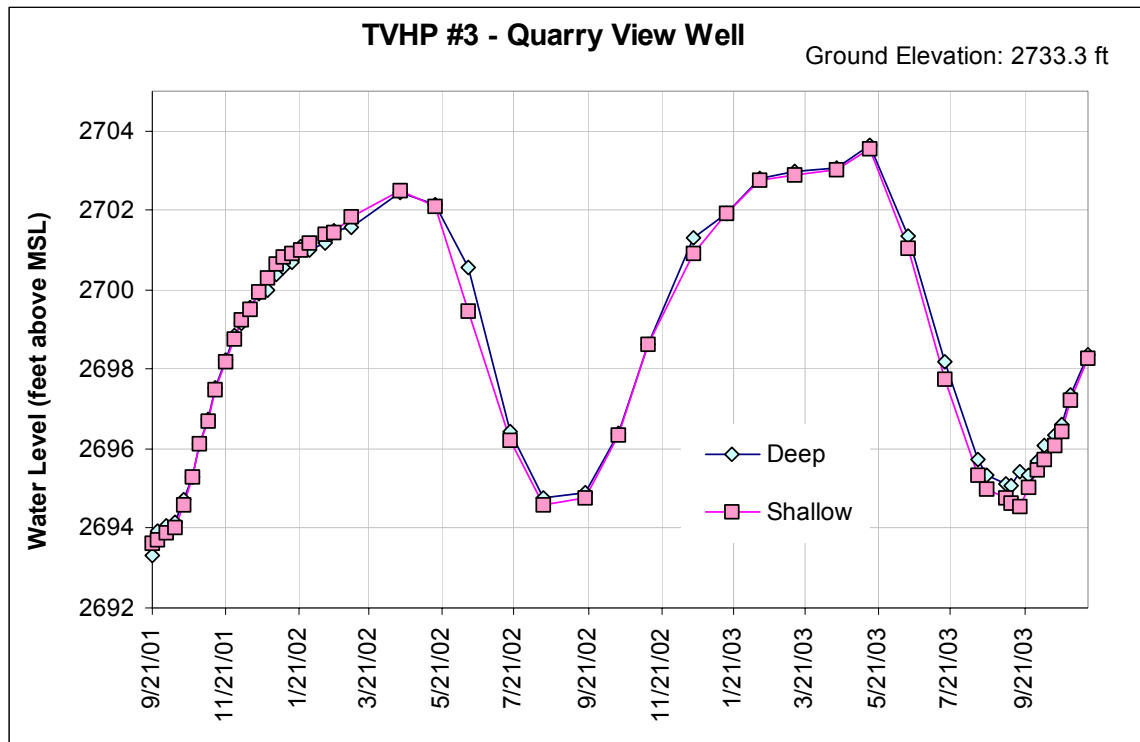
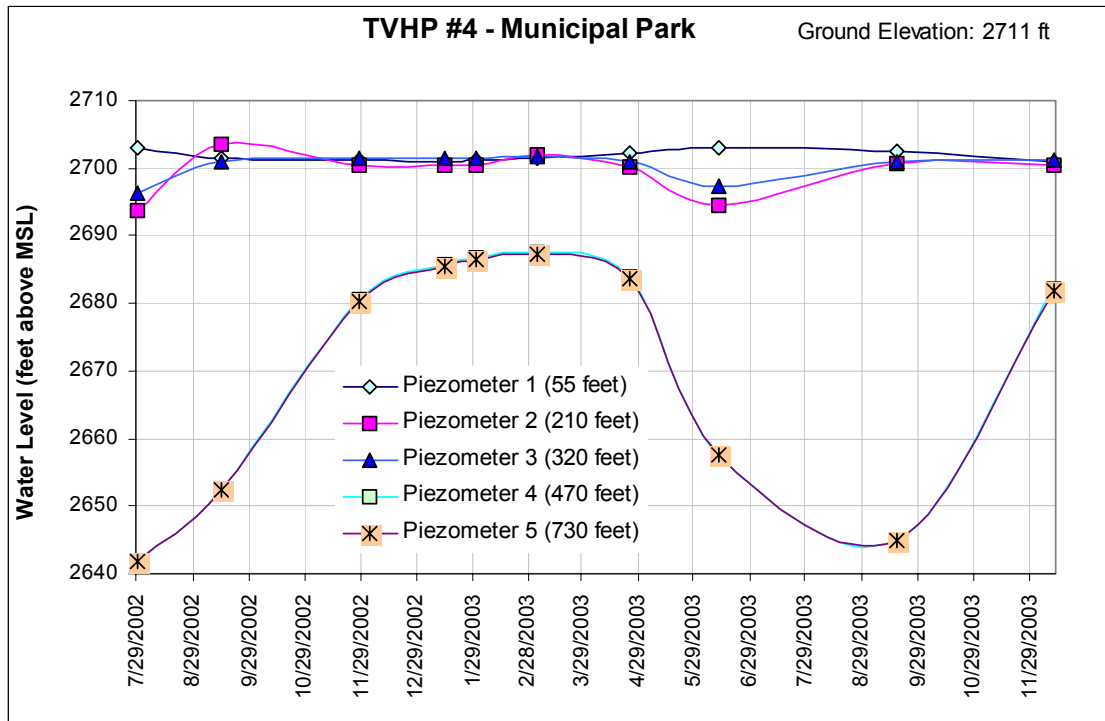


Figure 4-4: Hydrograph for TVHP #3.

Monitoring Well TVHP #4 was completed in July 2002. Located in the southeast corner of Boise's Municipal Park, this well was constructed as a multi-completion monitoring well in an area of downward hydraulic gradients. Initially drilled to a depth of 800 feet, this well includes five piezometers ranging in depth from 55 to 730 feet. Water levels in this well (Figure 4-5) indicate similar water levels in the upper three completions and lower water levels in the lowest two completions, confirming a downward hydraulic gradient. Water level differences in the Boise Municipal Park monitoring well ranged from about 15 to 61 feet between 7/29/02 and 4/24/03 (downward gradient). Decreased water levels in the deepest completions during summer months reflect nearby municipal and irrigation withdrawals. Several municipal wells are located near monitoring well TVHP #4, with peak usage of these wells occurring during the summer months; some are not used at all during the winter and spring months (R. Dittus, pers. comm., 2003).



Piezometers 4 and 5 indicate virtually the same water level elevations.

Figure 4-5: Hydrograph for TVHP #4.

5. GROUND WATER LEVELS

5.1. Introduction

Water level measurements conducted as part of the TVHP include seven mass ground water level measurements in approximately 300 wells and monthly ground water level measurements in approximately 70 wells. This section describes and presents results from these measurements.

5.2. Mass Ground Water Level Measurements

A “mass measurement” consists of a series of ground water level measurements taken within a short period of time (in this case, one to two weeks). The purpose of a mass ground water level measurement is to define a *potentiometric surface* at a point in time. A potentiometric surface represents the levels to which water rises in wells over a given area. The water table is the potentiometric surface of an unconfined aquifer. There may be more than one potentiometric surface for a given area if the hydraulic head¹⁰ varies significantly with depth. A contour map describing a potentiometric surface is used for evaluating ground water flow directions and hydraulic gradients.

Mass ground water level measurements were conducted as part of the TVHP in the spring and fall of 1996, 1998, 2000, and fall 2001. Water levels throughout the Treasure Valley were measured within a one- to two-week time period during each mass measurement. This section describes the selection of mass measurement wells and presents potentiometric surface maps created with the mass measurement data.

The U.S. Geological Survey (USGS) selected wells for the mass measurements and performed the water level measurements. The USGS selected wells by:

1. Identifying candidate wells from the USGS Ground Water Site Inventory (GWSI) database.
2. Categorizing candidate wells on the basis of open intervals in shallow, deep, and geothermal aquifers.
3. Choosing wells that are spatially and vertically distributed throughout the Treasure Valley (where possible) in the non-geothermal aquifers. The shallow aquifer was targeted for about 60% of the measurements.

The numbers of wells included in the mass measurements are shown in Table 5-1. Additional wells were included for use in developing potentiometric surfaces if they were measured at approximately the same time as

¹⁰ Hydraulic head consists of elevation head and pressure head; the hydraulic head for a given aquifer zone is indicated by the water level in a well screened in the aquifer zone.

the mass measurement. The open interval of each well was categorized by depth on the basis of ground water flow model layers (see Petrich, 2004a, for more information)

Table 5-2). Wells with screen openings in layers 3 and 4 are grouped together in the subsequent potentiometric surface maps because of the relatively small number of wells in each zone.

| Mass Measurement | Number of Wells | Measuring Entity |
|------------------|-----------------|-------------------|
| Spring 1996 | 343 | USGS |
| Fall 1996 | 342 | USGS |
| Spring 1998 | 383 | USGS |
| Fall 1998 | 372 | USGS |
| Spring 2000 | 392 | USGS |
| Fall 2000 | 390 | Kleinfelder, Inc. |
| Fall 2001 | 341 | Kleinfelder, Inc. |

Table 5-1: Numbers of wells measured during each of four mass water level measurements.

| Layer | Thickness (feet) | Depth below Potentiometric Surface (feet) |
|---------|------------------|---|
| Layer 1 | 200 | 0-200 |
| Layer 2 | 200 | 200-400 |
| Layer 3 | 400 | 400-800 |
| Layer 4 | 400 | 800-1200 |

(see Petrich, 2004a, for more information)

Table 5-2: Model layer thicknesses.

Well construction details for the mass measurement wells are provided in Appendix D. The information includes:

1. Well codes indicating whether the well was used only as a mass measurement well or also for monthly well measurements
2. Well use (e.g., municipal, domestic, irrigation, industrial, etc.)
3. Upper and lower screen opening elevations (provides a basis for associating water level data with model layers)
4. Total screen length
5. Aquifer penetration depth (depth of standing water in well)

The aquifer penetration depth is provided because even deep wells may only penetrate a short distance into an aquifer. Lack of well depth data indicates that there is no drillers' log available for the well¹¹.

5.2.1. Data Collection

Water level measurements during 1996-2000 were collected by the USGS; Kleinfelder, Inc., collected water levels in fall 2000 and 2001. Pre-measurement tasks included contacting owners for permission to measure wells, preparing field maps, forms, and other necessary equipment, and assembling a field crew. Measurement tasks included visiting well sites, measuring and recording water levels, and updating well inventory information. Post-measurement tasks included entering measurement and inventory data into USGS GWSI database and publishing measurements in USGS annual water data reports.

5.2.2. Potentiometric Surface Maps

Potentiometric surface contour maps based on kriged interpolations for the mass measurements conducted in spring and fall of 1996, 1998, and 2000, and fall 2001 (for shallow, intermediate, and deep zones) are provided in Appendix E. Monitoring wells with open intervals in the layer of interest are shown with gray dots. Three examples of potentiometric surface plots are shown in Figure 5-1 through Figure 5-3. The following sections describe some of these figures.

There are several observations that can be made from the potentiometric surface maps presented in the previous sections and in Appendix E. In general, contour maps drawn from mass measurement data indicate ground water flow from the eastern part of the valley toward the west, except for the area south of Boise, where ground water flow is to the south or southwest. Potentiometric surface contours in the southeastern portion and parts of the northern part of the study area are uncertain because of the paucity of data in these areas.

¹¹ A few wells were used for water level measurements despite the lack of well construction or lithologic information because they were located in areas of few or no other observation alternatives.

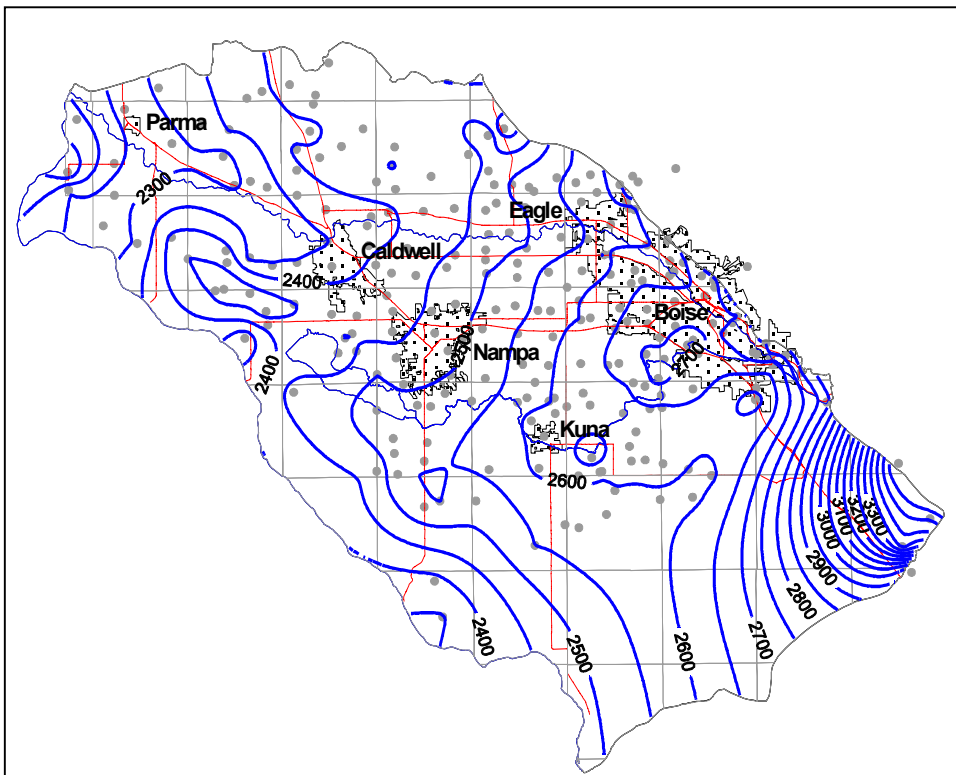


Figure 5-1: Potentiometric surface, spring 1996, shallow zone (240 wells).

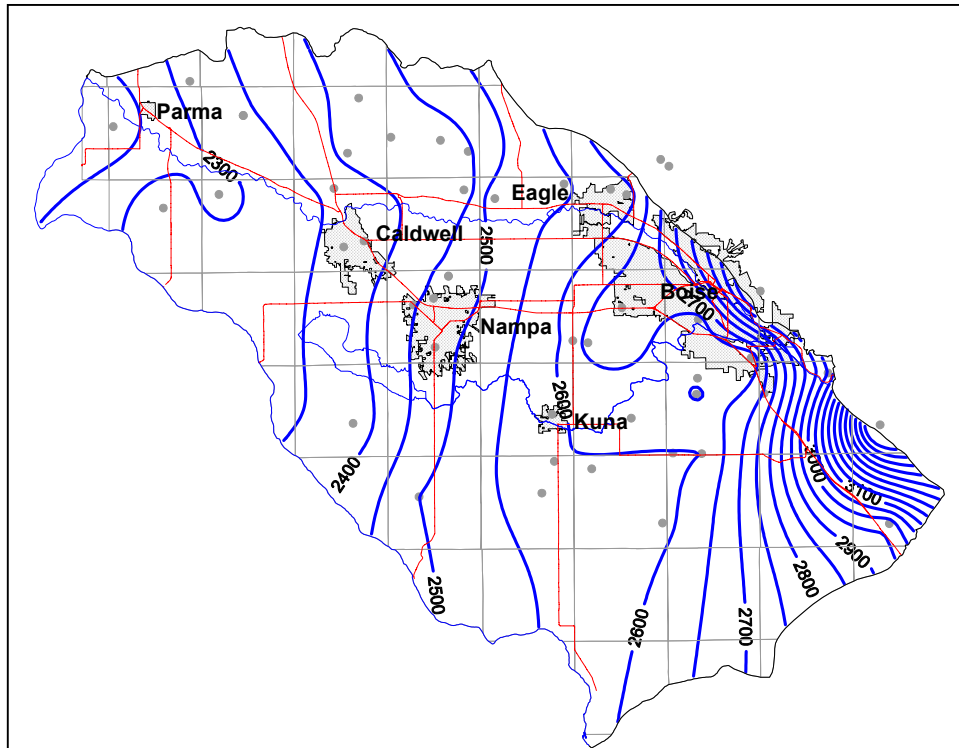


Figure 5-2: Potentiometric surface, spring 1996, intermediate zone (49 wells).

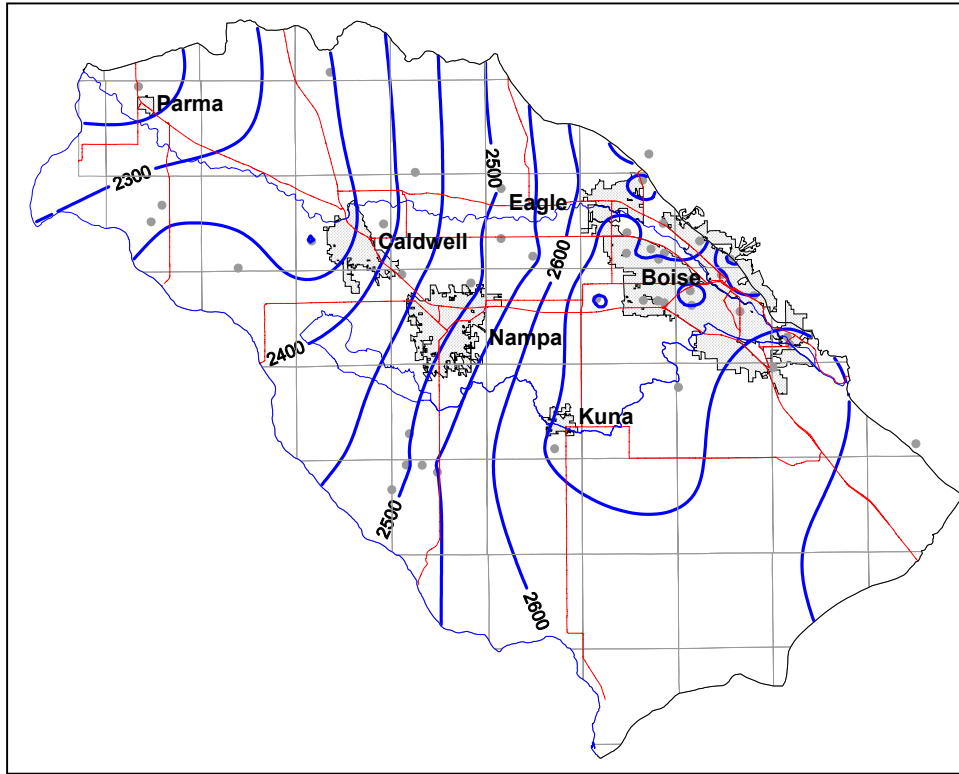


Figure 5-3: Potentiometric surface, spring 1996, deep zone (45 wells).

Additional specific observations include the following:

1. Potentiometric contours from deeper aquifer zones indicate ground water movement in a westerly direction.
2. Potentiometric surface contours in maps indicate ground water mounding in the vicinity of the New York and Mora Canals, presumably from canal leakage (Berenbrock, 1999; Carlson and Petrich, 1998) and infiltration from irrigated fields.
3. Ground water mounding appears in the area northwest of Lake Lowell.
4. Ground water mounding appears to form a ground water divide between the Boise and Snake Rivers along the New York and Mora Canals, and extending northwest from Lake Lowell. North of these canals ground water flows toward the Boise River, south of these canals hydraulic gradients indicate ground water flow toward the Snake River. The effects of ground water mounding underneath the New York Canal are evident in both the potentiometric surfaces based on shallow and deeper wells, although water from the New York Canal is not reaching these lower zones (Hutchings and Petrich, 2002b).
5. The potentiometric surface maps indicate ground water movement from the Boise Foothills in a west-southwest direction toward the Boise River.

5.2.3. Seasonal Water Level Changes

Seasonal water level changes occur in the Treasure Valley in response to ground water withdrawals, surface irrigation, and canal leakage. Figure 5-4 illustrates seasonal water level changes between spring and fall 1996. The map was prepared by subtracting fall potentiometric surface in the shallow zone from that of the spring potentiometric surface in the shallow zone. The map indicates general ground water level increases (in the uppermost aquifer zone) in the central portion of the valley south of the Boise River. These rises were attributed to infiltration associated with summer irrigation. Ground water declines are indicated in the southwestern portion of the valley, though these declines appear to be associated with select wells and may not necessarily reflect regional trends.

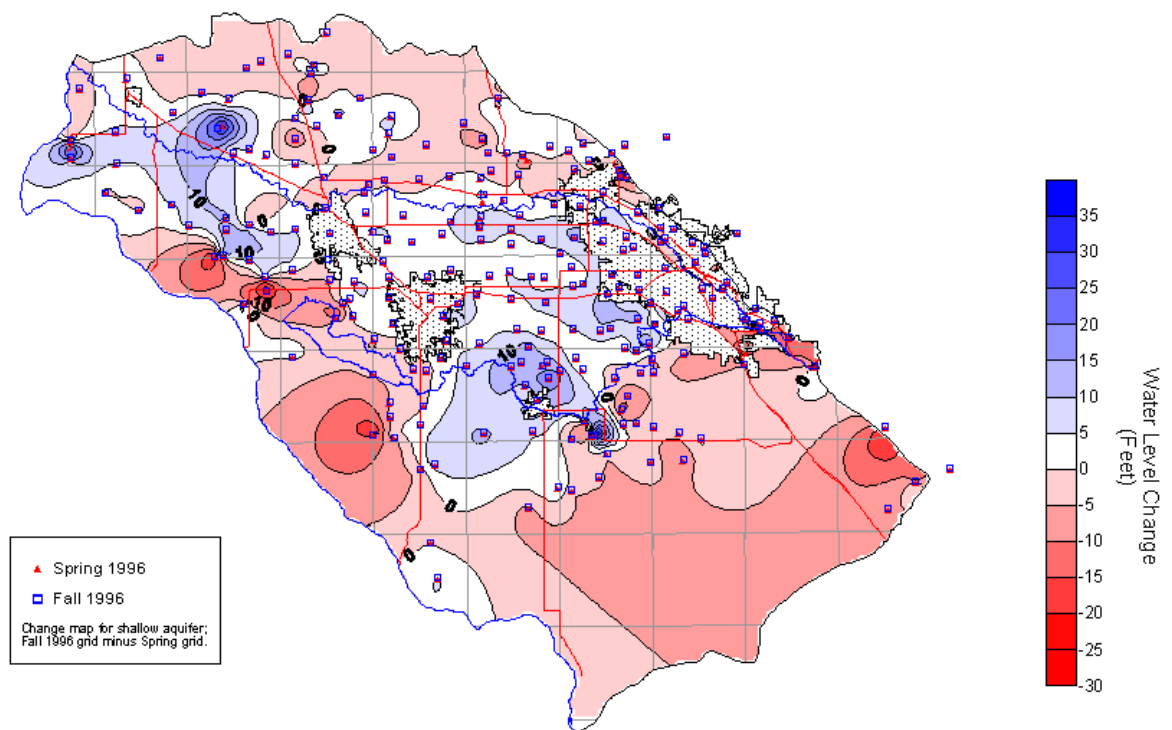


Figure 5-4: Spring and fall 1996 change map.

The reliability of the water level change map is limited by the reliability of the spring and fall water level interpolations. The interpolations, and comparisons based on interpolations, may contain substantial error, especially in areas containing few data points (such as areas along the periphery of the project area).

5.3. Periodic Ground Water Level Monitoring

Monthly, quarterly, or semi-annual ground water level measurements were made in a variety of Treasure Valley wells. The monitoring network and monitoring results are described in the following sections.

5.3.1. Well Network Description

The TVHP monitoring well network consisted of approximately 72 wells¹². The purpose of the periodic measurements was to provide a basis for (1) evaluating seasonal fluctuations in water levels and (2) establishing long-term water level trends. The wells were measured on a monthly basis from 1996 through 2001, and measured on a quarterly basis thereafter. The locations of the monthly monitoring wells are shown in Figure 5-5. Well construction details for these wells are provided in Appendix D.

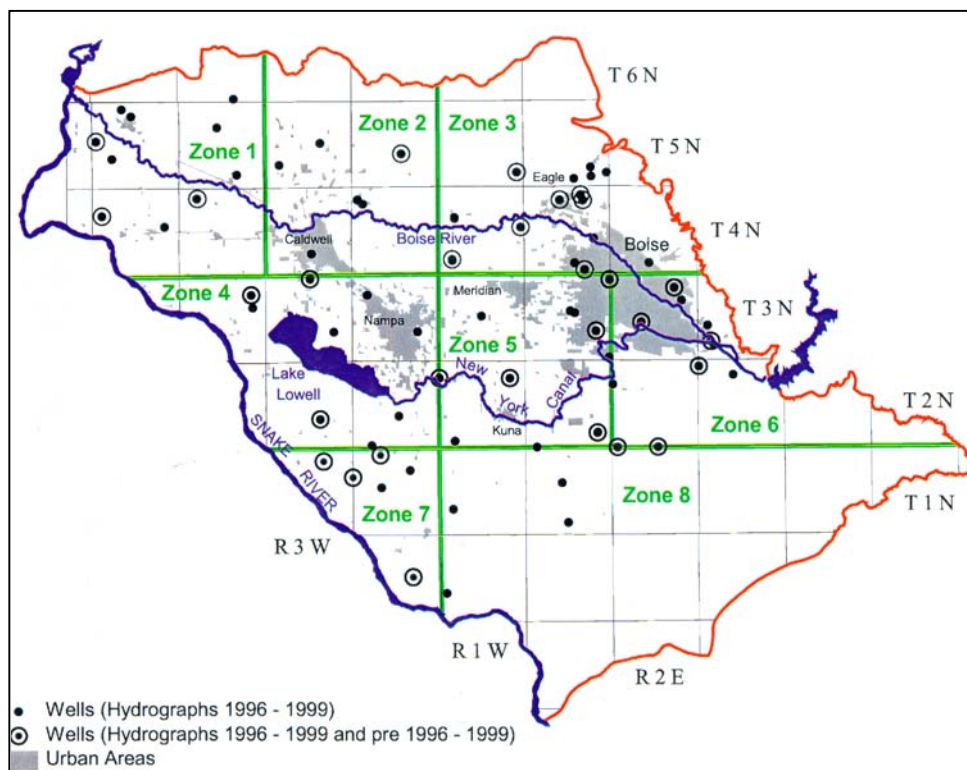


Figure 5-5: Locations of hydrograph wells

¹² These wells were also included in the mass measurements described in Section 5.2.

Thirty of the TVHP monitoring wells have been monitored cooperatively by the IDWR and the USGS since the 1950s. Water levels in these wells (referred to as “co-op wells”) were measured primarily on a semi-annual basis, although a few of the wells were measured more frequently. The measurement frequency in these wells was increased to a monthly basis in 1996 as part of the TVHP.

Forty-two wells were added to the monthly measurement program in 1996. The 42 monitoring wells were selected from 305 wells measured in the spring 1996 mass water-level measurement. Criteria for selecting the additional monitoring wells included

1. Spatial distribution throughout project area
2. Available drillers’ report
3. Reasonably detailed lithologic log
4. Discrete open interval, preferably corresponding with specific aquifer depths
5. Access to well by USGS, IDWR, or other personnel for conducting measurements

5.3.2. Hydrographs

Water level measurements from these wells were used to construct well hydrographs. Hydrographs from the TVHP monthly monitoring wells for April 1996 through December 2002 are presented in Appendix F. These hydrographs are organized by area for convenience (Figure 5-5). Hydrographs from wells with a longer sampling record (long-term “co-op” wells) are also presented in Appendix F.

Hydrograph data indicate that (1) water levels in many parts of the valley appear to be relatively stable, but water level declines have occurred in some areas; (2) long term water level increases have occurred in some areas; and (3) most wells fluctuate on a seasonal basis. The seasonal variations can be caused by pumping, recharge, or both.

In general, water levels in many parts of the valley appear to be relatively stable from year to year. Some of the stability reflects shallow water levels in the central and western parts of the valley that are being controlled by topography (e.g., the elevations of canals and drains). There are, however, a number of wells that have experienced increasing or decreasing water levels (Table 5-3). Of the 32 wells with long-term data records, approximately 13 showed water level decreases and 5 showed increases (the rest were relatively stable)¹³. Of the 71 wells with short-term records (which includes all of the wells with long-term records), approximately 24 showed some amount of

¹³ The number of wells showing water level increases or decreases is somewhat subjective.

water level decrease and 8 showed increases. The greatest declines have occurred in the area south of Lake Lowell (declines of about 65 feet) and southeast Boise (declines of 30 feet). Water levels in several intermediate and deep wells have declined in areas 3 and 5 (Figure 5-5 and Appendix F), which represent the central portion of the basin (west Boise, Eagle, Meridian, and Kuna).

The wells showing water level increases or decreases (Table 5-3) may or may not reflect regional conditions. For example, increased withdrawals from an extraction well used for monitoring (or a nearby pumping well) may cause an apparent local decline that does not reflect regional water levels. A field survey of select wells (Figure 5-6) was conducted during August 1999 to determine the possible cause of the water level changes. Each well was visited and any obvious changes in land use that may have contributed to the observed water level changes were noted. Appendix G contains hydrographs for these wells, including a brief description of what may have contributed to the observed water level changes. In most cases, wells displaying decreasing trends are located in areas that appeared to be undergoing transitions from flood irrigated farmland to residential development. It is unclear whether observed drawdowns in these areas reflect local equilibria required for increased withdrawals or regional ground water level declines. Additional monitoring is recommended in these areas using non-pumping wells.

| | Area (see Figure 3-7) | Total Number of Wells in Area | Number of Wells with Increasing Water Level (categorized by total well depth below ground surface) | | | Number of Wells with Decreasing Water Level (categorized by total well depth below ground surface) | | |
|---|--------------------------------|--|--|--------------|-------|--|--------------|-------|
| | | | 0-200' | 200- 400' | >400' | 0-200' | 200- 400' | >400' |
| Long-Term Data Record (> 7 years) | 1&2 | 4 | | 1 | | 1 | | |
| | 3 | 9 | | | | 3 | 3 | 1 |
| | 4 | 3 | | | | 1 | | |
| | 5 | 5 | | | | 1 | 1 | 2 |
| | 6 | 6 | | | 2 | 1 | | |
| | 7 & 8 | 5 | | | 2 | | | |
| Total number of wells | | 32 | | 1 | 4 | 6 | 4 | 3 |
| Short-Term Data Record (~7 years) | 1 | 10 | | | | 1 | | |
| | 2 | 6 | | | 1 | 2 | | |
| | 3 | 15 | | | | 5 | 1 | 3 |
| | 4 | 9 | | 1 | 1 | 3 | | |
| | 5 | 11 | | | | 3 | 4 | |
| | 6 | 10 | | 2 | 2 | | 1 | |
| | 7 | 5 | | | 1 | | | 1 |
| | 8 | 5 | | | | | | |
| Total number of wells | | 71 | | 3 | 5 | 14 | 6 | 4 |

Table 5-3: Approximate number of monitoring wells with increasing or decreasing water levels.

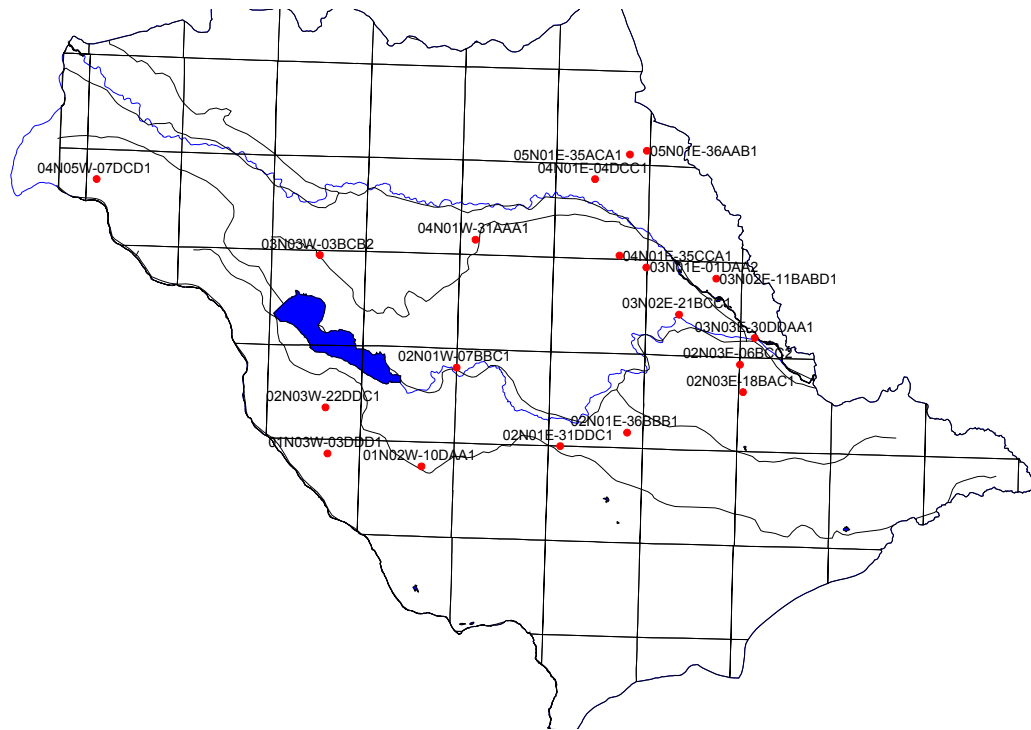


Figure 5-6: Locations of wells showing substantial water level changes.

6. AQUIFER INFLOWS AND OUTFLOWS

6.1. Introduction

An annual water budget was prepared for the Treasure Valley aquifer system for the calendar year 1996 (Urban and Petrich, 1998). The water budget provides an estimate of the current balance between total aquifer withdrawals and discharge, aquifer recharge, and changes in aquifer storage. Specific objectives for this water budget were to (1) define major water budget components, (2) estimate inflows and outflows for the Treasure Valley aquifer systems, (3) describe, where possible, the spatial characteristics of inflows and outflows, (4) create GIS coverages of the water budget data, and (5) create input files (e.g., recharge, withdrawals and ET) for the Treasure Valley ground water flow model. A revised 1996 water budget was completed more recently (Urban, 2004) and also includes a water budget for the year 2000.

6.2. 1996 Water Budget

Inflows to the Treasure Valley aquifer system include (1) seepage from canals and irrigated fields, (2) seepage from rivers and streams, (3) seepage from Lake Lowell, (4) underflow, (5) infiltration of precipitation and surface water, and (6) seepage from rural domestic septic systems. Outflows include (1) municipal withdrawals, (2) industrial withdrawals, (3) irrigation withdrawals, (4) rural domestic withdrawals, (5) stock withdrawals, (6) discharge to canals, drains, and rivers, and (7) evapotranspiration.

Total inflow (Table 6-1) into the Treasure Valley aquifer system was estimated to be 1,035,000 acre-feet (af) in 1996, while total outflow was estimated to be 999,000 af. The net difference shows an apparent increase in aquifer storage of 36,000 af. This difference is less than 4% of the total recharge or discharge and is well within the estimated margin of error of individual component estimates.

The largest source of estimated ground water recharge was seepage from the canal system, followed by seepage from flood irrigation and precipitation. The aggregate discharge to the Boise and Snake Rivers (through canals, drains, or direct discharge) is far greater than all withdrawals combined. On a valley-wide basis, the volume of annual ground water withdrawals represents approximately 20% of the total 1996 ground water recharge (Table 6-1).

| Sources of Recharge and Discharge | Estimated Recharge/Discharge for 1996 | |
|---|---------------------------------------|------------------|
| Recharge ¹ | acre-feet | Percent of Total |
| Canal Seepage | 637,000 | 61 |
| Seepage from Rivers and Streams | 16,000 | 1 |
| Seepage from Lake Lowell | 19,000 | 2 |
| Underflow | 8,000 | 1 |
| Flood Irrigation and Precipitation ² | 302,000 | 30 |
| Recharge by Other Land Uses ³ | 48,000 | 4 |
| Rural Domestic Septic Systems | 5,000 | <1 |
| Total Recharge¹ | 1,035,000 | |
| Discharge | | |
| Domestic and Industrial Withdrawals | 66,000 | 6 |
| Municipal Irrigation | 10,000 | 1 |
| Self-Supplied Industrial | 21,000 | 2 |
| Agricultural Irrigation | 72,000 | 7 |
| Rural Domestic Withdrawals | 27,000 | 2 |
| Stock Watering | 3,000 | <1 |
| Discharge to Rivers and Drains | 800,000 | 81 |
| Total Discharge | 999,000 | |
| Net Difference⁴ | +36,000 | |

1. See text for explanations; values shown in this table are rounded to the nearest 1,000 acre-feet.

2. Includes recharge from precipitation and irrigation on flood-irrigated lands only.

3. Includes recharge from precipitation by land use; does not include flood-irrigated land.

4. Because of the error associated with the individual water budget components, a positive net difference does not necessarily indicate a positive change in aquifer storage.

Table 6-1: Summary of recharge and discharge estimates contained in the 1996 water budget.

Primary ground water withdrawal and recharge areas do not necessarily coincide throughout the valley. The primary recharge areas are those with extensive canals and/or flood irrigation, while the greatest withdrawals occur in areas that are not flood irrigated. For example, agricultural irrigation withdrawals (non-supplemental) are concentrated in areas where surface water irrigation is unavailable, and municipal withdrawals are concentrated near the urban areas of Boise, Nampa, Caldwell, and Meridian. As a result, withdrawals may exceed recharge in local areas within the Treasure Valley, resulting in local water level declines. Water level increases were noted in areas where recharge appears greater than local withdrawals.

The aggregate nature of the water budget masks the differences between inflows to and outflows from individual aquifer zones. Much of the inflow may only recharge shallow aquifers; recharge to deeper zones depends on local vertical hydraulic gradients and aquifer material properties. Recharge to deeper zones is estimated to be a small portion of the total aquifer inflows (Petrich, 2004a).

The aggregate nature of the water budget also masks the temporal characteristics of ground water recharge, withdrawals, and natural discharge. Infiltration from the

surface water distribution system and irrigation occurs primarily in the summer. The actual aquifer recharge from irrigation activities lags the initial infiltration, thus water levels may be rising months after irrigation has ceased. Municipal withdrawals also vary throughout the year but are generally greatest during the summer irrigation season.

Several general conclusions were drawn from this 1996 water budget:

1. The largest components of aquifer recharge in the Treasure Valley are seepage from the canal system and infiltration associated with irrigated agriculture.
2. Discharge to rivers, drains, and canals is the largest source of discharge from the Treasure Valley aquifer system.
3. Overall, aggregate aquifer recharge to the Treasure Valley aquifer system appears to be in dynamic equilibrium with the aggregate aquifer discharge. The net difference between estimated recharge and discharge is well within the error range of the large water budget components and is therefore negligible.
4. Recharge to shallow Treasure Valley aquifers is influenced significantly by land use (by the location of irrigation activities).

7. TREASURE VALLEY GROUND WATER FLOW CHARACTERISTICS

This section presents a summary of ground water flow in the Treasure Valley based on the descriptions of aquifer characteristics (Section 3, page 13), water level measurements (Section 5, page 36), and inflows and outflows (Section 6, page 46). This summary represents a “conceptual model” of ground water flow in the basin that was the basis for a series of aquifer simulations (Petrich, 2004a; 2004b).

The Treasure Valley aquifer system is comprised of a complex series of interbedded, tilted, faulted, and eroded sediments extending to depths of over 6,000 feet in the deepest parts of the basin (Wood and Clemens, in press). The valley contains shallow, local flow systems (with ground water residence times ranging from years to hundreds of years) and a deep, regional flow system (with residence times ranging from hundreds to tens of thousands of years). Few water wells extend beyond a depth of about 1,200 feet.

The Treasure Valley sedimentary section reflects a history of lacustrine, deltaic, fluvial, and alluvial deposition (see Section 3.3). In general, basin sedimentary deposits grade from coarser, more permeable sediments near the Boise Front to finer, less permeable sediments at the distal end of the basin. At the basin scale, sediments also grade finer with depth. Highly permeable deposits associated with deltaic and/or fluvial deposition are often sandwiched between lacustrine deposits of lower permeability.

Ground water flow in the Treasure Valley is controlled by aquifer characteristics and hydraulic gradient. Aquifer characteristics influencing ground water flow include grain size, sorting, stratigraphic layering, sedimentary layer dip, sediment grain cementation, and the degree of fracturing (in basalt aquifers). Additional controls on the movement of ground water are attributed to structural processes, including faulting throughout the basin and along the basin margin. A series of southeast-northwest trending faults dissect the valley, with stratigraphic offsets of several hundred feet or more. Analyses of aquifer test data from southeast Boise (West and Osiensky, 1999) indicate negative boundary conditions associated with faults in the southeast Boise area. Artesian conditions just north of the Boise River in the vicinity of monitoring well TVHP #1 may be created in part by restricted flow across the Eagle–West Boise Fault Zone (Figure 3-2). Ground water chemistry data (Hutchings and Petrich, 2002a) indicate different ground water chemistry north of the fault zone compared to the area south of the fault zone, suggesting restricted flow across the fault zone. Basin downwarping and an associated downslope trend in sediment deposition contribute to steeply dipping sedimentary deposits that may cause deeper aquifer units to pinch out at depth (Wood, 1997a). Based on seismic imaging and outcrop mapping, aquifer sediments of various fault blocks are dipping at angles ranging from zero to approximately 12 degrees (Wood, 1997a).

Fractures within shallow Pleistocene basalts or along upper and lower surfaces of individual basalt flows can contribute to ground water movement. For instance, basalt fractures and coarse-grained sediments underlying the basalt may greatly contribute to transmitting leakage from the New York Canal (and other surface water channels) into shallow aquifers.

An erosional unconformity associated with changing lake levels in Pliocene Lake Idaho truncates down-dipping units near the basin margin near Boise (Squires and Wood, 2001; Squires et al., 1992; Wood, 1997a). The unconformity separates lacustrine and deltaic sediments (tilted in the Boise area) from overlying lacustrine/deltaic sediments. Coarse-grained sediments associated with the erosional unconformity (Squires et al., 1992; Wood, 1997a) appear to serve as a manifold for deeper, regional ground water migrating horizontally into the basin from alluvial fan sediments in the eastern portion of the basin (corroborated by E. Squires, pers. comm., 2002).

Potentiometric surface contours indicate ground water movement in a westerly to southwesterly direction, depending on depth and location (Section 5.2.2, page 38). Potentiometric surface contours in shallow aquifer zones reflect surface hydrologic conditions, such as mounding under the New York and Mora Canals (e.g., Figure 5-1) or discharge to the Boise River. The mounding in the vicinity of the New York Canal represents a local ground water divide, with shallow ground water north of the canal flowing toward the Boise River and shallow ground water south of the canal flowing toward the Snake River. Potentiometric surface contours from shallow aquifers show ground water flow toward and discharge to the Boise River in mid- to lower reaches. Potentiometric surface contours in deeper zones indicate a more uniform westerly flow direction (Section 5.2.2, page 38). Downward hydraulic gradients are indicated along the Boise Foothills, the eastern part of the study area (see TVHP #4 well in Figure 4-5), and in the vicinity of the New York and Mora Canals. Upward gradients are evident in the central and western portions of the valley (see TVHP #2 hydrographs in Figure 4-3) and in the vicinity of the Boise River.

Individual hydrographs (Section 5.3 and Appendix F) indicate relatively stable water levels in many areas, although water level declines have occurred in a number of wells. Wells in two areas, southeast Boise (e.g., well 03N03E-30DDAA1) and south of Lake Lowell (e.g., well 03N04W-11ADA1), have experienced declines of approximately 30 feet and 65 feet, respectively. Water levels in these areas appear to have stabilized in recent years.

Additional ground water level declines were observed (Appendix F and Table 5-3) in areas 3 (northwest Boise and Eagle, Figure 5-5) and 5 (southwest Boise, Meridian, and Kuna). Most of the long-term declines in these wells have been less than 10 feet. Reasons for the declines may include increased withdrawals from the measured wells

(very few of the monitoring wells are dedicated to monitoring alone), increased nearby withdrawals, and/or changes in local infiltration rates (Appendix G). Further investigation of these apparent declines is warranted to determine if they reflect regional or local conditions. Additional monitoring wells would also be warranted in these areas of apparent declines.

A number of shallow monitoring wells indicated water level decreases (Table 5-3). Shallow wells may be especially sensitive to changes in local surface water irrigation patterns in areas where the water table is not in direct hydraulic connection with surface channels. Ground water level changes are less likely in shallow wells in areas where the water table is controlled by topography (by virtue of drains and canals).

Seasonal water level fluctuations are evident in many Treasure Valley wells. The fluctuations generally are a response to seasonal increases in withdrawals (e.g., summer irrigation withdrawals) or increases in recharge associated with surface water irrigation.

The largest component of recharge to shallow aquifers is seepage from the canal system and infiltration associated with irrigated agriculture (Urban, 2004; Urban and Petrich, 1998). Water enters shallow aquifers as infiltration from canals, irrigated areas, and other water bodies (e.g., Lake Lowell), and possibly from upper reaches of the Boise River (e.g., Barber Dam to Capitol Street Bridge) during high flows. Infiltration from surface channels occurs if and when (1) water is available and (2) hydraulic heads in the channel (or lake) are higher than the surrounding aquifer heads. Additional recharge sources include mountain front recharge, underflow from the granitic Idaho Batholith and tributary sedimentary aquifers, and direct precipitation.

Shallow aquifer levels increased by as much as 100 feet in some areas in response to the initiation of large-scale flood irrigation in the late 1800s and early 1900s. Shallow ground water levels rose to and remained at (or near) ground surface in many areas (at least seasonally), discharging to drains and other surface channels.

Shallow and intermediate aquifers are separated from deeper zones by interbedded silt and clay layers in many parts of the valley. While individual clay layers are not necessarily areally extensive, multiple clay layers in aggregate form effective barriers to vertical ground water movement.

Recharge to the deeper aquifers begins as downward flow through coarse-grained alluvial fan sediments in the eastern portion of the basin and as underflow at basin margins. Ground water is then thought to flow horizontally into the basin via more permeable sediments (e.g., coarse-grained sediments of the geological unconformity overlying Chalk Hills sediments), intersecting the alluvial fan sediments.

This is illustrated in water chemistry data collected from shallow aquifers near the New York Canal. Water in the canal, as in upper portions of the Boise River, has relatively low specific conductance (and by inference, total dissolved solids). In shallow aquifers underlying the canal, specific conductance was found to increase with depth, corresponding with canal water that has infiltrated through soil horizons. In contrast, water in deeper sand units separated from upper zones by multiple clay layers has lower specific conductance than water in overlying horizons (Hutchings and Petrich, 2002a; Hutchings and Petrich, 2002b). This finding indicates that water in at least some deeper aquifers originates at the basin margins and does not enter the ground water regime through the carbon-rich sediments found in Treasure Valley soils.

Residence times of Treasure Valley ground water were generally found to increase with depth and distance along a regional east-to-west-trending flow path (Hutchings and Petrich, 2002a). Residence time estimates ranged from thousands to tens of thousands of years. The youngest waters entered the subsurface a few thousand years ago and were found along the northeastern boundary of the basin, adjacent to the Boise Foothills. The oldest waters entered the subsurface between 20,000 and 40,000 years ago and were found in the western reaches of the basin near the Snake River. Ground water in the deep deltaic aquifers beneath Boise entered the subsurface between 10,000 and 20,000 years ago.

Comparisons between measured water chemistry constituents and established models of geochemical processes (Hutchings and Petrich, 2002a) show that (1) ground water near the northeastern basin margin has experienced little interaction with aquifer minerals, and (2) ground water beyond the northeastern basin margin has experienced substantial interaction with aquifer minerals. Geochemical evolution of Treasure Valley ground water appears to be influenced by solution of both carbonate and silicate minerals.

Ground water discharge to rivers, drains, and canals represents the dominant form of discharge from the Treasure Valley aquifer system (Urban and Petrich, 1998). The primary form of natural discharge from the deeper aquifers is thought to be regional upwelling in the southern and western portions of the basin, with ultimate discharge to the Boise River and/or Snake River. Rates of discharge from the deeper aquifers in the western portions of the valley are unknown but are probably low because of the thick accumulation of lacustrine clays separating these aquifers from ground surface.

Relatively long residence times in the regional flow system (over 20,000 years) implies that (1) regional aquifers are not very transmissive, (2) recharge rates to the deeper regional aquifers are very limited, and/or (3) regional aquifers are discharge-limited. Although there are abundant silt and clay layers with low hydraulic conductivity, productive sand layers are present throughout central portions of the valley; these sand zones are tapped by many irrigation and municipal wells. Recharge to the deeper,

regional system is limited but has generally been sufficient for current rates of withdrawal. Thick lacustrine clays at the distal end of the valley likely inhibit upward (discharge) flow, limiting the amount of water that can flow through the system.

In summary, the Treasure Valley aquifer system consists of shallow aquifers containing local ground water flow systems and a deeper, regional ground water flow system. Recharge to the shallow system consists largely of infiltration from irrigated fields and canals. Primary discharge is to the Boise and Snake Rivers and other streams and to drains discharging into these channels. The deeper, regional flow system consists of (1) recharge in alluvial sediments in southeast Boise and at the base of the mountain front north of Boise, (2) movement of ground water from the recharge areas into the deeper Boise area fluvio-lacustrine aquifers, and (3) movement of ground water from the Boise area aquifers into regional lacustrine/deltaic aquifers in the central and western portions of the valley.

8. REFERENCES

- Anderson, J.E. and Wood, S.H., 1981. Geological, Hydrological Geochemical and Geophysical Investigations of the Nampa-Caldwell and Adjacent Areas, Southwestern Idaho. Chapter 3, Geohydrology, In: Mitchell, J. C., ed., Geothermal Investigations in Idaho, Part 11: Idaho Department of Water Resources, Water Information Bulletin 30: p. 33-42.
- Barrash, W. and Dougherty, M.E., 1995. High-Resolution Seismic Reflection Profiling and Modeling of the Hydrogeologic System, Goddard 2 Well, Northwest Boise, Idaho. Center for Geophysical Investigation of the Shallow Subsurface, Boise State University.
- Berenbrock, C., 1999. Streamflow Gains and Losses in the Lower Boise River Basin, Idaho, 1996-97. U.S. Geologic Survey, Water-Resources Investigations Report 99-4105.
- Beukelman, G., 1997a. Cross Section of the Treasure Valley in the Boise Area: Notes on the Geology of the Boise Area. Department of Geosciences, Boise State University, prepared for the Treasure Valley Hydrologic Project.
- Beukelman, G., 1997b. Cross Section of the Treasure Valley in the Notus Area: Notes on the Geology of the Notus area, Gem, Payette, Canyon, and Owyhee Counties, Idaho. Department of Geosciences, Boise State University, prepared for the Treasure Valley Hydrologic Project.
- Beukelman, G., 1997c. Cross Section of the Treasure Valley in the Ontario Area: Notes on the Geology of the Ontario area, Payette and Canyon Counties, Idaho, and Malheur County, Oregon. Department of Geosciences, Boise State University, prepared for the Treasure Valley Hydrologic Project.
- Beukelman, G., 1997d. Cross Section of the Treasure Valley in the Parma Area: Notes on the Geology of the Ontario area, Payette, Canyon, and Owyhee Counties, Idaho. Department of Geosciences, Boise State University, prepared for the Treasure Valley Hydrologic Project.
- Brockway, C.E. and Brockway, C.G., 1999. Southeast Boise Aquifer Simulation and Aquifer Recharge and Recovery Evaluation. Brockway Engineering, prepared for Micron Technology, Inc.
- Burnham, W.L. and Wood, S.H., 1992. Geologic Map of the Boise South Quadrangle, Ada County, Idaho. Preprint in review for the Idaho Geological Survey Technical Report Series, April 22, 1992.
- Carlson, R.A. and Petrich, C.R., 1998. New York Canal Geologic Cross Section, Seepage Gain/Loss Data, and Ground Water Hydrographs: Compilation and Findings. Idaho Water Resources Research Institute and Idaho Department of Water Resources.
- Clemens, D.M., 1993. Volcanic stratigraphy and tectonic development, Western Snake River Plain, Idaho. M.S. Thesis, Arizona State University.

- Cook, Z., Urban, S., Maupin, M., Pratt, R. and Church, J., 2001. Domestic, Commercial, Municipal, and Industrial Water Demand Assessment and Forecast in Ada and Canyon Counties, Idaho. Idaho Department of Water Resources.
- Dion, N.P., 1972. Some effects of land-use changes on the shallow ground-water system in the Boise-Nampa Area, Idaho. Idaho Department of Water Administration, Water Information Bulletin No. 26.
- Dittus, R., Allred, J. and Squires, E., 1998. Supporting Data for Groundwater Conditions and Aquifer Testing of the Tenmile Ridge Area of South Boise, Ada County, Idaho. United Water Idaho Groundwater Report Series Data Release No. 98-D1.
- Dittus, R., Allred, J. and Squires, E., 1999. Hydrogeology, Geochemistry, and Well Construction of the Treasure Valley Hydrologic Project Monitoring Well #1, Ada County, Idaho. United Water Idaho, Prepared for the Treasure Valley Hydrologic Project.
- Driscoll, F.G., 1986. Groundwater and Wells. Johnson Division, St. Paul, MN.
- Hutchings, J. and Petrich, C., 2002a. Ground water recharge and flow in the regional Treasure Valley aquifer system - geochemistry and isotope study. Idaho Water Resources Research Institute, Research Report IWRRI-2002-08.
- Hutchings, J. and Petrich, C., 2002b. Influence of canal seepage on aquifer recharge near the New York Canal. Idaho Water Resources Research Institute, Research Report IWRRI-2002-09.
- Kimmel, P.G., 1982. Stratigraphy, Age, and Tectonic Setting of the Miocene-Pliocene Lacustrine Sediments of the Western Snake River Plain, Oregon and Idaho. Cenozoic Geology of Idaho. Idaho Bureau of Mines and Geology Bulletin 26, pp. 559-578 pp.
- Liberty, L.M., 1996a. Seismic Reflection Imaging of the Boise Geothermal Aquifer. Center for the Geophysical Investigation of the Shallow Subsurface, Boise State University, BSU CGISS 96-05, Boise, ID.
- Liberty, L.M., 1996b. Seismic Reflection Results: Stewart Gulch Region, Boise, Idaho. Center for Geophysical Investigation of the Shallow Subsurface, Boise State University, BSU CGISS 96-04.
- Liberty, L.M., 1998. Seismic reflection imaging of a geothermal aquifer in an urban setting. Geophysics, 63(4): 1285-1294.
- Liberty, L.M. and Wood, S.H., 2001. Treasure Valley Seismic Reflection Project - UPRR 2000 Profile. Center for Geophysical Investigation of the Shallow Subsurface, Department of Geosciences, Boise State University, CGISS 01-01.
- Lindgren, J.E., 1982. Application of a ground water model to the Boise Valley Aquifer in Idaho. M.S. Thesis, University of Idaho.
- Lindgren, W., 1898. Description of the Boise Quadrangle, Idaho. U.S. Geological Survey.
- Mabey, D.R., 1982. Geophysics and tectonics of the Snake River Plain, Idaho. In: Bill Bonnicksen and R. M. Breckenridge, editors, Cenozoic Geology of Idaho. Idaho Bureau of Mines and Geology Bulletin 26: 193-153.

- Malde, H.E., 1991. Quaternary geology and structural history of the Snake River Plain, Idaho and Oregon. In: The Geology of North America, Quaternary Nonglacial Geology: Conterminous U.S., Vol. K-2, 252-281 pp.
- Malde, H.E. and Powers, H.A., 1962. Upper Cenozoic stratigraphy of Western Snake River Plain. Geological Society of America Bulletin, 73: 1197-1220.
- Neely, K.W. and Crockett, J.K., 1998. Ground water quality characterization and initial trend analysis for the Treasure Valley shallow and deep hydrologic subareas. Idaho Department of Water Resources, No. 50 Part 3.
- Newton, G.D., 1991. Geohydrology of the regional aquifer system, Western Snake River Plain, Southwestern Idaho. U.S. Geological Survey Professional Paper 1408-G.
- Othberg, K.L., 1994. Geology and geomorphology of the Boise Valley and adjoining areas, western Snake River Plain, Idaho. Idaho Geological Survey Bulletin 29: 54 pp.
- Othberg, K.L. and Stanford, L., 1992. Geologic map of the Boise Valley and adjoining area, Western Snake River Plain, Idaho. Idaho Geological Survey.
- Petrich, C., 2003. Investigation of Hydrogeologic Conditions and Ground Water Flow in the Boise Front Geothermal Aquifer (Executive Summary). Idaho Water Resources Research Institute, Research Report IWRRI-2003-07.
- Petrich, C.R., 2004a. Simulation of Ground Water Flow in the Lower Boise River Basin. Idaho Water Resources Research Institute, Research Report IWRRI-2004-02.
- Petrich, C.R., 2004b. Simulation of Increased Ground Water Withdrawals in the Treasure Valley Associated with Unprocessed Well Applications. Idaho Water Resources Research Institute, Research Report IWRRI-2004-03.
- Petrich, C.R., 2004c. Treasure Valley Hydrologic Project - Executive Summary. Idaho Water Resources Research Institute, Research Report IWRRI-2004-04.
- Ralston, D.R. and Chapman, S.L., 1970. Ground-water resource of southern Ada and western Elmore Counties, Idaho. Idaho Department of Reclamation, Water Information Bulletin No. 15.
- Scanlan, T.M., 2001. Final Report on the Quarry View Park Well Project. Scanlan Engineering, prepared for the City of Boise.
- Squires, E. and Derricott, S.L., 1992. Hydrogeologic investigation for the proposed State of Idaho, Department of Transportation Blacks Creek rest area, Ada County Idaho. A report to the Idaho State Department of Transportation.
- Squires, E. and Wood, S., 1989. Investigation of groundwater in the Tenmile Ridge area of South Boise, Idaho. Department of Geology and Geophysics, Boise State University, Boise, Idaho.
- Squires, E., Wood, S., Osiensky, J. and Dittus, R., 1993. Groundwater conditions and hydraulic testing of the Boise-Fan Aquifer of Southeast Boise River Valley, Ada County, Idaho. prepared for the Boise Water Corporation.
- Squires, E. and Wood, S.H., 2001. Stratigraphic Studies of the Boise (Idaho) Aquifer System using Borehole Geophysical logs with Emphasis on Facies Identification of Sand

- Aquifers, prepared for the Treasure Valley Hydrologic Study, Idaho Department of Water Resources.
- Squires, E., Wood, S.H. and Osiensky, J.L., 1992. Hydrogeologic Framework of the Boise Aquifer System, Ada County, Idaho. Research Technical Completion Report, Idaho Water Resources Research Institute, University of Idaho. 114 pp.
- Urban, S.M., 2004. Water Budget for the Treasure Valley Aquifer System for the Years 1996 and 2000. Idaho Department of Water Resources.
- Urban, S.M. and Petrich, C.R., 1998. 1996 Water Budget for the Treasure Valley Aquifer System. Idaho Department of Water Resources Research Report.
- West, S. and Osiensky, J., 1999. Analysis of aquifer test data from selected southeast Boise wells, Idaho.
- Wood, S.H., 1994. Seismic expression and geological significance of a lacustrine delta in Neogene deposits of the Western Snake River Plain, Idaho. AAPG Bulletin, 1(January): p. 102-121.
- Wood, S.H., 1996a. Cross Sections of the Southeast Boundary of the Treasure Valley Groundwater Study Area: Notes on the Geology of the Mayfield-Orchard Area, Ada and Elmore County, Idaho. Boise State University Geosciences, prepared for the Treasure Valley Hydrologic Project.
- Wood, S.H., 1996b. Preliminary Map of the Base of the Sedimentary Section of the Western Snake River Plain. Department of Geosciences, Boise State University, Geological interpretation for the Treasure Valley Hydrologic Project.
- Wood, S.H., 1997a. Hydrogeologic Framework of the Boise Valley of Southwest Idaho. Dept. of Geosciences, Boise State University.
- Wood, S.H., 1997b. Structural contour map of the top of Miocene basalt basement rocks, Western Snake River Plain, Idaho.
- Wood, S.H., 1997c. Structure Contour map of the Top of the Mudstone Facies, Western Snake River Plain, Idaho. Geosciences Department, Boise State University.
- Wood, S.H. and Anderson, J.E., 1981. Part 11: Geological, hydrological, and geochemical and geophysical investigations of the Nampa-Caldwell and adjacent areas, southwestern Idaho. In: J.C. Mitchell (Editor), Geothermal investigations in Idaho. Idaho Department of Water Resources.
- Wood, S.H. and Burnham, W.L., 1987. Geologic Framework of the Boise Warm Springs Geothermal Area, Idaho. Geological Society of America Centennial Field Guide-Rocky Mountain Section: pp. 117-122.
- Wood, S.H. and Clemens, D.M., *in press*. Geologic and tectonic history of the western Snake River Plain, Idaho and Oregon. In: B. Bonnicksen, C.M. White and M. McCurry (Editors), Tectonic and Magmatic Evolution of the Snake River Plain Volcanic Province. Idaho Geologic Survey.

Wood, W.W. and Low, W.H., 1988. Solute Geochemistry of the Snake River Plain Regional Aquifer System, Idaho and Eastern Oregon. Regional Aquifer System Analysis, U. S. Geological Survey Professional Paper 1408-D: 79 pp.

Appendix A. CONVERSION FACTORS

Volume

- 1 cubic foot of water = 7.4805 gallons = 62.37 pounds of water
- 1 acre-foot (af) = enough water to cover 1 acre of land 1 foot deep
- 1 acre-foot (af) = 43,560 cubic feet
- 1 acre-foot (af) = 325,850 gallons
- 1 million gallons = 3.0689 acre-feet

Flow Rates

- 1 cubic foot per second (cfs) = 448.83 gallons per minute (gpm) = 26,930 gallons per hour
- 1 cubic foot per second (cfs) = 646,635 gallons per day = 1.935 acre-feet per day
- 1 cubic foot per second (cfs) for 30 days = 59.502 acre-feet
- 1 cubic foot per second (cfs) for 1 year = 723.94 acre-feet
- 1 cubic meter per second (cms) = 25.31 cubic feet per second
- 1 cubic meter per second (cms) = 15,850 gallons per minute
- 1 million gallons per day (mgd) = 1,120.147 acre-feet per year
- 1 miner's inch = 9 gallons per minute
- 1 miner's inch = 0.02 cubic feet per second

Hydraulic Conductivity

- 1 gallon per day per foot² (gal/day/ft²) = 0.134 foot/day = 0.0408 meters/day

Economic

- \$0.10 per 1,000 gallons = \$32.59 per acre-foot

Appendix B. AQUIFER TEST DATA

This appendix contains selected aquifer test data (compiled by Rick Carlson, formerly with the Idaho Water Resources Research Institute). References for the aquifer test data are listed beginning on page 81.

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANSMISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|---------------------|----------|----------------------------|-------------------------|--------------------------|--------------------|----------------------|----------------|-------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|-----------------------------|
| New Playground Well | 3N2E9DC | 260 | 111 - 260 | m | 1145 | pumping well | early | 13,200 | 150 | 88 | *** | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | med. Sand | 2/13/92 | 1 | A step test was completed |
| New Playground Well | 3N2E9DC | 260 | 111 - 260 | m | 1145 | pumping well | late | 16,000 | 150 | 107 | *** | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | med. Sand | 2/13/92 | 1 | |
| New Playground Well | 3N2E9DC | 260 | 111 - 260 | m | 1145 | obs. well 1 (80ft) | early | 12,300 | 150 | 82 | *** | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | med. Sand | 2/13/92 | 1 | |
| New Playground Well | 3N2E9DC | 260 | 111 - 260 | m | 1145 | obs. well 1 (80ft) | late | 18,300 | 150 | 122 | 8E-04 | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | med. Sand | 2/13/92 | 1 | |
| New Playground Well | 3N2E9DC | 260 | 111 - 260 | m | 1145 | obs. well 2 (1700ft) | early | *** | 150 | | *** | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | med. Sand | 2/13/92 | 1 | |
| New Playground Well | 3N2E9DC | 260 | 111 - 260 | m | 1145 | obs. well 2 (1700ft) | late | 23,000 | 150 | 153 | *** | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | med. Sand | 2/13/92 | 1 | T for this well is suspect. |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|-----------------------|----------|----------------------------|-------------------------|--------------------------|--------------------|----------------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|---|
| New Playground Well | 3N2E9DC | 260 | 111 - 260 | m | 1145 | obs. well 3 (2000ft) | early | *** | 150 | *** | *** | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | med. Sand | 2/13/92 | 1 | |
| New Playground Well | 3N2E9DC | 260 | 111 - 260 | m | 1145 | obs. well 3 (2000ft) | late | *** | 150 | *** | *** | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | med. Sand | 2/13/92 | 1 | |
| New Ball Diamond Well | 3N2E9DD | 435 | 186-396 | m | 1200 | obs. well 1 | early | 58,000 | 150 | 387 | *** | 31.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | med. Sand | 3/2/92 | 2 | |
| New Ball Diamond Well | 3N2E9DD | 435 | 186-396 | m | 1200 | obs. well 1 | late | 13,000 | 150 | 87 | 7E-04 | 31.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | med. Sand | 3/2/92 | 2 | |
| New Ball Diamond Well | 3N2E9DD | 435 | 186-396 | m | 1200 | obs. well 2 | early | *** | 150 | *** | 8E-04 | 31.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | med. Sand | 3/2/92 | 2 | High, late, T values suggest hydraulic boundaries |
| New Ball Diamond Well | 3N2E9DD | 435 | 186-396 | m | 1200 | obs. well 2 | late | 13,000 | 150 | 87 | *** | 31.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | med. Sand | 3/2/92 | 2 | |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|-----------------------------|----------|----------------------------|-------------------------|--------------------------|--------------------|----------------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|---|------------------|--------------------------|------------|-----------|--|
| New Ball Diamond Well | 3N2E9DD | 435 | 186-396 | m | 1200 | obs. well 3 | early | *** | 150 | *** | 3E-04 | 31.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | med. Sand | 3/2/92 | 2 | |
| Floating Feather Hills Well | 4N1E3CCC | 415 | 215-265, 375-385 | m | 743 | pumping well | early | 11,986 | 160 | *** | *** | 10.3 | constant rate pump test, Jacobs Semi-log Drawdown Method | 720 | fine sand to course sand | 3/26/91 | 3 | Early T believed to be affected by casing storage. |
| Floating Feather Hills Well | 4N1E3CCC | 415 | 215-265, 375-385 | m | 743 | pumping well | late | 143,749 | 160 | 898 | *** | 10.3 | constant rate pump test, Jacobs Semi-log Drawdown Method | 720 | fine sand to course sand | 3/26/91 | 3 | |
| Floating Feather Hills Well | 4N1E3CCC | 415 | 215-265, 375-385 | m | 743 | obs. well 1 (900ft) | late | 83,350 | 160 | 521 | 0.019 | 10.3 | constant rate pump test, Chow Semi-log Time Drawdown Method | 720 | fine sand to course sand | 3/26/91 | 3 | |
| Floating Feather Hills Well | 4N1E3CCC | 415 | 215-265, 375-385 | m | 743 | obs. well 2 (1300ft) | early | 553,418 | 160 | 3459 | 0.02 | 10.3 | constant rate pump test, Chow Semi-log Time Drawdown Method | 720 | fine sand to course sand | 3/26/91 | 3 | High T from gravity drainage effects |
| Floating Feather Hills Well | 4N1E3CCC | 415 | 215-265, 375-385 | m | 743 | obs. well 4 (2500ft) | early | 681,132 | 160 | 4257 | 0.005 | 10.3 | constant rate pump test, Chow Semi-log Time Drawdown Method | 720 | fine sand to course sand | 3/26/91 | 3 | High T from gravity drainage effects |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|--------------------------------------|----------|----------------------------|-------------------------|--------------------------|--------------------|----------------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|---|------------------|--------------------------|------------|-----------|---|
| Floating Feather Hills Well | 4N1E3CCC | 415 | 215-265, 375-385 | m | 743 | obs. well 4 (2500ft) | late | 219,720 | 160 | 1373 | 0.017 | 10.3 | constant rate pump test, Chow Semi-log Time Drawdown Method | 720 | fine sand to coarse sand | 3/26/91 | 3 | |
| Floating Feather Hills Well | 4N1E3CCC | 415 | 215-265, 375-385 | m | 743 | obs. well 5 (3700ft) | early | 315,339 | 160 | 1971 | 0.017 | 10.3 | constant rate pump test, Chow Semi-log Time Drawdown Method | 720 | fine sand to coarse sand | 3/26/91 | 3 | |
| Floating Feather Hills Well | 4N1E3CCC | 415 | 215-265, 375-385 | m | 743 | obs. well 5 (3700ft) | late | 287,490 | 160 | 1797 | 0.006 | 10.3 | constant rate pump test, Chow Semi-log Time Drawdown Method | 720 | fine sand to coarse sand | 3/26/91 | 3 | |
| Broadway Well | 3N2E22DD | 532 | 250-524 | m | 2975 | pumping well | no | | 225 | *** | *** | 66.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 6 | sand | 7/20/72 | 4 | |
| Redwood Creek Subdivision Well No. 1 | 4N1E7BD | 415 | 298-313, 361 - 401 | m | 2100 | pumping well | no | 55,000 | 200 | 275 | *** | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8.5 | course sand to gravel | 4/7/94 | 5 | Artesian - static water level is 5 feet above ground surface. |
| Redwood Creek Subdivision Well No. 1 | 4N1E7BD | 415 | 298-313, 361 - 401 | m | 2100 | obs. well 1 (2600ft) | no | 154,000 | 200 | 770 | 2E-04 | 24.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8.5 | course sand to gravel | 4/7/94 | 5 | |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY (gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|------------------------|-----------|----------------------------|-------------------------|--------------------------|--------------------|----------------|----------------|--------------------------|--------------------------------|---|-------------|----------------------------|--|------------------|-----------------------|------------|-----------|---|
| Willow Lane Well Field | 4N2E32BCB | 90 | unknown | m | 1400 | yes | no | 274,000 | 90 | 3044 | 0.02 | 23.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 72 | course sand to gravel | 9/14/62 | 6 | 9 observation wells were monitored. |
| Veterans Well | 4N2E32DDC | 275 | 150-275 | m | 800 | pumping well | yes | *** | 125 | *** | *** | 12.3 | constant rate pump test, Jacobs Semi-log Drawdown Method | 94 | course sand to gravel | 5/10/96 | 7 | Unclear if time drawdown measurements were recorded from observation wells. |
| Veterans Well | 4N2E32DDC | 275 | 150-277 | m | 800 | obs. well | late | 10,036 | 125 | 80 | *** | 12.3 | constant rate pump test, Jacobs Semi-log Drawdown Method | 94 | course sand to gravel | 5/10/96 | 7 | Unclear if time drawdown measurements were recorded from observation wells. |
| Gary Lane Well | 4N2E24DBA | 837 | 742-837 | m | 600 | pumping well | yes | *** | 100 | *** | *** | 7.8 | constant rate pump test, Jacobs Semi-log Drawdown Method | 34 | course sand to gravel | 3/23/96 | 8 | Unclear if time drawdown measurements were recorded from observation wells. |
| Gary Lane Well | 4N2E24DBA | 837 | 742-837 | m | 600 | obs. well | late | 3,955 | 100 | 40 | *** | 7.8 | constant rate pump test, Jacobs Semi-log Drawdown Method | 34 | course sand to gravel | 3/23/96 | 8 | Unclear if time drawdown measurements were recorded from observation wells. |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|-------------------|------------|----------------------------|---|--------------------------|--------------------|----------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|---|
| Fisk Well | 3N2E6DDC1 | 850 | 569-589, 604-624, 639-660, 705-715 | m | 1500 | pumping well | no | 39,554 | 145 | 273 | *** | 68.2 | constant rate pump test, Jacobs Semi-log Drawdown Method | 7 | sand? | 1/28/92 | 9 | Aquifer parameters determined from pumping well |
| Market Well | 3N2E35DAD1 | 944 | 460-470, 495-515, 600-610, 695-705, 725-735, 760-775, 804-814, 830-840, 892-902 | s | 1,500 | no | no | 40,000 | 440 | 91 | *** | 40.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | sand? | 5/28/91 | 10 | Aquifer parameters determined from pumping well |
| HP Well | 4N1E27ADC1 | 700 | 598.5-685 | s | 1,400 | no | early | 29,600 | 87 | 340 | *** | 19.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | sand? | 5/17/91 | 11 | |
| HP Well | 4N1E27ADC1 | 700 | 598.5-685 | s | 1,400 | no | late | 12,300 | 87 | 141 | *** | 19.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | sand? | 5/17/92 | 11 | Low, late, T values suggest hydraulic barriers. |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|--------------------|-------------|----------------------------|------------------------------------|--------------------------|--------------------|----------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|--|
| New Goddard Well | 4N1E36BAC | 551 | 475-545 | s | 1,714 | yes | late | 22,000 | 70 | 314 | *** | 15.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 8 | sand | 2/28/91 | 12 | Low, late, T values suggest hydraulic barriers. |
| Columbia Test Well | 3N3E32CD D1 | 802 | 560-575, 628-638, 711-731 | s | 22 | no | early | 5,000 | 150 | 33 | *** | 3.0 | step-rate pump test, Jacobs Semi-log Drawdown Method | 4 | fine sand | 10/5/90 | 13 | Estimated long term yields less than 200gpm. |
| Columbia Test Well | 3N3E32CD D1 | 802 | 560-575, 628-638, 711-731 | s | 40 | no | middle | 1,100 | 150 | 7 | *** | 3.3 | step-rate pump test, Jacobs Semi-log Drawdown Method | 4 | fine sand | 10/5/90 | 13 | |
| Columbia Test Well | 3N3E32CD D1 | 802 | 560-575, 628-638, 711-731 | s | 88 | no | late | 500 | 150 | 3 | *** | 2.1 | step-rate pump test, Jacobs Semi-log Drawdown Method | 4 | fine sand | 10/5/90 | 13 | Low, late, T values suggest hydraulic barriers. |
| Cassia Well | 3N2E16DAA1 | 590 | 215-241, 285-321, 357-367, 390-400 | s | 850 | no | early | 50,000 | 150 | 333 | *** | 29.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 5.7 | unknown | 5/29/90 | 14 | T values may have decreased with longer pump test. |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|-------------------|------------|----------------------------|------------------------------------|--------------------------|--------------------|----------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|--|
| Cassia Well | 3N2E16DDA1 | 590 | 215-241, 285-321, 357-367, 390-400 | s | 850 | no | late | 40,000 | 150 | 267 | *** | 29.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 5.7 | unknown | 5/29/90 | 14 | T values may have decreased with longer pump test. |
| Bergeson Well | 3N2E26DAB1 | 852 | ? | m | 1200 | pumping well | early | 60,000 | 385 | 156 | *** | 15.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | ? | 2/13/90 | 16 | S.C. Determined from step-rate pump test. |
| Bergeson Well | 3N2E26DAB1 | 852 | ? | m | 1200 | pumping well | late | 25,000 | 385 | 65 | *** | 15.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | ? | 2/13/90 | 16 | S.C. Determined from step-rate pump test. |
| Bergeson Well | 3N2E26DAB1 | 852 | ? | m | 1200 | obs. well 1 | early | 150,000 | 385 | 390 | 0.005 | 15.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | ? | 2/13/90 | 16 | Storativity value is suspect. |
| Bergeson Well | 3N2E26DAB1 | 852 | ? | m | 1200 | obs. well 1 | late | 60,000 | 385 | 156 | 0.005 | 15.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | ? | 2/13/90 | 16 | Storativity value is suspect. |
| Bergeson Well | 3N2E26DAB1 | 852 | ? | m | 1200 | obs. well 2 | no | 40,000 | 385 | 104 | 4E-04 | 15.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | ? | 2/13/90 | 16 | |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|----------------------------|--------------|----------------------------|-------------------------|--------------------------|--------------------|----------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|--------------------|------------|-----------|---|
| Bergeson Well | 3N2E26DAB 1 | 852 | ? | m | 1200 | obs. well 3 | no | 40,000 | 385 | 104 | 2E-04 | 15.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | ? | 2/13/90 | 16 | |
| Clinton Street Well | 3N2E8CBB1 | 485 | ? | s | 1500 | pumping well | late | 13,000 | | | *** | 18.9 | constant rate pump test, Jacobs Semi-log Drawdown Method | 9 | ? | 2/8/91 | 17 | Short term S.C averaged 27 gpm/ft. |
| Yanke-Nicholson North Well | 2N2E17AAD 1 | 880 | 537-692, 697-860 | s | 1500 | pumping well | no | 29,000 | 320 | 91 | *** | 30.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 120 | sand, clay, gravel | 11/16/90 | 18 | S.C. is suspect because of discrepancies in static water level. |
| J.R. Flat Test Well | 2N2E2BBC2 | 567 | | s | 725 | pumping well | early | 8,500 | | | | | constant rate pump test, Jacobs Semi-log Drawdown Method | 0.3 | | 7/28/89 | 19 | |
| J.R. Flat Test Well | 2N2E2BBC2 | 567 | | s | 815 | pumping well | late | 25,000 | | | | | constant rate pump test, Jacobs Semi-log Drawdown Method | 6 | | 7/28/89 | 19 | |
| New Long Meadow Well | 3N2E713BC B1 | 415 | 123-401 | m | 1775 | pumping well | early | 62,000 | 278 | 223 | *** | 32.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | | 3/14/89 | 20 | Pumping well was determined to have high efficiency. |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | COND-UCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|----------------------|--------------|----------------------------|-------------------------|--------------------------|--------------------|----------------|----------------|--------------------------|--------------------------------|--------------------------------------|-------------|---------------------------|--|------------------|-----------|------------|-----------|--|
| New Long Meadow Well | 3N2E713BC B2 | 415 | 123-401 | m | 1775 | pumping well | late | 31,000 | 278 | 112 | *** | 32.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | | 3/14/89 | 20 | Pumping well was determined to have high efficiency. |
| New Long Meadow Well | 3N2E713BC B3 | 415 | 123-401 | m | 1175 | obs. well 2 | no | 43,000 | 278 | 155 | *** | 32.0 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | | 3/14/89 | 20 | Pumping well was determined to have high efficiency. |
| Swift No. 2 Well | 4N2E30DC2 | | | m | 2200 | pumping well | early | 100,000 | | | *** | 32 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | | 3/11/89 | 21 | |
| Swift No. 2 Well | 4N2E30DC2 | | | m | 2200 | pumping well | middle | 30,000 | | | *** | 32 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | | 3/11/89 | 21 | |
| Swift No. 2 Well | 4N2E30DC2 | | | m | 2200 | pumping well | late | 15,000 | | | *** | 32 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | | 3/11/89 | 21 | |
| Swift No. 2 Well | 4N2E30DC2 | | | m | 2200 | obs. well | early | 100,000 | | | 0.001 | 32 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | | 3/11/89 | 21 | |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|-------------------|--------------|----------------------------|-------------------------|--------------------------|--------------------|----------------|-----------------------------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|--|
| Swift No. 2 Well | 4NZE30DC2 | | | m | 2200 | obs. well | middle | 35,000 | | | 0.001 | 32 | constant rate pump test, Jacobs Semi-log Drawdown Method | 12 | | 3/11/89 | 21 | |
| Londoner Well | 3NZE?23BA A1 | ?1200 | | s | 55 | pumping well | early-deep zone (810-875) | 8,500 | 65 | 131 | *** | *** | step rate pump test, Jacobs Semi-log Drawdown Method | 6 | | 9/8/88 | 22 | Late, low T values likely due to aquifer thinning. |
| Londoner Well | 3NZE?23BA A1 | ?1200 | | s | 140 | pumping well | late-deep zone (810-875) | 2,500 | 65 | 38 | *** | *** | step rate pump test, Jacobs Semi-log Drawdown Method | 6 | | 9/8/88 | 22 | Late, low T values likely due to aquifer thinning. |
| Londoner Well | 3NZE?23BAA 1 | ?1200 | | s | 35 | pumping well | early-intermediate zone (650-750) | 5,000 | 100 | 50 | *** | *** | step rate pump test, Jacobs Semi-log Drawdown Method | 4.5 | | 9/2/88 | 22 | Low amount of drawdown likely due to upper zone leakage. |
| Londoner Well | 3NZE?23BAA 1 | ?1200 | | s | 135 | pumping well | late-intermediate zone (650-750) | 5,000 | 100 | 50 | *** | *** | step rate pump test, Jacobs Semi-log Drawdown Method | 4.5 | | 9/2/88 | 22 | Low amount of drawdown likely due to upper zone leakage. |
| Londoner Well | 3NZE?23BAA 1 | ?1200 | | s | 82 | pumping well | early-upper zone (220-550) | 10,000 | 330 | 30 | *** | *** | step rate pump test, Jacobs Semi-log Drawdown Method | 4 | | 8/19/88 | 22 | |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|-------------------|-------------|----------------------------|-------------------------|--------------------------|--------------------|--------------------------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|---|
| River Run Well | 3N2E24DB D2 | 485 | 198-480 | m | 1880 | pumping well | early | 50,000 | | | *** | | step rate pump test, Jacobs Semi-log Drawdown Method | 11 | | 3/11/88 | 23 | Third step of test was used as constant rate pump test (9.5 hours). |
| River Run Well | 3N2E24DB D2 | 485 | 198-480 | m | 1880 | pumping well | middle | 25,000 | | | *** | | step rate pump test, Jacobs Semi-log Drawdown Method | 11 | | 3/11/88 | 23 | Third step of test was used as constant rate pump test (9.5 hours). |
| River Run Well | 3N2E24DB D2 | 485 | 198-480 | m | 1880 | pumping well | late | 5,000 | | | *** | | step rate pump test, Jacobs Semi-log Drawdown Method | 11 | | 3/11/88 | 23 | Third step of test was used as constant rate pump test (9.5 hours). |
| River Run Well | 3N2E24DB D2 | 485 | 198-480 | m | 1880 | obs. well 1 (100ft) | no | 10,000 | | | 0.03 | | step rate pump test, Jacobs Semi-log Drawdown Method | 11 | | 3/11/88 | 23 | Third step of test was used as constant rate pump test (9.5 hours). |
| River Run Well | 3N2E24DB D2 | 485 | 198-480 | m | 1880 | obs. well 2 (Logger well) | no | 7,500 | | | 5E-05 | | step rate pump test, Jacobs Semi-log Drawdown Method | 11 | | 3/11/88 | 23 | Third step of test was used as constant rate pump test (9.5 hours). |
| River Run Well | 3N2E24DB D2 | 485 | 198-480 | M | 1880 | obs. well 3 (Long Meadow Well) | no | 6,000 | | | 3E-05 | | step rate pump test, Jacobs Semi-log Drawdown Method | 11 | | 3/11/88 | 23 | Third step of test was used as constant rate pump test (9.5 hours). |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|-----------------------------|----------|----------------------------|-------------------------|--------------------------|--------------------|---------------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|---|------------------|--------------------------|------------|-----------|--|
| Hidden Hollow Landfill EW-2 | | 58 | 32-52 | m | 45 | pumping well | no | 5,400 | 18 | 300 | *** | 10.1 | constant rate pump-bailer test, Neuman Method | 2.5 | fine sand to coarse sand | 4/24/97 | 25 | Pumping rate is based on an average of variable pumping rates. |
| Hidden Hollow Landfill EW-2 | | 58 | 32-53 | m | 45 | obs. well1(10ft) | no | 10,900 | 17 | 641 | 0.05 | 10.1 | constant rate pump-bailer test, Nueman Method | 2.5 | fine sand to coarse sand | 4/24/97 | 25 | Pumping rate is based on an average of variable pumping rates. |
| Hidden Hollow Landfill EW-2 | | 58 | 32-54 | m | 45 | obs. well 2 (160ft) | no | 24,400 | 22 | 1,109 | 0.1 | 10.1 | constant rate pump-bailer test, Nueman Method | 2.5 | fine sand to coarse sand | 4/24/97 | 25 | Pumping rate is based on an average of variable pumping rates. |
| Hidden Hollow Landfill EW-3 | | 98 | 50-70 | m | 45 | pumping well | no | 4,300 | 22 | 195 | *** | 8.2 | constant rate pump-bailer test, Nueman Method | 2 | fine sand to coarse sand | 4/22/97 | 25 | Pumping rate is based on an average of variable pumping rates. |
| Hidden Hollow Landfill EW-3 | | 98 | 50-71 | m | 45 | obs. well 1 (9ft) | no | 10,700 | 22 | 486 | 0.04 | 8.2 | constant rate pump-bailer test, Nueman Method | 2 | fine sand to coarse sand | 4/22/97 | 25 | Pumping rate is based on an average of variable pumping rates. |
| Hidden Hollow Landfill EW-3 | | 98 | 50-72 | m | 45 | obs. well 2 (136ft) | no | 19,300 | 21 | 919 | 0.1 | 8.2 | constant rate pump-bailer test, Nueman Method | 2 | fine sand to coarse sand | 4/22/97 | 25 | Pumping rate is based on an average of variable pumping rates. |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|-----------------------------|----------|----------------------------|-------------------------|--------------------------|--------------------|--------------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|--------------------------|------------|-----------|--|
| Hidden Hollow Landfill EW-4 | | 78 | 51-71 | m | 45 | pumping well | no | 2,100 | 20 | 105 | *** | 4.7 | constant rate pump-bailer test, Nueman Method | 1 | fine sand to coarse sand | 4/28/97 | 25 | Pumping rate is based on an average of variable pumping rates. |
| Hidden Hollow Landfill EW-4 | | 78 | 51-72 | m | 45 | obs. well 1 (12ft) | no | 4,200 | 21 | 200 | 0.06 | 4.7 | constant rate pump-bailer test, Nueman Method | 1 | fine sand to coarse sand | 4/28/97 | 25 | Pumping rate is based on an average of variable pumping rates. |
| Hidden Hollow Landfill EW-4 | | 78 | 51-73 | m | 45 | obs. well 2 (80) | no | 21,000 | 22 | 955 | 0.002 | 4.7 | constant rate pump-bailer test, Nueman Method | 1 | fine sand to coarse sand | 4/28/97 | 25 | Pumping rate is based on an average of variable pumping rates. |
| Allied Seed Coop MW-1 | 3N2W | 21.5 | 5.0-20.0 | s | 6 | pumping well | no | 1,491 | 11.5 | 130 | *** | 3.8 | constant rate pump test, Jacobs Semi-log Drawdown Method | 1 | fine sand | 7/16/91 | 26 | Short duration pump test with recovery data. |
| Mark Lynn Stock Water Well | 5N1W | 429 | 165-300 | m | 172 | pumping well | no | 77,000 | 135 | 570 | *** | *** | water level recovery test, Jacobs Semi-log Drawdown Method | 120 | sand and gravel | 10/17/94 | 27 | Domestic pump was pumping intermittently during test. |
| Mark Lynn Stock Water Well | 5N1W | 429 | 165-300 | m | 172 | obs. well (275ft) | no | 108,000 | 135 | 800 | 0.01 | *** | water level recovery test, Jacobs Semi-log Drawdown Method | 120 | sand and gravel | 10/17/95 | 27 | Domestic pump was pumping intermittently during test. |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|------------------------------------|----------|----------------------------|-------------------------|--------------------------|--------------------|-------------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|---|
| Westpark Commercial Center Well 9 | | 45 | 25-45 | m | ? | pumping well | no | 143,100 | 30 | 4,770 | 0.03 | *** | *** | 10 | gravel | 9/1988 | 28 | Several monitoring wells are located at the site. |
| N. Fivemile Extraction Well FMEW-2 | | 67 | 12.0-65.0 | m | 82 | pumping well | late | 86,730 | 23 | 3,771 | 0.115 | 1.5 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | gravel | 11/16/95 | 29 | Some fluctuation in Q was noted. Specific capacity value is likely attributed to 10% well efficiency. |
| N. Fivemile Extraction Well FMEW-2 | | 67 | 12.0-65.0 | m | 82 | obs. well 1 (125) | early | 696,388 | 23 | 30,278 | 0.009 | 1.5 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | gravel | 11/16/95 | 29 | Some fluctuation in Q was noted. Specific capacity value is likely attributed to 10% well efficiency. |
| N. Fivemile Extraction Well FMEW-2 | | 67 | 12.0-65.0 | m | 82 | obs. well 1 (125) | late | 111,751 | 23 | 4,859 | 0.185 | 1.5 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | gravel | 11/16/95 | 29 | Some fluctuation in Q was noted. Specific capacity value is likely attributed to 10% well efficiency. |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|------------------------------------|----------|----------------------------|-------------------------|--------------------------|--------------------|--------------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|---|
| N. Fivemile Extraction Well FMEW-2 | | 67 | 12.0-65.0 | m | 82 | obs. well 2 (157) | early | 404,668 | 23 | 17,594 | 0.006 | 1.5 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | gravel | 11/16/95 | 29 | Some fluctuation in Q was noted. Specific capacity value is likely attributed to 10% well efficiency. |
| N. Fivemile Extraction Well FMEW-2 | | 67 | 12.0-65.0 | m | 82 | obs. well 2 (157) | late | 123,644 | 23 | 5376 | 0.053 | 1.5 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | gravel | 11/16/95 | 29 | Some fluctuation in Q was noted. Specific capacity value is likely attributed to 10% well efficiency. |
| N. Fivemile Extraction Well FMEW-2 | | 67 | 12.0-65.0 | m | 82 | obs. well 3 (168)) | late | 169,870 | 23 | 7386 | 0.027 | 1.5 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | gravel | 11/16/95 | 29 | Some fluctuation in Q was noted. Specific capacity value is likely attributed to 10% well efficiency. |
| N. Fivemile Extraction Well FMEW-2 | | 67 | 12.0-65.0 | m | 82 | obs. well 4 (335) | early | *** | 23 | *** | *** | 1.5 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | gravel | 11/16/95 | 29 | Some fluctuation in Q was noted. Specific capacity value is likely attributed to 10% well efficiency. |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|------------------------------------|----------|----------------------------|-------------------------|--------------------------|--------------------|-------------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|--|------------------|-----------|------------|-----------|---|
| N. Fivemile Extraction Well FMEW-2 | | 67 | 12.0-65.0 | m | 82 | obs. well 4 (335) | late | 165,981 | 23 | 7217 | 0.079 | 1.5 | constant rate pump test, Jacobs Semi-log Drawdown Method | 24 | gravel | 11/16/95 | 29 | Some fluctuation in Q was noted. Specific capacity value is likely attributed to 10% well efficiency. |
| Caldwell Geothermal Well 1 | | | | m | 1000 | obs. well | no | 10,472 | 23 | 455 | 2E-04 | 38.5 | water level recovery test, Theis Drawdown Test Method | 3.9 | ? | 8/23/89 | 30 | 5 aquifer test periods were completed |
| Oregon Trail Well | 3N3E | 838 | | | | pumping well | | 9,000 | 800 | 11 | *** | | constant rate pump test, Theis Drawdown Test Method | 720 | | 1/13/92 | 31 | |
| Terteling Production Well | 3N2E | 642 | 342-632 | | | obs. well | | 31,000 | 300 | 103 | 2E-04 | | constant rate pump test, Theis Drawdown Test Method | 720 | | 1/13/92 | | |
| Centennial Production Well | 3N2E | 416 | | | | obs. well | | 31,000 | 800 | 39 | 2E-04 | | water level recovery test, Theis Drawdown Test Method | 720 | | 1/13/92 | 31 | Observation well for Oregon Trail 30 day pump test |

| PUMPING WELL NAME | LOCATION | DEPTH OF PUMPING WELL (FT) | COMPLETION INTERVAL(FT) | Multiple or Single Well? | PUMPING RATE (gpm) | MULTIPLE WELLS | MULTIPLE TIMES | TRANS-MISSIVITY (gpd/ft) | Assumed Aquifer Thickness (ft) | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | STORATIVITY | SPECIFIC CAPACITY(gpm/ft) | METHOD | DURATION (hours) | LITHOLOGY | START DATE | REFERENCE | COMMENTS |
|-----------------------------------|-----------|----------------------------|-------------------------|--------------------------|--------------------|----------------|----------------|--------------------------|--------------------------------|---|-------------|---------------------------|---|------------------|-----------|------------|-----------|--|
| Gowen Production Well | 2N2E | 702 | 375-507 | | | obs. well | | 45,000 | 125 | 360 | 0.001 | | water level recovery test, Theis Drawdown Test Method | 720 | | 1/13/92 | 31 | Observation well for Oregon Trail 30 day pump test |
| Micron Test Well | 2N3E | 855 | 629-845 | | | obs. well | | 480,000 | 215 | 2,233 | 0.002 | | water level recovery test, Theis Drawdown Test Method | 720 | | 1/13/92 | 31 | Observation well for Oregon Trail 30 day pump test |
| Columbia Test Well | 3N3E | 802 | | | | obs. well | | 30,000 | 800 | 38 | 0.003 | | water level recovery test, Theis Drawdown Test Method | | | | 31 | Observation well for Oregon Trail 30 day pump test |
| Canyon Co Drainage District No. 4 | 5N4W28CC1 | | | | 1030 | | | | | | 0.025 | | | | | 6/53 | 32 | |
| Pioneer Irrigation District | 4N3W25DA1 | | | | 1550 | | | | | 5,000 | 0.004 | | | | | 10/53 | 32 | |
| Pioneer Irrigation District | 4N3W3BB1 | | | | 2110 | | | | | 23,000 | 0.23 | | | | | 11/53 | 32 | |

| COMMENTS | REFERENCE | START DATE | LITHOLOGY | DURATION (hours) | METHOD | SPECIFIC CAPACITY (gpm/ft) | STORATIVITY | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | Assumed Aquifer Thickness (ft) | TRANS-MISSIVITY (gpd/ft) | MULTIPLE TIMES | MULTIPLE WELLS | PUMPING RATE (gpm) | Multiple or Single Well? | COMPLETION INTERVAL(FT) | DEPTH OF PUMPING WELL (FT) | LOCATION | PUMPING WELL NAME |
|----------|-----------|------------|-----------|------------------|--------|----------------------------|-------------|---|--------------------------------|--------------------------|----------------|----------------|--------------------|--------------------------|-------------------------|----------------------------|-----------|-----------------------------|
| | 32 | 10/53 | | | | | 0.006 | 25,000 | | | | | 2,175 | | | | 3N3W11DA1 | Pioneer Irrigation District |
| | 32 | 10/53 | | | | | 0.0006 | | | | | | 1,480 | | | | 3N2W8CC1 | Pioneer Irrigation District |
| | 32 | 2/53 | | | | | 0.0001 | 5,900 | | | | | 1,830 | | | | 3N2W9DD4 | Amalgamated Sugar |
| | 32 | 11/53 | | | | | 0.003 | 3,700 | | | | | 1,060 | | | | 3N1W7BB1 | Pioneer Irrigation District |
| | 32 | 9/53 | | | | | 0.004 | 18,000 | | | | | 2,900 | | | | 2N1W7BC4 | US Bureau of Reclamation |
| | 32 | 3/51 | | | | | | 300 | | | | | 480 | | | | 4N1W13DC1 | State Fish Hatchery |

| COMMENTS | REFERENCE | START DATE | LITHOLOGY | DURATION (hours) | METHOD | SPECIFIC CAPACITY (gpm/ft) | STORATIVITY | HYDRAULIC CONDUCTIVITY (gpd/ft ²) | Assumed Aquifer Thickness (ft) | TRANS-MISSIVITY (gpd/ft) | MULTIPLE TIMES | MULTIPLE WELLS | PUMPING RATE (gpm) | Multiple or Single Well? | COMPLETION INTERVAL(FT) | DEPTH OF PUMPING WELL (FT) | LOCATION | PUMPING WELL NAME |
|----------|-----------|------------|-----------|------------------|--------|----------------------------|-------------|---|--------------------------------|--------------------------|----------------|----------------|--------------------|--------------------------|-------------------------|----------------------------|-----------|--------------------------------|
| | 32 | 3/51 | | | | | 0.001 | 660 | | | | | 600 | | | | 4N1W13DC2 | State Fish Hatchery |
| | 32 | 11/53 | | | | | 0.001 | 900 | | | | | 125 | | | | 3N1E5AB1 | US Bureau of Reclamation |
| | 32 | 11/53 | | | | | 0.006 | 2,400 | | | | | 600 | | | | 3N1E5AB1 | US Bureau of Reclamation |
| | 32 | 9/53 | | | | | 0.00007 | 1,500 | | | | | 980 | | | | 3N1E36AD2 | M.S. Ayres |
| | 32 | 11/53 | | | | | 0.43 | 2,500 | | | | | 1,380 | | | | 3N2E25BB1 | Ada Co Drainage District No. 2 |

References for Aquifer Test Data

1. Montgomery, J. M., Sept. 1992, New Playground Well, City of Boise Project Closeout Report, JMM, Boise, Idaho.
2. Montgomery, J. M., Sept. 1992, New Diamond Well, City of Boise Project Closeout Report, JMM, Boise, Idaho.
3. CH2M Hill, June 1991, Results of The 30-Day Pumping Test and Aquifer Analysis Report, Prepared For Floating Hills, Inc., Boise, Idaho.
4. Anderson & Kelly Consultants, July 1992, Effects Of Pumping Boise Water Corporation Broadway Well Report, Prepared for Boise Water Corporation, Boise, Idaho.
5. Scanlan, T. M., June 3, 1994, Personnel memorandum to Mr. Gary Madenford—Redwood Creek Subdivision Well No.1 Report, Scanlan Engineering, Boise, Idaho.
6. Anderson, K. E., October 1962, Willow Lane Well Field Report, Prepared for Boise Water Corporation, Boise, Idaho.
7. Dittus, R., June 6, 1996, United Water Idaho Veterans Well Fact Sheet, United Water, Boise, Idaho.
8. Dittus, R., June 6, 1996, United Water Idaho Gary Lane Well Fact Sheet, United Water, Boise, Idaho.
9. Naylor, P. N., February 1992, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
10. Scanlan, T. M., June 24, 1991, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
11. Mills, D. E., May 30, 1991, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
12. Mills, D. E., March 14, 1991, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
13. Mills, D. E., October 24, 1990, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
14. Scanlan, T. M., June 18, 1990, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
15. Scanlan, T. M., April 30, 1990, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
16. Scanlan, T. M., February 28, 1990, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
17. Scanlan, T. M., February 16, 1990, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.

18. Scanlan, T. M., February 16, 1990, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
19. Scanlan, T. M., July 28, 1989, J. R Flat Well Test, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
20. Scanlan, T. M., April 6, 1989, Testing of the New Long Meadow Well, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
21. Scanlan, T. M., April 6, 1989, Testing of Swift Well No. 2, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
22. Scanlan, T. M., September 19, 1989, Londoner Well–Deep Zone Test, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
23. Scanlan, T. M., April 4 1988, River Run Well Test Summary, Boise Water Corporation Well Tests 1987–1992, Scanlan Engineering, Boise, Idaho.
24. Mikels, F. C., November 7, 1952, Report on Hydrogeological Survey for Boise Water Corporation, Ranney Method Water Supplies, Inc., Boise, Idaho.
25. CH2M Hill, Inc., March 1998, Well Construction and Hydrogeological Characterization of the Groundwater Remediation Site Ada County Landfill, Boise, Idaho.
26. Backe, M. A., June 13, 1991, Personnel memorandum to Craig Ranke of Sweet Edwards/EMCON, Inc., Special Resource Management, Boise, Idaho.
27. Scanlan, T. M., February 16, 1990, Personnel memorandum to Ms. Dana Hofstetter–Aquifer Test Results for Mark Lynn Ranch on Willow Creek, Scanlan Engineering, Boise, Idaho.
28. Special Resource Management, January 13, 1989, Groundwater Remedial Action Plan for the Westpark Commercial Center, Boise, Idaho.
29. Taraszki, R. G., March 15, 1996, Results of Aquifer Testing and Preliminary Capture Analysis North Five Mile Road Area Groundwater Extraction System, Harding Lawson Associates, Boise, Idaho.
30. Ralston, D. R., October 1989, Analysis of August 1989 Aquifer Tests, Caldwell Geothermal Wells, Prepared for J. R. Simplot Co., Moscow, Idaho.
31. Squires, E., Wood, S. H., Osiensky, J. L., and Dittus, R. D., October 1993, Groundwater Conditions and Hydraulic Testing of the Boise Fan Aquifer of Southeast Boise River Valley, Ada County, Idaho.
32. Nace, R. L., West, S. W., and Mower, R. W. 1957. Feasibility of Ground-Water Features of the Alternate Plan for the Mountain Home Project Idaho. U.S. Geological Survey Water Supply Paper 1376.

Appendix C. CONSTRUCTION DETAILS FOR DEDICATED, MULTI-LEVEL PIEZOMETERS

*** Construction diagrams for TVHP monitoring wells provided under separate cover. ***

Appendix D. CONSTRUCTION AND MEASUREMENT DETAILS FOR MASS MEASUREMENT WELLS

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|-------------|-----------|-----------|
| 01N 01E 03CCC1 | 432644116195401 | 43.44556 | -116.3317 | 2782 | I | 27-288 | 288 | X | X | X | X | X | X | X |
| 01N 01E 05CCD1 | 432641116221201 | 43.44473 | -116.37 | 2817 | I | 279-440 | 440 | X | X | X | | X | X | |
| 01N 01E 12DAA1 | 432613116162901 | 43.43695 | -116.2747 | 2860 | U | 232-312 | 322 | X | X | | | | | |
| 01N 01E 16ACC1 | 432525116203301 | 43.42361 | -116.3425 | 2820 | H | 38-386 | 386 | X | X | X | X | X | X | X |
| 01N 01E 19ADB1 | 432442116223901 | 43.41167 | -116.3775 | 2880 | I | 18-440 | 440 | X | X | X | X | X | X | X |
| 01N 01E 25DBA1 | 432336116164601 | 43.39333 | -116.2794 | 2849 | I | 36-530 | 530 | X | | | | | | |
| 01N 01E 33AAD1 | 432301116200401 | 43.38361 | -116.3344 | 2865 | I | 19-618 | 618 | | | X | X | X | X | X |
| 01N 01W 01BDB1 | 432717116242501 | 43.45472 | -116.4069 | 2800 | I | 183-325 | 401 | | | X | | X | X | X |
| 01N 01W 02ADC1 | 432707116250501 | 43.45195 | -116.4181 | 2850 | I | 245-455 | 455 | X | | | | | | |
| 01N 01W 07BCC1 | 432618116304401 | 43.43834 | -116.5122 | 2820 | I | 14-408 | 408 | | | X | X | X | X | |
| 01N 01W 07CAB1 | 432613116302601 | 43.43695 | -116.5072 | 2780 | I | 12-461 | 461 | X | | | | | | |
| 01N 01W 07DBB1 | 432613116300901 | 43.4375 | -116.5028 | 2800 | I | 18-591 | 591 | | X | | | | | |
| 01N 01W 15DAA1 | 432520116260401 | 43.42222 | -116.4344 | 2890 | I | 293-541 | 541 | X | | | | | | |
| 01N 01W 18CCC1 | 432500116303901 | 43.41667 | -116.5108 | 2730 | H | 484-520 | 520 | | | X | X | X | X | X |
| 01N 01W 22DDD1 | 432407116260001 | 43.40195 | -116.4333 | 2888 | I | 345-502 | 502 | | | X | X | X | X | |
| 01N 01W 24AAA1 | 432452116234201 | 43.41445 | -116.395 | 2880 | I | 20-366 | 366 | X | X | X | X | X | | |
| 01N 01W 27ADD1 | 432344116255901 | 43.39556 | -116.4331 | 2904 | U/I | 18-365 | 500 | X | X | X | X | X | X | X |
| 01N 01W 30AAD1 | 432351116293701 | 43.3975 | -116.4936 | 2740 | I | 21-415 | 415 | | | X | X | X | X | X |
| 01N 02E 04BBA1 | 432729116134201 | 43.45806 | -116.2283 | 3005 | I/M | 488-615 | 625 | X | X | X | | | | |
| 01N 02E 06BAA1 | 432732116155501 | 43.45889 | -116.2653 | 2910 | I/U | 448-510 | 535 | X | X | X | X | X | X | X |
| 01N 02E 08ADA2 | 432620116140102 | 43.43889 | -116.2336 | 2930 | H | 375-400 | 400 | X | X | X | X | X | X | |
| 01N 02W 04DDC1 | 432645116343001 | 43.44584 | -116.575 | 2700 | I | 450-685 | 685 | X | X | X | X | X | X | X |
| 01N 02W | 432708116353901 | 43.45222 | -116.5942 | 2675 | I | 415-720 | 720 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|--------------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|-------------|-----------|-----------|
| 05ADD1 | | | | | | | | | | | | | | |
| 01N 02W 06ADD1 | 432709116365101 | 43.4525 | -116.6142 | 2728 | I | 596-720 | 720 | X | X | X | | X | X | X |
| 01N 02W 09DDD2 | 432554116342101 | 43.43167 | -116.5725 | 2665 | H | - | 252 | X | X | X | X | X | X | X |
| 01N 02W 10DAA1 | 432613116331001 | 43.43695 | -116.5528 | 2660 | H | 19-150 | 150 | X | X | X | X | X | X | X |
| 01N 02W 17DDA1 | 432510116353301 | 43.41945 | -116.5925 | 2718 | I | 370-565 | 565 | X | X | X | X | | | |
| 01N 02W 35CDB1 | 432232116330401 | 43.37555 | -116.5511 | 2600 | H | 35-213 | 213 | | | X | X | X | X | X |
| 01N 03W 02CCB1 | 432652116401701 | 43.44778 | -116.6714 | 2730 | H | 500-1000 | 1000 | | | X | X | X | X | X |
| 01N 03W 03DDD1 | 432646116402101 | 43.44611 | -116.6725 | 2715 | H | 331-731 | 731 | X | X | X | X | X | X | X |
| 01N 03W 06DDC1 | 432640116440701 | 43.44445 | -116.7353 | 2240 | H | 416-560 | 560 | X | X | X | X | X | X | X |
| 01N 03W 13AAA1 | 432548116375701 | 43.43 | -116.6325 | 2688 | I | 220-607 | 607 | X | X | X | X | X | X | X |
| 01N 03W 25AAA1 | 432403116375601 | 43.40083 | -116.6322 | 2740 | H | 599-710 | 710 | | | X | X | X | X | X |
| 01N 04E 13CCCB1 | 432500115560301 | 43.41667 | -115.9342 | 3530 | H | 38-110 | 110 | X | X | | | | | |
| 01N 04E 28CAC1 | 432326115591601 | 43.39167 | -115.9889 | 3360 | N | 500-752 | 763 | X | X | | | X | X | X |
| 01N 05E 17BAB1 | 432539115532201 | 43.4275 | -115.8894 | 3660 | U | 53-68 | 82 | X | X | | | | | |
| 01S 01W 05BAC1 | 432209116282501 | 43.36916 | -116.4736 | 2738 | I | 9-370 | 370 | | | X | X | X | X | X |
| 01S 01W 19AAB1 | 431944116294401 | 43.32889 | -116.4956 | 2615 | I | 225-383 | 388 | | | X | X | X | X | |
| 01S 01W 29CBC1 | 431816116292801 | 43.30444 | -116.4911 | 2575 | I | 200-282 | 295 | | | X | X | X | X | |
| 01S 01W 29CBD1 | 431816116291401 | 43.30444 | -116.4872 | 2590 | I | 259-279 | 300 | | | X | X | X | X | |
| 01S 01W 30AAB1 | 431848116295001 | 43.31333 | -116.4972 | 2543 | H | 299-400 | 400 | | | X | X | X | X | |
| 01S 01W 30BAB1 | 431851116301101 | 43.31417 | -116.5031 | 2512 | H | 198-300 | 300 | | X | X | X | X | X | X |
| 01S 02W 03DBC1 | 432147116333601 | 43.36305 | -116.56 | 2410 | H | 32-44 | 44 | X | X | X | | | | |
| 01S 02W 08DCD1 | 432040116354701 | 43.34444 | -116.5964 | 2350 | H | 120-170 | 180 | | | X | X | X | X | X |
| 01S 02W 13ABBC1 | 432031116311201 | 43.34194 | -116.52 | 2530 | H | 137-183 | 183 | | | X | X | X | X | |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|-------------|-----------|-----------|
| 01S 02W 13ABBC2 | 432031116311202 | 43.34194 | -116.52 | 2530 | H | 18-300 | 300 | | | X | X | X | X | X |
| 01S 02W 14CCC2 | 431948116330001 | 43.33 | -116.55 | 2395 | H | - | 235 | X | X | X | X | X | X | X |
| 01S 02W 15ABA1 | 432037116332101 | 43.34361 | -116.5558 | 2450 | H | 220-420 | 420 | | | X | X | X | X | X |
| 01S 02W 24CBA1 | 431917116313301 | 43.32139 | -116.5258 | 2490 | I | 127-190 | 190 | | X | X | X | X | X | X |
| 01S 04E 03ADB1 | 432202115573001 | 43.36722 | -115.9583 | 3375 | U | - | 530 | X | X | X | X | X | X | X |
| 02N 01E 01BCBC1 | 433230116173301 | 43.54167 | -116.2925 | 2739 | H | - | 145 | X | X | X | X | X | X | |
| 02N 01E 02BACB1 | 433242116182601 | 43.545 | -116.3072 | 2729 | I | 169-184 | 184 | X | X | X | X | X | X | X |
| 02N 01E 05CBDC1 | 433220116222001 | 43.53583 | -116.3708 | 2735 | H | 236-242 | 242 | X | X | X | | | | |
| 02N 01E 07CBBC1 | 433124116233501 | 43.52361 | -116.3917 | 2670 | H/I | 135-145 | 145 | X | X | X | X | X | X | |
| 02N 01E 08ACC1 | 433129116214401 | 43.52472 | -116.3622 | 2728 | H | 254-260 | 260 | X | X | X | X | X | X | |
| 02N 01E 12CDB1 | 433127116170101 | 43.52083 | -116.2867 | 2885 | H | - | 290 | X | X | X | X | X | X | |
| 02N 01E 15ABA1 | 433101116191301 | 43.51694 | -116.3203 | 2766 | H | 240-243 | 243 | X | X | X | X | | | |
| 02N 01E 22DCA1 | 432931116190701 | 43.49194 | -116.3186 | 2836 | I | 360-440 | 444 | X | X | | | | | |
| 02N 01E 23BAD1 | 432959116181601 | 43.49972 | -116.3045 | 2910 | I | 332-382 | 386 | X | X | X | X | | | |
| 02N 01E 26BBC1 | 432911116184601 | 43.48639 | -116.3128 | 2840 | H | 298-300 | 300 | X | X | X | X | X | X | |
| 02N 01E 29BDB1 | 432915116222001 | 43.48417 | -116.3678 | 2730 | H | 19-215 | 215 | | | X | X | X | X | X |
| 02N 01E 29DCA1 | 432834116213801 | 43.47611 | -116.3606 | 2742 | H | 19-130 | 130 | X | X | X | X | X | X | |
| 02N 01E 31DDC1 | 432734116223901 | 43.45945 | -116.3775 | 2748 | H | 225-248 | 248 | X | X | X | X | X | X | X |
| 02N 01E 33CAC1 | 432748116205201 | 43.46333 | -116.3478 | 2758 | H | 16-224 | 224 | X | X | X | X | X | X | X |
| 02N 01E 33CCA2 | 432746116210202 | 43.46278 | -116.3506 | 2752 | H | - | 0 | X | X | | | | | |
| 02N 01E 35BBC1 | 432822116183801 | 43.47278 | -116.3106 | 2825 | I | 230-340 | 340 | X | X | X | X | X | X | X |
| 02N 01E 36BBB1 | 432825116173501 | 43.47361 | -116.2931 | 2867 | S/U | 300-305 | 305 | X | X | X | X | X | X | X |
| 02N 01W | 433246116255401 | 43.54611 | -116.4317 | 2658 | H | 100-104 | 104 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|--------|-----------|-----------|
| 02BBA1 | | | | | | | | | | | | | | |
| 02N 01W 03ABB1 | 433246116262701 | 43.54611 | -116.4408 | 2650 | H | 299-306 | 306 | X | X | X | X | X | X | X |
| 02N 01W 07AAB1 | 433155116294401 | 43.53194 | -116.4956 | 2570 | H | 30-126 | 126 | | | X | | X | X | X |
| 02N 01W 07BBC1 | 433145116304301 | 43.52917 | -116.5119 | 2548 | H | 98-102 | 103 | X | X | X | X | X | X | X |
| 02N 01W 08BBBA1 | 433155116292501 | 43.53194 | -116.4903 | 2570 | H | 33-94 | 94 | | | X | X | X | X | X |
| 02N 01W 09ADA1 | 433140116271401 | 43.52778 | -116.4539 | 2600 | H | - | 37 | X | X | X | X | X | X | X |
| 02N 01W 09ADA2 | 433140116271402 | 43.52778 | -116.4539 | 2600 | U | 192-197 | 197 | | | X | X | | X | X |
| 02N 01W 10ABB1 | 433155116263101 | 43.53194 | -116.4419 | 2640 | H | 128-130 | 130 | X | X | X | X | X | X | X |
| 02N 01W 11ADA1 | 433143116245101 | 43.52861 | -116.4142 | 2685 | I | 64-130 | 190 | X | X | X | X | X | X | X |
| 02N 01W 12BAA1 | 433154116242601 | 43.53167 | -116.4072 | 2675 | H | 93-95 | 95 | X | X | X | X | X | X | X |
| 02N 01W 13BAB1 | 433102116242301 | 43.51722 | -116.4064 | 2683 | H | - | 96 | X | X | X | X | X | X | X |
| 02N 01W 15ADC1 | 433038116261201 | 43.51056 | -116.4367 | 2675 | H | 95-96 | 96 | X | X | | | | | |
| 02N 01W 23ACC1 | 432946116251401 | 43.49611 | -116.4206 | 2691 | H | - | 110 | X | X | X | X | X | X | |
| 02N 01W 27BCC1 | 432853116270901 | 43.48139 | -116.4525 | 2689 | H | 400-410 | 410 | X | X | X | X | X | X | X |
| 02N 01W 29DCC1 | 432828116285001 | 43.47445 | -116.4806 | 2670 | H | 242-250 | 250 | | | X | X | X | X | X |
| 02N 01W 32CBB1 | 432757116292601 | 43.46584 | -116.4906 | 2685 | I | 150-234 | 240 | X | X | X | X | X | X | X |
| 02N 01W 35BDC1 | 432800116253901 | 43.46667 | -116.4275 | 2790 | I | 155-210 | 218 | X | X | X | X | X | X | X |
| 02N 02E 01BAB1 | 433244116095501 | 43.54556 | -116.1653 | 2921 | P | 375-507 | 702 | | | X | X | X | | |
| 02N 02E 02BBC1 | 433235116112801 | 43.54306 | -116.1911 | 2915 | U | 114-805 | 805 | X | X | | | | | |
| 02N 02E 02BBC2 | 433233116113201 | 43.5425 | -116.1922 | 2911 | P/P | 435-500 | 567 | | | | | | X | X |
| 02N 02E 04CAA1 | 433216116132201 | 43.53778 | -116.2228 | 2887 | I | - | 0 | | | | | X | X | X |
| 02N 02E 04CBA1 | 433218116134201 | 43.53833 | -116.2283 | 2884 | I | 300-400 | 555 | | | | | X | X | |
| 02N 02E 04CBB1 | 433218116135301 | 43.53889 | -116.2319 | 2880 | H/S | 332-353 | 353 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|--------|-----------|-----------|
| 02N 02E 06CCC1 | 433157116162301 | 43.5325 | -116.2731 | 2768 | H | - | 0 | | X | X | X | X | X | X |
| 02N 02E 06CCC2 | 433200116162001 | 43.53333 | -116.2722 | 2770 | H | 185-195 | 195 | X | X | | | | | |
| 02N 02E 07CBC1 | 433119116161601 | 43.52195 | -116.2711 | 2920 | H | 448-460 | 460 | X | X | X | X | X | X | X |
| 02N 02E 08AAD1 | 433144116135801 | 43.52889 | -116.2328 | 2873 | I | 362-640 | 640 | X | X | | | | | |
| 02N 02E 12AAC1 | 433143116092001 | 43.52833 | -116.1531 | 3035 | H | 417-503 | 503 | X | X | X | X | | | |
| 02N 02E 17AAD1 | 433050116140301 | 43.51389 | -116.2342 | 3139 | I | 537-860 | 880 | X | X | | | | | |
| 02N 02E 21BAB1 | 433007116133501 | 43.50195 | -116.2264 | 3142 | I/H | 523-800 | 800 | X | X | | | | | |
| 02N 02E 22BBB1 | IDWR-S2000-01 | 43.50195 | -116.2083 | 3175 | P | 691-912 | 930 | | | X | | X | X | X |
| 02N 02E 31BCA1 | 432812116161401 | 43.47 | -116.2706 | 2920 | H | 294-395 | 401 | X | X | X | X | X | X | |
| 02N 02E 32DBA1 | 432753116141901 | 43.46472 | -116.2386 | 2985 | I | 492-559 | 564 | X | X | | | | | |
| 02N 02E 34CCD1 | 432732116123401 | 43.45889 | -116.2094 | 3040 | H | 484-504 | 504 | X | X | X | X | X | X | X |
| 02N 02W 02CACC1 | 433211116324401 | 43.53639 | -116.5456 | 2550 | H | 20-73 | 73 | X | X | X | X | X | X | X |
| 02N 02W 05ABA1 | 433243116355401 | 43.545 | -116.5981 | 2555 | H | 178-180 | 180 | X | X | X | X | X | X | X |
| 02N 02W 07CBC1 | 433116116375501 | 43.52111 | -116.6319 | 2555 | H | - | 122 | X | X | X | X | X | X | X |
| 02N 02W 09ACC1 | 433132116345001 | 43.52555 | -116.5806 | 2602 | P | 178-194 | 194 | X | X | X | X | X | X | |
| 02N 02W 10CAA2 | 433128116335001 | 43.52444 | -116.5639 | 2575 | H | 178-183 | 183 | X | X | X | X | X | X | X |
| 02N 02W 12ADCD1 | 433129116305301 | 43.52472 | -116.5147 | 2570 | H | - | 76 | | | X | X | X | X | X |
| 02N 02W 20CBB1 | 432942116364101 | 43.495 | -116.6114 | 2563 | P/H | 155-177 | 177 | X | X | X | X | X | X | X |
| 02N 02W 22CCA1 | 432928116340601 | 43.49111 | -116.5683 | 2640 | H | 205-207 | 208 | X | X | X | X | X | X | X |
| 02N 02W 28DDD1 | 432826116342001 | 43.47389 | -116.5722 | 2610 | H | 99-135 | 135 | X | X | | | | | |
| 02N 02W 29BCC1 | 432852116363601 | 43.48111 | -116.61 | 2621 | I | 176-255 | 255 | X | X | X | X | X | X | X |
| 02N 02W 31CBA1 | 432801116374401 | 43.46695 | -116.6289 | 2705 | I | 697-920 | 920 | X | X | X | X | X | X | X |
| 02N 02W | 432743116362101 | 43.46194 | -116.6058 | 2700 | H | 225-240 | 240 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | Spring | 2000 Fall | 2001 Fall |
|-------------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|--------|-----------|-----------|
| 32CDB1 | | | | | | | | | | | | | | |
| 02N 03E 02CDD1 | 433157116035201 | 43.5325 | -116.0644 | 3180 | H | 78-470 | 470 | X | X | | | | | |
| 02N 03E 06AAB1 | 433246116081701 | 43.54389 | -116.1339 | 2960 | I | 475-1001 | 1001 | X | X | | | | | |
| 02N 03E 06BCC2 | 433221116090702 | 43.53917 | -116.1519 | 3015 | H/P | 335-460 | 460 | X | X | X | X | X | X | X |
| 02N 03E 06DCA1 | 433202116082001 | 43.53389 | -116.1389 | 3065 | U | 609-845 | 855 | X | X | X | X | X | X | X |
| 02N 03E 07BAC1 | IDWR-S2000-03 | 43.52806 | -116.1461 | 3064 | O | 553-580 | 580 | | | X | X | X | X | X |
| 02N 03E 07CDA1 | 433112116084501 | 43.52 | -116.1458 | 3058 | U/H | - | 549 | | | X | X | X | X | X |
| 02N 03E 07DBB1 | 433137116084301 | 43.52333 | -116.1431 | 3059 | Z | 551-561 | 561 | | | X | X | X | X | X |
| 02N 03E 07DBB2 | 433137116084601 | 43.52306 | -116.1497 | 3059 | Z | 801-811 | 811 | | | X | X | X | X | X |
| 02N 03E 09BAA2 | 433150116061802 | 43.53056 | -116.105 | 3140 | U/H | 499-522 | 522 | | | X | X | X | X | X |
| 02N 03E 09BCA2 | 433139116063402 | 43.5275 | -116.1094 | 3135 | H | 599-620 | 620 | | | | X | X | X | X |
| 02N 03E 11ACC1 | 433132116034701 | 43.52555 | -116.0631 | 2838 | P/R | 40-100 | 100 | X | X | X | X | X | X | X |
| 02N 03E 18BAC1 | 433050116085001 | 43.51389 | -116.1472 | 3070 | H | 605-635 | 642 | X | X | X | X | | | |
| 02N 03W 06DBA1 | 433217116441301 | 43.53806 | -116.7369 | 2600 | H | 239-247 | 247 | X | X | X | X | X | X | X |
| 02N 03W 13BCB1 | 433044116390601 | 43.51222 | -116.6517 | 2445 | I | 211-310 | 310 | | | X | X | X | X | X |
| 02N 03W 22DDC1 | 432919116403701 | 43.48861 | -116.6769 | 2750 | I | 400-603 | 603 | X | X | X | X | X | X | X |
| 02N 03W 36DAD1 | 432753116375701 | 43.46472 | -116.6325 | 2785 | H | 364-523 | 523 | X | X | | | | | |
| 02N 04E 29ADB1 | 432900115595301 | 43.48333 | -115.9981 | 3680 | H | 20-217 | 227 | X | X | | | | | |
| 02N 04E 34BCB1 | 432805115582301 | 43.46806 | -115.9731 | 3700 | I | 135-260 | 260 | X | X | | | | | X |
| 02N 04W 13ACD1 | 433035116452401 | 0 | 0 | 2315 | H | 97-205 | 205 | | | X | X | X | X | |
| 02N 04W 25CAD1 | 432840116460101 | 43.47778 | -116.7669 | 2260 | H | 99-121 | 121 | | | X | | X | X | |
| 02S 01E 23ADD1 | 431402116173701 | 43.23389 | -116.2936 | 3155 | U/I | 615-816 | 816 | | | | | X | X | X |
| 03N 01E 01DAA1 | IDWR-S2000-04 | 43.62666 | -116.2744 | 2690 | U/I | 40-417 | 420 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|--------|-----------|-----------|
| 03N 01E 01DAA2 | 433736116162802 | 43.62667 | -116.2744 | 2690 | I | 265-420 | 420 | X | X | X | X | X | X | X |
| 03N 01E 06BBAB1 | 433801116232401 | 43.63361 | -116.39 | 2590 | H | 63-64 | 64 | X | X | X | X | X | X | X |
| 03N 01E 06DDD1 | 433716116223001 | 43.62111 | -116.375 | 2606 | H | 81-83 | 83 | X | X | X | X | X | X | X |
| 03N 01E 08DCDC1 | 433619116214001 | 43.60528 | -116.3611 | 2650 | H | - | 67 | X | X | X | X | X | X | X |
| 03N 01E 10BDA1 | 433651116192501 | 43.61417 | -116.3236 | 2650 | H | 99-100 | 100 | X | X | X | X | X | X | X |
| 03N 01E 12BCD1 | 433646116172101 | 43.61278 | -116.2892 | 2690 | I | 77-87 | 87 | X | X | X | X | X | X | X |
| 03N 01E 13BDB1 | 433558116171701 | 43.59945 | -116.2881 | 2735 | H | 91-97 | 97 | X | X | X | X | X | X | X |
| 03N 01E 14AAC2 | 433605116174602 | 43.60139 | -116.2961 | 2726 | U | - | 1000 | X | X | | | X | X | X |
| 03N 01E 14AAC3 | 433605116174603 | 43.60139 | -116.2961 | 2726 | P | 318-920 | 952 | X | | X | | X | | |
| 03N 01E 15AAD1 | 433607116185201 | 43.60194 | -116.3144 | 2709 | H | 146-151 | 154 | X | X | X | X | X | X | X |
| 03N 01E 15ADD1 | 433554116184901 | 43.59833 | -116.3136 | 2701 | P | 479-565 | 565 | X | X | X | X | X | X | X |
| 03N 01E 15CBD1 | 433544116194601 | 43.59555 | -116.3294 | 2680 | H | 85-90 | 90 | X | X | X | X | X | X | X |
| 03N 01E 15CDA1 | 433537116192501 | 43.59361 | -116.3236 | 2706 | P | 301-335 | 335 | X | X | X | X | X | X | X |
| 03N 01E 16BCA1 | 433605116210001 | 43.60139 | -116.35 | 2660 | T/I | 792-877 | 902 | X | | | X | X | X | X |
| 03N 01E 17ACA1 | 433601116213701 | 43.60028 | -116.3603 | 2650 | H | 61-66 | 66 | | X | | X | | | X |
| 03N 01E 17BBB1 | 433613116222301 | 43.60361 | -116.3731 | 2620 | H | 100-105 | 105 | X | X | X | X | X | X | X |
| 03N 01E 23DDD1 | 433433116173801 | 43.57583 | -116.2939 | 2725 | Z/U | 25-443 | 446 | X | X | X | X | X | X | X |
| 03N 01E 24ADA1 | 433512116162501 | 43.58667 | -116.2736 | 2750 | H | - | 144 | X | X | X | X | X | X | X |
| 03N 01E 25BCB1 | 433417116172701 | 43.57139 | -116.2908 | 2751 | H | 103-109 | 117 | X | X | X | X | X | X | X |
| 03N 01E 27CDD1 | 433347116193101 | 43.56306 | -116.3253 | 2717 | H | 113-118 | 118 | X | X | X | X | X | X | X |
| 03N 01E 28DCDD2 | 433341116202102 | 43.56139 | -116.3392 | 2695 | H | 117-122 | 125 | X | X | X | X | X | X | X |
| 03N 01E 30DDD1 | 433347116222501 | 43.56306 | -116.3736 | 2667 | H | 84-132 | 132 | X | X | X | X | X | X | |
| 03N 01E | 433309116192401 | 43.5525 | -116.3233 | 2718 | P | 169-403 | 425 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|--------|-----------|-----------|
| 34CAA1 | | | | | | | | | | | | | | |
| 03N 01E 36DDB1 | 433256116163301 | 43.54889 | -116.2758 | 2810 | I | 46-152 | 152 | X | X | X | X | X | X | X |
| 03N 01W 03AAAA1 | 433800116255901 | 43.63334 | -116.4331 | 2555 | H | 145-155 | 156 | | | X | X | X | X | X |
| 03N 01W 03DADD1 | 433724116255801 | 43.62333 | -116.4328 | 2560 | H | 70-72 | 72 | | | X | X | X | X | X |
| 03N 01W 06CBBB1 | 433736116304201 | 43.62666 | -116.5117 | 2495 | H | 173-175 | 175 | | | X | X | X | X | X |
| 03N 01W 06DDDC1 | 433712116294001 | 43.62 | -116.4944 | 2510 | H | 69-74 | 80 | | | X | X | X | X | X |
| 03N 01W 08BDAC1 | 433648116285001 | 43.61333 | -116.4806 | 2520 | H | 140-160 | 160 | X | X | X | X | X | X | |
| 03N 01W 09AACB1 | 433701116272201 | 43.61694 | -116.4561 | 2539 | H | 94-102 | 102 | X | X | X | X | X | X | |
| 03N 01W 11BDCC1 | 433645116253801 | 43.6125 | -116.4272 | 2572 | H | 145-150 | 150 | X | X | X | X | X | X | X |
| 03N 01W 12CBBB1 | 433646116244101 | 43.61194 | -116.4114 | 2595 | I | - | 36 | X | X | X | X | X | X | X |
| 03N 01W 16DDDD1 | 433528116271101 | 43.59111 | -116.453 | 2677 | H | 183-190 | 190 | X | X | X | X | X | X | X |
| 03N 01W 18DAC1 | 433545116295201 | 43.59583 | -116.4978 | 2635 | H | 237-240 | 240 | X | X | X | X | X | X | X |
| 03N 01W 21DBCA1 | 433450116274001 | 43.58055 | -116.4611 | 2620 | H | 193-295 | 295 | | | X | X | X | X | X |
| 03N 01W 24BBDA1 | 433517116243101 | 43.58805 | -116.4086 | 2612 | H | 55-60 | 60 | X | X | X | X | X | X | X |
| 03N 01W 25DAD1 | 433354116233501 | 43.565 | -116.3931 | 2712 | H/S | 327-330 | 330 | X | X | X | X | X | X | X |
| 03N 01W 26DDDC1 | 433342116245201 | 43.56166 | -116.4144 | 2700 | H | 202-213 | 213 | X | X | X | X | X | X | X |
| 03N 01W 27CDCB1 | 433346116264901 | 43.56278 | -116.4469 | 2645 | H | - | 200 | X | X | X | X | X | X | |
| 03N 01W 31DDA1 | 433302116294101 | 43.55 | -116.4944 | 2542 | H | 31-67 | 67 | X | X | X | X | X | X | X |
| 03N 02E 03BAAD2 | 433757116121101 | 43.6325 | -116.2031 | 2712 | I | 72-77 | 78 | X | X | X | X | X | X | X |
| 03N 02E 04DAB1 | 433729116125701 | 43.62472 | -116.2158 | 2675 | I | - | 50 | X | X | X | X | X | X | X |
| 03N 02E 06DDC1 | 433713116152101 | 43.62028 | -116.2558 | 2708 | P | 568-850 | 850 | X | X | X | | X | X | X |
| 03N 02E 06DDD1 | 433710116151501 | 43.61945 | -116.2539 | 2712 | C | 94-98 | 98 | X | X | X | X | X | X | X |
| 03N 02E 06DDD2 | 433711116151501 | 43.61972 | -116.2542 | 2712 | C | 124-136 | 137 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|--------|-----------|-----------|
| 03N 02E 07DAAC1 | 433637116151901 | 43.61028 | -116.2553 | 2715 | I | 456-471 | 471 | X | X | X | X | X | X | X |
| 03N 02E 11BABD1 | 433705116110601 | 43.61806 | -116.185 | 2743 | U | 781-1220 | 1220 | X | X | X | X | X | X | X |
| 03N 02E 11DDD1 | 433619116103001 | 43.60528 | -116.175 | 2718 | H | - | 68 | X | X | X | X | X | X | X |
| 03N 02E 13BABA1 | 433614116095801 | 43.60389 | -116.1661 | 2730 | I | - | 0 | X | X | X | X | X | X | X |
| 03N 02E 14ACB2 | 433559116105201 | 43.59972 | -116.1811 | 2710 | I | 35-55 | 55 | X | X | X | X | X | X | X |
| 03N 02E 15BDB2 | 433557116122201 | 43.59917 | -116.2061 | 2700 | H/I | 78-84 | 84 | X | X | X | X | X | X | X |
| 03N 02E 15DDDD1 | 433527116113401 | 43.59083 | -116.1928 | 2719 | U/P | - | 165 | X | X | X | X | | | |
| 03N 02E 17CAD2 | IDWR-S2000-05 | 43.59444 | -116.2447 | 2727 | P | 399-612 | 650 | X | | | X | X | X | X |
| 03N 02E 18DAA1 | 433549116151301 | 43.59694 | -116.2536 | 2720 | I | 78-80 | 80 | X | X | X | X | X | X | X |
| 03N 02E 19BAA2 | 433522116155502 | 43.58944 | -116.2653 | 2765 | P | 468-519 | 525 | X | | X | X | X | X | |
| 03N 02E 20DBD1 | 433446116141801 | 43.57944 | -116.2383 | 2793 | U | - | 106 | X | X | X | X | X | X | |
| 03N 02E 21BCC1 | 433502116135201 | 43.58389 | -116.2311 | 2751 | D/U | - | 58 | X | X | X | X | X | X | X |
| 03N 02E 23BAA1 | 433517116110101 | 43.58805 | -116.1836 | 2720 | U | - | 1200 | | | | | X | X | X |
| 03N 02E 23DDBC2 | 433439116103501 | 43.5775 | -116.1764 | 2742 | I | 292-362 | 425 | X | X | | | | | |
| 03N 02E 25AAC1 | 433420116091901 | 43.57222 | -116.1553 | 2758 | H | 63-68 | 70 | X | X | X | X | X | X | X |
| 03N 02E 25BDA1 | IDWR-S2000-06 | 43.57028 | -116.1631 | 2759 | I | 39-65 | 75 | | | | | X | X | X |
| 03N 02E 25CAA1 | IDWR-S2000-07 | 43.56778 | -116.1628 | 2788 | P | - | 416 | | | | | X | X | X |
| 03N 02E 25CACC1 | 433353116100001 | 43.56472 | -116.1667 | 2800 | U | 32-42 | 43 | | | X | X | X | X | |
| 03N 02E 25BCA1 | 433358116101301 | 43.56611 | -116.1703 | 2755 | U | - | 0 | | | X | X | X | X | X |
| 03N 02E 25CDBA1 | 433351116095701 | 43.56417 | -116.1658 | 2815 | U | 37-51 | 51 | | | X | X | X | X | X |
| 03N 02E 25CDBB1 | 433351116100201 | 43.56417 | -116.1672 | 2813 | U | 35-47 | 47 | | | X | X | X | X | X |
| 03N 02E 26DBA1 | IDWR-S2000-08 | 43.5675 | -116.1778 | 2800 | P | 355-644 | 663 | | | | | X | X | X |
| 03N 02E | 433353116115201 | 43.56472 | -116.1978 | 2871 | P/P | 365-455 | 455 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|-------------|-----------|-------------|-----------|--------|-----------|-----------|
| 27DBD1 | | | | | | | | | | | | | | |
| 03N 02E 28BDB1 | 433417116133001 | 43.57139 | -116.225 | 2830 | N | 275-280 | 280 | X | X | X | X | X | X | |
| 03N 02E 30CAC1 | 433359116160301 | 43.56667 | -116.2681 | 2765 | H | 100-103 | 103 | X | X | X | X | X | X | X |
| 03N 02E 30DDB1 | 433350116152201 | 43.56389 | -116.2561 | 2785 | H | - | 212 | | | X | X | X | X | X |
| 03N 02E 31AAC1 | 433332116152301 | 43.55889 | -116.2564 | 2682 | H | 136-143 | 143 | | | X | X | X | X | X |
| 03N 02E 35BAB1 | 433334116110601 | 43.55944 | -116.185 | 2892 | P | - | 944 | | | | | | | X |
| 03N 02E 36ABC1 | 433328116094201 | 43.55833 | -116.1611 | 2890 | P | 342-642 | 642 | | | | | X | X | X |
| 03N 02E 36CDD1 | IDWR303824 | 43.5475 | -116.1633 | 2930 | I | 517-566 | 570 | X | X | | | | | |
| 03N 02W 03DAA1 | 433735116331101 | 43.62639 | -116.5531 | 2470 | H | 229-234 | 234 | X | X | X | X | X | X | X |
| 03N 02W 04ADD1 | 433741116342201 | 43.62806 | -116.5728 | 2460 | H | 310-314 | 319 | X | X | X | X | X | X | X |
| 03N 02W 06ACD1 | 433737116370701 | 43.62694 | -116.6186 | 2441 | I | 80-87 | 87 | X | X | X | X | X | X | X |
| 03N 02W 06DCC1 | 433714116371901 | 43.62055 | -116.6219 | 2430 | P | 380-510 | 550 | X | X | X | X | X | X | X |
| 03N 02W 08BCCC1 | 433645116364001 | 43.6125 | -116.6111 | 2445 | C | - | 94 | X | X | X | X | X | X | X |
| 03N 02W 09DDDD1 | 433620116342101 | 43.60555 | -116.5725 | 2470 | U/N | 58-289 | 292 | X | X | | | | | |
| 03N 02W 10ACC1 | 433645116334301 | 43.6125 | -116.562 | 2460 | I/D | 84-138 | 138 | X | X | X | X | | | |
| 03N 02W 12BBB1 | 433708116315401 | 43.61889 | -116.5317 | 2488 | H | 58-60 | 61 | X | X | X | X | X | X | X |
| 03N 02W 14DBA1 | 433552116321501 | 43.59778 | -116.5375 | 2540 | P | 400-605 | 700 | X | X | X | X | X | X | X |
| 03N 02W 15DCDA1 | 433532116332901 | 43.59222 | -116.5581 | 2485 | I/D | 114-131 | 131 | X | X | X | | | | |
| 03N 02W 17ACDB1 | 433558116355401 | 43.59944 | -116.5983 | 2460 | U | 123-300 | 300 | X | X | X | X | X | X | |
| 03N 02W 17CCB2 | 433537116364301 | 43.59361 | -116.6119 | 2450 | H | 73-76 | 104 | X | X | X | X | X | X | |
| 03N 02W 24BAD2 | 433516116312701 | 43.58694 | -116.5231 | 2544 | H | - | 71 | X | X | X | X | X | X | X |
| 03N 02W 26BAA1 | 433433116323001 | 43.57583 | -116.5417 | 2505 | H | 34-83 | 83 | X | X | X | X | X | X | X |
| 03N 02W 29BCD1 | 433410116362601 | 43.56944 | -116.6072 | 2467 | H | - | 116 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|--------|-----------|-------------|-----------|-------------|-----------|-----------|
| 03N 02W 31BCC1 | 433317116375401 | 43.55416 | -116.6314 | 2590 | I | 152-172 | 172 | X | X | X | X | X | X | X |
| 03N 02W 34BBCB1 | 433335116341501 | 43.55972 | -116.5708 | 2490 | I | 165-200 | 210 | X | X | X | X | X | X | X |
| 03N 02W 35DBAC1 | 433311116321901 | 43.55305 | -116.5386 | 2503 | I/H | 67-117 | 117 | X | X | X | X | X | X | X |
| 03N 03E 07CBAC1 | 433636116090201 | 43.61 | -116.1506 | 3160 | U | 129-290 | 290 | X | X | | | | | |
| 03N 03E 19DBD1 | 433449116082001 | 43.58028 | -116.1389 | 2800 | H | 75-80 | 80 | X | X | X | X | X | X | X |
| 03N 03E 29ADD2 | 433408116065202 | 43.56889 | -116.1144 | 2810 | P | 81-101 | 106 | X | X | X | X | X | X | X |
| 03N 03E 29CCDA2 | 433343116074301 | 43.56194 | -116.1286 | 2820 | H | 140-100 | 100 | | | X | X | X | X | X |
| 03N 03E 30BCBD1 | 433413116090401 | 43.57028 | -116.1508 | 2762 | H | - | 48 | X | X | X | X | X | X | X |
| 03N 03E 30DAAD2 | 433406116080101 | 43.56694 | -116.1333 | 2750 | P/I | - | 60 | X | X | X | X | X | X | X |
| 03N 03E 30DDAA1 | 433351116380301 | 43.56417 | -116.1342 | 2800 | U | 246-940 | 940 | X | X | X | X | X | X | X |
| 03N 03E 31BDD1 | IDWR-S2000-09 | 43.55361 | -116.1444 | 2945 | P | 527-818 | 838 | | | | | X | X | X |
| 03N 03E 31CAA1 | 433313116083901 | 43.55416 | -116.1444 | 2945 | P | - | 0 | | | | | X | X | |
| 03N 03E 32BBA1 | 433337116075001 | 43.56028 | -116.1306 | 2823 | U/C | 232-260 | 280 | X | X | X | X | X | X | X |
| 03N 03E 32CDD1 | 433247116072601 | 43.54639 | -116.1239 | 2965 | Z/Z | 560-731 | 802 | X | X | X | X | X | X | X |
| 03N 03E 33DAA1 | 433310116054201 | 43.55278 | -116.095 | 2862 | H | 120-127 | 127 | X | X | X | X | X | X | X |
| 03N 03W 03BCB2 | 433745116412501 | 43.62917 | -116.6903 | 2429 | U | 22-94 | 95 | | X | X | X | X | X | X |
| 03N 03W 06DDC1 | 433710116441101 | 43.61944 | -116.7361 | 2560 | I | 131-137 | 255 | X | X | X | X | X | X | X |
| 03N 03W 09BAB1 | 433704116421901 | 43.61777 | -116.7053 | 2500 | H | 98-122 | 122 | | X | X | X | X | X | X |
| 03N 03W 10CBA3 | 433636116411901 | 43.61 | -116.6886 | 2560 | T/I | 70-300 | 300 | X | X | | | | | |
| 03N 03W 11DAC1 | 433630116392401 | 43.60833 | -116.6567 | 2441 | I/D | - | 90 | X | X | X | X | | | |
| 03N 03W 14CDA1 | 433531116394601 | 43.59194 | -116.6628 | 2480 | H | 69-79 | 80 | X | X | | | | | |
| 03N 03W 23BBC1 | 433517116401801 | 43.58805 | -116.6717 | 2540 | U/I | 118-190 | 250 | X | X | X | X | X | X | X |
| 03N 03W | 433433116392701 | 43.57583 | -116.6575 | 2490 | I | 50-80 | 97 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|--------|-----------|-------------|-----------|-------------|-----------|-----------|
| 23DCD1 | | | | | | | | | | | | | | |
| 03N 03W 27ABB1 | 433427116405001 | 43.57417 | -116.6805 | 2450 | I | 119-122 | 122 | X | X | X | X | X | X | X |
| 03N 03W 31ADA1 | 433321116435601 | 43.55583 | -116.7322 | 2630 | H | 159-260 | 260 | | | X | X | X | X | |
| 03N 04W 03AAD1 | 433746116473101 | 43.62944 | -116.7919 | 2487 | P | 70-75 | 78 | X | X | X | X | X | X | |
| 03N 04W 05AAB1 | 433755116500901 | 43.63194 | -116.8358 | 2618 | I | 140-325 | 325 | X | X | | | | | |
| 03N 04W 07ABA1 | 433703116513001 | 43.6175 | -116.8583 | 2462 | I | 208-503 | 503 | | | X | X | X | X | X |
| 03N 04W 11ADA1 | 433646116461801 | 43.61278 | -116.7717 | 2497 | U | 94-175 | 175 | X | X | X | X | X | X | X |
| 03N 04W 12AAD2 | 433655116451001 | 43.61528 | -116.7528 | 2492 | H | 233-270 | 270 | | | X | X | X | X | X |
| 03N 04W 13BBC1 | 433601116461001 | 43.60028 | -116.7694 | 2535 | H | 205-295 | 295 | X | X | X | X | X | | |
| 03N 04W 15DCC1 | 433517116475501 | 43.58805 | -116.7986 | 2378 | H | 79-80 | 80 | X | X | X | X | X | X | X |
| 03N 05W 03ADA1 | 433740116544201 | 43.62778 | -116.9117 | 2285 | C | 40-55 | 55 | | | X | X | X | X | |
| 03N 05W 03DBD1 | 433723116550201 | 43.62305 | -116.9172 | 2250 | P | 456-533 | 533 | | | X | X | X | X | X |
| 03N 05W 11DAD1 | 433627116532701 | 43.6075 | -116.8908 | 2280 | H/S | 85-86 | 86 | | | X | X | X | X | X |
| 04N 01E 03DAD1 | 434243116185001 | 43.71194 | -116.3139 | 2700 | U | 100-140 | 250 | X | X | X | X | X | X | X |
| 04N 01E 04BCCD1 | 434250116210401 | 43.71389 | -116.3511 | 2600 | H | 387-465 | 470 | X | X | X | X | X | X | X |
| 04N 01E 04DCC1 | IDWR347115 | 43.70694 | -116.3428 | 2632 | U | 276-285 | 285 | X | X | X | X | | | |
| 04N 01E 05CBBD1 | 434245116221701 | 43.7125 | -116.3714 | 2590 | H | - | 30 | X | X | X | X | X | X | X |
| 04N 01E 10ACB2 | 434206116192001 | 43.70167 | -116.3222 | 2636 | H | 289-308 | 308 | X | X | | X | X | X | X |
| 04N 01E 11BAA1 | 434216116183501 | 43.705 | -116.3039 | 2800 | H | 290-300 | 335 | X | X | X | X | X | X | X |
| 04N 01E 11BBB1 | 434223116183901 | 43.70639 | -116.3108 | 2690 | H | 120-203 | 203 | X | X | X | X | X | X | X |
| 04N 01E 13BDD1 | 434109116170701 | 43.68583 | -116.2853 | 2620 | H | 70-78 | 78 | | | | | X | X | X |
| 04N 01E 14CCB1 | 434048116184401 | 43.68 | -116.3122 | 2582 | U | 300-340 | 357 | | | | | X | X | X |
| 04N 01E 14CCB2 | 434048116184402 | 43.68 | -116.3122 | 2582 | U | 270-290 | 295 | | | | | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|--------|-----------|-------------|-----------|-------------|-----------|-----------|
| 04N 01E 14CCB3 | 434048116184403 | 43.68 | -116.3122 | 2582 | U | 210-250 | 250 | | | | | X | X | X |
| 04N 01E 14CCB4 | 434048116184404 | 43.68 | -116.3122 | 2582 | U | 130-170 | 177 | | | | | X | X | X |
| 04N 01E 15BADC1 | 434121116192901 | 43.68917 | -116.3247 | 2575 | P | 1-18 | 103 | | | | | | X | X |
| 04N 01E 16AAA1 | 434129116200301 | 43.69139 | -116.3342 | 2565 | H/S | 87-88 | 88 | X | X | X | X | X | X | |
| 04N 01E 17CDD1 | 434042116215001 | 43.67833 | -116.3639 | 2546 | H | - | 115 | X | X | X | X | X | X | X |
| 04N 01E 21DCCC1 | 433948116203401 | 43.66333 | -116.3428 | 2605 | H | 99-104 | 106 | X | X | X | X | X | X | X |
| 04N 01E 21DDDC1 | 433950116200401 | 43.66389 | -116.3344 | 2630 | U | 93-102 | 102 | X | X | X | X | X | X | X |
| 04N 01E 23DAC1 | 433957116173601 | 43.66833 | -116.2961 | 2698 | P | 327-403 | 403 | X | X | X | X | | | |
| 04N 01E 24BCA1 | 434020116171901 | 43.67222 | -116.2886 | 2602 | H | 50-70 | 71 | X | X | X | X | | | |
| 04N 01E 26CDD1 | 433856116181501 | 43.64889 | -116.3042 | 2660 | H | 96-105 | 105 | X | X | X | X | X | X | X |
| 04N 01E 27AADA1 | 433939116184801 | 43.66084 | -116.3133 | 2613 | U/U | 620-868 | 892 | X | X | X | X | X | X | X |
| 04N 01E 29CCCD1 | 433856116221601 | 43.64889 | -116.3711 | 2605 | H | 84-89 | 90 | X | X | X | X | X | X | X |
| 04N 01E 33AADC1 | 433843116200701 | 43.64528 | -116.3353 | 2637 | H | 96-101 | 103 | X | X | X | X | X | X | X |
| 04N 01E 34ACB1 | 433838116192301 | 43.64389 | -116.3231 | 2643 | H | 145-150 | 160 | | | | | | | X |
| 04N 01E 34ACBC1 | 433837116192301 | 43.64361 | -116.3231 | 2644 | H | 476-481 | 481 | | X | X | X | X | X | X |
| 04N 01E 34CAD1 | 433819116192501 | 43.6375 | -116.3247 | 2650 | P | 671-752 | 755 | X | X | | | | | |
| 04N 01E 35CCA1 | 433813116183201 | 43.63695 | -116.3089 | 2660 | D/I | 90-108 | 109 | X | X | X | X | X | X | X |
| 04N 01E 35DAA1 | 433822116174101 | 43.63945 | -116.2947 | 2675 | H | 175-205 | 205 | X | X | X | X | X | X | X |
| 04N 01E 36BAC1 | 433843116171601 | 43.645 | -116.2875 | 2673 | U | 760-1005 | 1005 | X | X | X | X | | | |
| 04N 01E 36BAC2 | 433842116171601 | 43.645 | -116.2875 | 2673 | P | 474-545 | 551 | X | | X | | X | X | X |
| 04N 01W 01CAA1 | 434244116241101 | 43.71222 | -116.4031 | 2552 | H | 239-260 | 260 | X | X | X | X | X | X | X |
| 04N 01W 03CDDA1 | 434228116263401 | 43.70778 | -116.4428 | 2502 | H | 51-57 | 57 | X | X | X | X | X | X | X |
| 04N 01W | 434243116284501 | 43.71194 | -116.4792 | 2520 | H | 132-142 | 142 | X | X | X | X | X | X | |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|--------|-----------|-------------|-----------|-------------|-----------|-----------|
| 05DBD1 | | | | | | | | | | | | | | |
| 04N 01W 07AAD1 | 434219116293401 | 43.70528 | -116.4928 | 2465 | H | 162-172 | 172 | X | X | X | X | X | X | X |
| 04N 01W 07DAAA1 | 434156116293301 | 43.69889 | -116.4925 | 2465 | U/P | 420-440 | 440 | X | X | X | X | X | X | X |
| 04N 01W 13AACC1 | 434106116240301 | 43.68861 | -116.3972 | 2525 | I | 240-320 | 332 | X | X | X | X | X | X | X |
| 04N 01W 13DDB1 | 434048116235101 | 43.68 | -116.3975 | 2525 | I | - | 130 | X | X | X | X | X | | |
| 04N 01W 16CAA1 | 434104116274701 | 43.68444 | -116.4631 | 2482 | H | 150-152 | 160 | X | X | | | | | |
| 04N 01W 17BBDB1 | 434124116292101 | 43.69 | -116.4892 | 2470 | H | 140-149 | 149 | | X | X | X | X | X | X |
| 04N 01W 17BDBC1 | 434120116292101 | 43.68889 | -116.4892 | 2468 | H | 381-424 | 424 | X | X | X | X | X | X | X |
| 04N 01W 17CBDB1 | 434059116292101 | 43.68306 | -116.4892 | 2465 | H | 113-118 | 118 | X | | | | | | |
| 04N 01W 19DADA1 | 434007116293501 | 43.66861 | -116.4931 | 2495 | H | 161-170 | 170 | X | X | X | X | X | X | |
| 04N 01W 22DBB1 | 434013116262801 | 43.67028 | -116.4411 | 2545 | H | 80-93 | 93 | X | X | X | X | X | X | |
| 04N 01W 23ACCC2 | 434013116252201 | 43.67028 | -116.4228 | 2560 | H | 150-155 | 155 | | | X | X | X | X | X |
| 04N 01W 24ACAB1 | 434026116235601 | 43.67389 | -116.3989 | 2570 | H | 109-120 | 120 | | | X | X | X | X | X |
| 04N 01W 24ACAB3 | 434025116235901 | 43.67361 | -116.3997 | 2570 | Q | 300-313 | 313 | | | X | X | X | X | |
| 04N 01W 24BCAC1 | 434020116243401 | 43.67222 | -116.4094 | 2575 | H | 230-235 | 235 | | | X | X | X | X | X |
| 04N 01W 28ADD1 | 433923116271001 | 43.65639 | -116.4528 | 2535 | H | 72-80 | 80 | X | X | X | X | X | X | X |
| 04N 01W 30ABBC1 | 433942116300901 | 43.66167 | -116.5025 | 2500 | H | 230-237 | 237 | | | X | X | X | X | X |
| 04N 01W 30ADAA2 | 433934116293602 | 43.65917 | -116.493 | 2505 | H | 89-99 | 99 | X | X | | X | X | X | X |
| 04N 01W 31AAA1 | 433852116293401 | 43.64778 | -116.4928 | 2508 | I | 455-462 | 462 | X | X | X | X | X | X | X |
| 04N 01W 32BBBC1 | 433849116293201 | 43.64695 | -116.4922 | 2510 | H | 60-65 | 65 | X | X | X | X | X | X | X |
| 04N 01W 33ADAD1 | 433835116271201 | 43.64306 | -116.4533 | 2530 | H | 67-77 | 77 | X | X | X | X | X | X | X |
| 04N 01W 33CBB1 | 433828116281701 | 43.64111 | -116.4714 | 2525 | H | - | 400 | X | X | | | | | |
| 04N 01W 35AAA1 | 433852116244801 | 43.64778 | -116.4133 | 2571 | H/U | - | 44 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|--------|-----------|-------------|-----------|-------------|-----------|-----------|
| 04N 02E 09CCD2 | 434131116134201 | 43.69194 | -116.2283 | 3200 | H | - | 0 | | | | | | | X |
| 04N 02E 17CABC1 | 434103116143601 | 43.68278 | -116.2467 | 3020 | H | 110-525 | 525 | | | | | X | X | X |
| 04N 02E 19ABB1 | 434035116154401 | 43.67639 | -116.2622 | 2680 | H | - | 98 | X | X | X | X | X | X | X |
| 04N 02E 21DACA1 | 434003116125701 | 43.6675 | -116.2158 | 2890 | A | 644-880 | 880 | X | X | | | | | |
| 04N 02E 25DCBB1 | 433901116093901 | 43.65139 | -116.1614 | 3490 | H | 339-340 | 340 | X | X | | | | | |
| 04N 02E 29ACA1 | 433930116141901 | 43.65833 | -116.2386 | 2670 | H | 43-48 | 85 | | | | | | | X |
| 04N 02E 29ACC1 | 433921116143401 | 43.65583 | -116.2428 | 2663 | I | - | 45 | X | X | X | X | X | X | X |
| 04N 02E 29ACDB1 | 433925116141901 | 43.65694 | -116.2386 | 2670 | I/A | - | 1195 | X | X | X | X | X | X | X |
| 04N 02E 30ACAC1 | 433929116153701 | 43.65778 | -116.2594 | 2630 | I | - | 0 | X | X | | | | | |
| 04N 02E 30ACDB1 | 433928116153801 | 43.6575 | -116.2597 | 2630 | H | - | 41 | X | X | X | X | X | X | X |
| 04N 02E 31AAB2 | 433850116151701 | 43.64722 | -116.2547 | 2630 | H | - | 60 | X | X | X | X | X | X | X |
| 04N 02E 31ACAB1 | 433838116153601 | 43.64389 | -116.26 | 2632 | U | - | 0 | X | X | | | | | |
| 04N 02E 33ACAC1 | 433836116132701 | 43.64333 | -116.2194 | 2695 | I/H | 47-52 | 53 | X | X | X | X | X | X | X |
| 04N 02E 34CAAC1 | 433821116121701 | 43.63917 | -116.2047 | 2728 | H/I | 69-100 | 100 | X | X | X | X | X | X | X |
| 04N 02E 35CBBA1 | 433824116112501 | 43.63972 | -116.1894 | 2850 | U | 737-771 | 781 | X | X | | | | | |
| 04N 02W 01AADA1 | 434310116304501 | 43.71944 | -116.5125 | 2480 | H | - | 0 | | | X | X | X | X | X |
| 04N 02W 01ADAA3 | 434301116304401 | 43.71695 | -116.5122 | 2480 | H | 74-84 | 84 | | | X | X | X | X | X |
| 04N 02W 01DCDD1 | 434225116310301 | 43.70694 | -116.5175 | 2450 | H | 530-675 | 675 | | | X | X | X | X | X |
| 04N 02W 02DDD1 | 434226116315701 | 43.70722 | -116.5325 | 2445 | H | 31-50 | 50 | X | X | X | X | X | X | X |
| 04N 02W 05ABB1 | 434314116360401 | 43.72055 | -116.6011 | 2497 | P | - | 475 | X | X | | | | | |
| 04N 02W 06CDD1 | 434228116372701 | 43.70778 | -116.6242 | 2404 | P | 404-420 | 420 | X | X | X | X | X | X | X |
| 04N 02W 07AAC1 | 434214116365901 | 43.70389 | -116.6164 | 2395 | H | 40-42 | 42 | X | X | X | X | X | X | X |
| 04N 02W | 434200116353201 | 43.7 | -116.5922 | 2407 | H | 60-80 | 80 | | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|--------|-----------|-------------|-----------|-------------|-----------|-----------|
| 08ADD1 | | | | | | | | | | | | | | |
| 04N 02W 10BBCB1 | 434217116341801 | 43.70472 | -116.5717 | 2420 | H | 128-133 | 133 | X | X | X | X | X | X | X |
| 04N 02W 21CBB1 | 434014116353201 | 43.67056 | -116.5922 | 2432 | H | 79-90 | 90 | X | X | X | X | X | X | X |
| 04N 02W 22DCD1 | 433948116333201 | 43.66333 | -116.5589 | 2458 | H | 237-262 | 262 | | | X | X | X | X | |
| 04N 02W 24CCC1 | 433951116315401 | 43.66417 | -116.5317 | 2479 | I | 53-77 | 77 | X | X | X | X | X | X | X |
| 04N 02W 26CAD1 | 433910116323301 | 43.65278 | -116.5425 | 2472 | I | 140-152 | 152 | X | X | X | X | | | |
| 04N 02W 31AAA1 | 433852116364501 | 43.64778 | -116.6125 | 2438 | H | - | 150 | X | X | X | X | X | X | X |
| 04N 02W 33ABC1 | 433844116345401 | 43.64556 | -116.5817 | 2455 | I | 123-148 | 148 | X | X | X | X | | | |
| 04N 02W 36CCC1 | 433757116320101 | 43.63472 | -116.5317 | 2480 | H | 106-108 | 108 | | | X | X | X | X | X |
| 04N 03W 01CBBA1 | 434248116385901 | 43.71333 | -116.6497 | 2420 | H | 213-218 | 218 | | | X | X | X | X | X |
| 04N 03W 02ADD1 | 434249116390901 | 43.71361 | -116.6525 | 2430 | H | 97-135 | 135 | | | X | X | X | X | X |
| 04N 03W 04DCB1 | 434233116420201 | 43.70917 | -116.7006 | 2430 | H/I | 259-293 | 296 | X | X | X | X | X | X | X |
| 04N 03W 04DDCD1 | 434224116414401 | 43.70667 | -116.6956 | 2465 | H | 199-227 | 227 | X | X | X | X | X | X | X |
| 04N 03W 06AAA1 | 434312116435501 | 43.72 | -116.7319 | 2372 | I | 31-160 | 160 | X | X | X | X | X | X | X |
| 04N 03W 12ACDD1 | 434200116381701 | 43.7 | -116.6381 | 2387 | U/I | 10-35 | 40 | X | X | X | X | X | X | X |
| 04N 03W 13BAA1 | 434128116383601 | 43.69111 | -116.6433 | 2370 | S | 181-185 | 185 | X | X | X | X | X | X | X |
| 04N 03W 15ADC1 | 434105116402701 | 43.68472 | -116.6742 | 2440 | U | 875-1010 | 1010 | | | | | X | X | X |
| 04N 03W 15ADC2 | 434105116402702 | 43.68472 | -116.6742 | 2440 | U | 579-725 | 725 | | | | | X | X | X |
| 04N 03W 15ADC3 | 434105116402703 | 43.68472 | -116.6742 | 2440 | U | 430-550 | 550 | | | | | X | X | X |
| 04N 03W 15ADC4 | 434105116402704 | 43.68472 | -116.6742 | 2440 | U | 270-407 | 407 | | | | | X | X | X |
| 04N 03W 15ADC5 | 434105116402705 | 43.68472 | -116.6742 | 2440 | U | 208-270 | 270 | | | | | X | X | X |
| 04N 03W 15ADC6 | 434105116402706 | 43.68472 | -116.6742 | 2440 | U | 166-208 | 208 | | | | | X | X | X |
| 04N 03W 15ADC7 | 434105116402707 | 43.68472 | -116.6742 | 2440 | U | 122-166 | 166 | | | | | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-----------|-----|---------------|------------|-------------|-----------|-------------|-----------|-------------|-----------|-----------|
| 04N 03W 15ADC8 | 434105116402708 | 43.68472 | -116.6742 | 2440 | U | 110-120 | 122 | | | | | X | X | X |
| 04N 03W 16DDDC1 | 434038116413801 | 43.67722 | -116.6939 | 2348 | U/I | 57-75 | 80 | X | X | X | X | X | X | X |
| 04N 03W 24ACB1 | 434024116382901 | 43.67334 | -116.6414 | 2412 | H | - | 92 | X | X | X | X | X | X | X |
| 04N 03W 25DAA3 | 433919116375701 | 43.65528 | -116.6325 | 2424 | U | 62-68 | 80 | X | X | X | X | | | |
| 04N 03W 26ABCC1 | 433935116394301 | 43.65973 | -116.6619 | 2412 | P | 286-503 | 515 | X | X | | | | | |
| 04N 03W 27AACD1 | 433934116403201 | 43.65945 | -116.6756 | 2380 | P | 175-320 | 330 | X | X | X | X | X | X | X |
| 04N 03W 27CBAD1 | 433915116411701 | 43.65417 | -116.6881 | 2380 | I | 76-97 | 97 | X | X | X | X | X | X | X |
| 04N 03W 28ADD1 | 433921116413501 | 43.65583 | -116.6931 | 2378 | P | 150-200 | 395 | X | X | X | X | X | X | X |
| 04N 03W 30ADA1 | 433935116441001 | 43.65806 | -116.7322 | 2353 | H | 160-192 | 192 | X | X | X | X | X | X | X |
| 04N 03W 31CBA2 | 433825116445702 | 43.64028 | -116.7492 | 2467 | H | - | 0 | | | X | X | X | X | X |
| 04N 03W 33DADC1 | 433815116413801 | 43.6375 | -116.6939 | 2440 | H | 348-357 | 357 | | | X | X | X | X | X |
| 04N 04W 04CDC1 | 434225116493101 | 43.70694 | -116.8253 | 2285 | H/S | 387-420 | 420 | X | X | X | X | X | X | X |
| 04N 04W 05CAC1 | 434234116504601 | 43.70945 | -116.8461 | 2280 | H | 168-224 | 224 | | X | X | X | X | X | X |
| 04N 04W 08BB1 | IDWR297941 | 43.70383 | -116.8492 | 2280 | H | 210-230 | 230 | X | | | | | | |
| 04N 04W 08CDCC1 | 434128116504401 | 43.69111 | -116.8456 | 2350 | H | 58-70 | 70 | | | X | X | X | X | X |
| 04N 04W 10CDAB1 | 434138116481201 | 43.69389 | -116.8033 | 2300 | H/S | 97-116 | 116 | | | X | X | X | X | X |
| 04N 04W 15ACCB2 | 434108116480402 | 43.68555 | -116.8011 | 2304 | H | 68-74 | 74 | | | X | X | X | X | |
| 04N 04W 15ACCB3 | 434107116480501 | 43.68528 | -116.8014 | 2304 | H | 215-220 | 220 | X | | X | | X | X | X |
| 04N 04W 21CAA1 | 434008116492001 | 43.66889 | -116.8222 | 2440 | H | 35-36 | 36 | X | X | X | | X | X | X |
| 04N 04W 21CAA2 | 432835116492501 | 43.66945 | -116.8225 | 2420 | H | 35-36 | 36 | X | X | X | | X | X | |
| 04N 04W 22DDD1 | 433945116473201 | 43.6625 | -116.7922 | 2353 | I | 72-132 | 137 | X | X | X | | | | |
| 04N 04W 25BDD3 | 433919116454903 | 43.65528 | -116.7636 | 2368 | I/U | 138-175 | 175 | X | X | X | X | | | |
| 04N 04W | 433929116491501 | 43.65806 | -116.8208 | 2470 | H/S | 54-56 | 56 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Surface Elevation | Use | Open Interval | Well Depth | Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-------------------|-----|---------------|------------|--------|-----------|-------------|-----------|-------------|-----------|-----------|
| 28ACB1 | | | | | | | | | | | | | | |
| 04N 04W 30BBB1 | 433942116520101 | 43.66167 | -116.8669 | 2461 | U/H | 76-85 | 85 | X | | X | X | X | X | X |
| 04N 04W 30BBB2 | 433941116521301 | 43.66139 | -116.8703 | 2480 | H | 34-71 | 71 | X | X | X | X | X | X | X |
| 04N 04W 33CDC2 | 433800116493001 | 43.63334 | -116.825 | 2525 | U/I | 50-63 | 72 | X | X | X | X | X | X | X |
| 04N 04W 36DB1 | IDWR297845-X | 43.63867 | -116.7695 | 2494 | H | 564-586 | 586 | X | | | | | | |
| 04N 05W 07DCD1 | 434132116584001 | 43.69222 | -116.9778 | 2292 | I | 64-131 | 131 | X | X | X | X | X | X | X |
| 04N 05W 10CDD1 | 434128116551601 | 43.69111 | -116.9211 | 2423 | H/S | 287-306 | 306 | X | X | X | X | X | X | X |
| 04N 05W 14CCC2 | 434040116543502 | 43.67778 | -116.9097 | 2424 | P | 500-910 | 910 | X | X | X | | | | |
| 04N 05W 14DAD1 | 434053116532901 | 43.68139 | -116.8914 | 2421 | H | 56-65 | 65 | X | X | X | X | X | X | X |
| 04N 05W 21AAB2 | 434033116560501 | 43.67583 | -116.9347 | 2440 | H | 178-220 | 220 | X | X | X | X | X | X | X |
| 04N 05W 23BCC1 | 434009116543701 | 43.66917 | -116.9103 | 2465 | P | 285-515 | 525 | X | X | | | | | |
| 04N 05W 23CBB1 | 434006116543701 | 43.66833 | -116.9103 | 2467 | H | 68-80 | 80 | | | X | X | X | X | |
| 04N 06W 02DDA1 | 434234117004501 | 43.70945 | -117.0125 | 2420 | H | 123-280 | 280 | | | X | X | X | X | X |
| 04N 06W 11DCA1 | 434138117010101 | 43.69389 | -117.0169 | 2240 | H/S | 30-31 | 31 | | | X | X | X | X | X |
| 04N 06W 12CAC1 | 434141117002001 | 43.69473 | -117.0056 | 2275 | H | 83-123 | 123 | | | X | X | X | X | X |
| 05N 01E 26CDDC1 | 434409116182101 | 43.73583 | -116.3058 | 2715 | H | - | 61 | X | X | X | X | X | X | X |
| 05N 01E 26DCD1 | 434412116175801 | 43.73972 | -116.2992 | 2750 | H/I | 633-688 | 688 | X | X | X | X | X | X | X |
| 05N 01E 29DCA1 | 434415116213401 | 43.7375 | -116.3594 | 2740 | H/S | 244-246 | 247 | X | X | X | X | X | X | X |
| 05N 01E 31ACA1 | 434349116224101 | 43.73028 | -116.3781 | 2655 | H | 90-99 | 99 | X | X | X | X | X | X | |
| 05N 01E 33CCCD1 | 434316116210501 | 43.72111 | -116.3514 | 2632 | H | 168-190 | 190 | X | X | X | X | X | X | X |
| 05N 01E 34DBB1 | 434341116192001 | 43.72805 | -116.3222 | 2680 | I | - | 175 | X | X | X | X | X | X | X |
| 05N 01E 35ACA1 | 434350116175701 | 43.73056 | -116.2992 | 2720 | S | - | 0 | X | X | X | X | X | X | X |
| 05N 01E 36AAB1 | 434404116164001 | 43.73444 | -116.2778 | 2780 | I | 144-230 | 230 | X | X | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-----------|-----|---------------|------------|-------------|-----------|-------------|-----------|-------------|-----------|-----------|
| 05N 01W 09CAD1 | 434700116274501 | 43.78333 | -116.4625 | 2688 | H/I | 390-450 | 450 | | | X | X | X | X | X |
| 05N 01W 09CCD2 | 434650116280802 | 43.78056 | -116.4689 | 2680 | I | 285-415 | 425 | X | X | | X | X | X | X |
| 05N 01W 16CAB1 | 434615116275801 | 43.77083 | -116.4656 | 2715 | H | 492-628 | 628 | | | X | X | X | X | |
| 05N 01W 17BCA1 | 434628116292101 | 43.77444 | -116.4892 | 2630 | H/I | 222-237 | 237 | X | X | X | X | X | X | |
| 05N 01W 29CBA1 | 434433116291601 | 43.74167 | -116.4889 | 2630 | I | 272-332 | 332 | X | X | X | X | X | X | X |
| 05N 01W 32ACC1 | 434344116285401 | 43.72889 | -116.4817 | 2595 | H | - | 280 | X | X | X | X | X | X | X |
| 05N 01W 33ACD1 | 434344116273301 | 43.72889 | -116.4592 | 2590 | H | 106-108 | 108 | X | X | X | X | X | X | |
| 05N 01W 33CBDA1 | 434336116280301 | 43.72667 | -116.4675 | 2560 | H | 185-188 | 188 | | | X | X | X | X | X |
| 05N 01W 34DBAD1 | 434335116261501 | 43.72639 | -116.4375 | 2585 | H | - | 74 | X | X | X | X | X | X | X |
| 05N 01W 35CCC1 | 434321116255301 | 43.7225 | -116.4314 | 2582 | I | 44-84 | 84 | X | X | X | X | X | X | X |
| 05N 01W 36ABB1 | 434406116240801 | 43.735 | -116.4022 | 2618 | H/I | 204-208 | 208 | X | X | X | X | X | X | X |
| 05N 02E 29BCC1 | 434433116150401 | 43.7425 | -116.2511 | 2990 | H | 14-68 | 68 | X | X | | | | | |
| 05N 02E 31CAB1 | 434341116160201 | 43.72806 | -116.2672 | 2815 | I | 48-254 | 254 | X | X | | | | | |
| 05N 02W 19CBA1 | 434525116373601 | 43.75694 | -116.6267 | 2482 | U | 254-260 | 261 | X | X | X | X | X | X | X |
| 05N 02W 19CBA2 | 434525116373602 | 43.75694 | -116.6267 | 2482 | H | - | 0 | | X | X | X | X | X | X |
| 05N 02W 20BBA1 | 434551116362801 | 43.76417 | -116.6078 | 2500 | S | 71-114 | 117 | X | X | X | X | X | X | X |
| 05N 02W 22CAD1 | 434514116334501 | 43.75389 | -116.5625 | 2605 | I | 279-403 | 450 | X | X | X | X | X | X | X |
| 05N 02W 24DAB1 | 434525116305101 | 43.75694 | -116.5142 | 2595 | S | 280-320 | 330 | X | X | X | X | X | X | |
| 05N 02W 25BCD1 | 434436116313601 | 43.74333 | -116.5267 | 2632 | I | - | 448 | X | X | | | | | |
| 05N 02W 27DCC1 | 434413116334201 | 43.73695 | -116.5617 | 2565 | H | 213-218 | 218 | X | X | X | X | X | X | X |
| 05N 02W 29BBC2 | 434452116364101 | 43.74778 | -116.6114 | 2505 | H | 164-180 | 180 | X | X | X | X | X | X | X |
| 05N 02W 31BBC1 | 434356116375201 | 43.73222 | -116.6311 | 2472 | H | 102-132 | 133 | X | X | X | X | X | X | |
| 05N 02W | 434331116362501 | 43.72528 | -116.6069 | 2500 | H | 230-233 | 233 | X | X | X | X | X | X | |

| Well Name | Site ID | Well Latitude | Well Longitude | Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|-----------------|-----------------|---------------|----------------|-----------|-----|---------------|------------|-------------|-----------|-------------|-----------|-------------|-----------|-----------|
| 32CBD1 | | | | | | | | | | | | | | |
| 05N 03W 02CCD1 | 434738116400501 | 43.79389 | -116.6681 | 2560 | H | 380-384 | 386 | X | X | X | X | X | X | X |
| 05N 03W 04BCB1 | 434815116423901 | 43.80416 | -116.7108 | 2460 | H | 140-143 | 143 | X | X | X | X | X | X | |
| 05N 03W 08DDC1 | 434646116425401 | 43.77917 | -116.7153 | 2450 | H | 197-203 | 203 | X | X | X | X | X | X | X |
| 05N 03W 12CCA1 | 434652116385201 | 43.78111 | -116.6478 | 2560 | H | 60-314 | 314 | X | X | X | X | X | X | X |
| 05N 03W 15DDC1 | 434554116403101 | 43.765 | -116.6753 | 2495 | H/S | 147-152 | 152 | X | X | X | X | X | X | X |
| 05N 03W 19AAD1 | 434545116435701 | 43.7625 | -116.7325 | 2440 | H | 131-143 | 143 | X | X | X | X | X | X | X |
| 05N 03W 21CAD1 | 434517116421101 | 43.75472 | -116.703 | 2480 | H | 177-200 | 200 | X | X | X | X | X | X | X |
| 05N 03W 23BC1 | IDWR297637 | 43.75923 | -116.6693 | 2500 | H | 345-352 | 352 | | X | | | | | |
| 05N 03W 27CAA1 | 434432116405801 | 43.74222 | -116.6828 | 2450 | H | 236-287 | 287 | X | X | | | | | |
| 05N 03W 30ADD1 | 434430116435601 | 43.74306 | -116.7322 | 2475 | H | 158-180 | 180 | X | X | X | X | X | X | X |
| 05N 04W 08BCC1 | 434716116505401 | 43.78667 | -116.8519 | 2430 | H | 196-202 | 202 | X | X | X | X | X | X | X |
| 05N 04W 09DCA1 | 434651116490501 | 43.78083 | -116.8181 | 2460 | H | 274-279 | 281 | X | X | X | X | X | X | X |
| 05N 04W 16ABA1 | 434640116490301 | 43.77778 | -116.8175 | 2430 | H | 261-333 | 333 | X | X | X | X | X | X | |
| 05N 04W 20DADD1 | 434510116495501 | 43.75278 | -116.8319 | 2350 | H | 99-102 | 102 | | X | X | X | X | X | X |
| 05N 04W 21CABB2 | 434522116493201 | 43.75611 | -116.8256 | 2350 | H | 180-203 | 203 | X | | X | X | X | X | X |
| 05N 04W 24ABA1 | 434543116453301 | 43.76194 | -116.7592 | 2510 | I | 264-415 | 448 | X | X | X | X | X | X | X |
| 05N 04W 34BCB1 | 434346116484101 | 43.72945 | -116.8114 | 2300 | H/S | 115-190 | 190 | X | X | X | X | X | X | X |
| 05N 04W 35BBB1 | 434359116472801 | 43.73306 | -116.7911 | 2330 | H | 74-75 | 75 | X | X | X | X | X | X | X |
| 05N 04W 36BCC1 | 434339116461201 | 43.7275 | -116.77 | 2345 | I | 135-146 | 146 | X | X | X | X | X | X | X |
| 05N 05W 04BCC1 | 434759116570201 | 43.79972 | -116.9506 | 2285 | S/I | 45-46 | 46 | X | X | X | X | X | X | X |
| 05N 05W 04DCD1 | 434733116561501 | 43.7925 | -116.9375 | 2281 | P | 245-477 | 505 | X | X | X | X | X | X | X |
| 05N 05W 09BDB1 | 434714116564201 | 43.7875 | -116.9444 | 2225 | U/P | 245-440 | 450 | | | X | X | X | X | X |

| Well Name | Site ID | Well Latitude | Well Longitude | Elevation | Use | Open Interval | Well Depth | 1996 Spring | 1996 Fall | 1998 Spring | 1998 Fall | 2000 Spring | 2000 Fall | 2001 Fall |
|---------------------------------|-----------------|---------------|----------------|-----------|-----|---------------|------------|-------------|------------|-------------|------------|-------------|------------|------------|
| 05N 05W 10BBCB1 | 434724116555001 | 43.79 | -116.9305 | 2275 | H | 100-122 | 123 | | | X | X | X | X | X |
| 05N 05W 13CBC1 | 434605116532601 | 43.76805 | -116.8906 | 2311 | U/I | 39-142 | 142 | X | X | X | X | X | X | X |
| 05N 05W 18CAC1 | 434603116590901 | 43.7675 | -116.9858 | 2225 | H | - | 250 | X | X | X | X | X | X | X |
| 05N 05W 20CCD1 | 434459116575001 | 43.74972 | -116.9639 | 2255 | H | 36-37 | 37 | X | X | X | X | X | X | X |
| 05N 05W 27DDBC1 | 434411116545301 | 43.73639 | -116.9147 | 2260 | H | 60-61 | 61 | | | X | X | X | X | X |
| 05N 05W 29CDDA1 | 434409116574101 | 43.73583 | -116.9614 | 2375 | H | 199-222 | 222 | | | X | X | X | X | X |
| 05N 05W 32AAAA1 | 434402116570501 | 43.73389 | -116.9514 | 2378 | I | 210-380 | 385 | | | X | X | X | X | X |
| 05N 05W 32CDC1 | 434313116574901 | 43.72028 | -116.9636 | 2312 | H/S | 57-58 | 58 | X | X | X | X | X | X | X |
| 05N 05W 33ACCC1 | 434349116562401 | 43.7275 | -116.9408 | 2380 | I | 198-348 | 368 | | | X | X | X | X | |
| 05N 06W 01CDD1 | 434735117000801 | 43.79306 | -117.0022 | 2200 | S | 40-47 | 47 | | | X | X | X | X | X |
| 05N 06W 11AAD1 | 434725117004101 | 43.79028 | -117.0114 | 2195 | H | 76-82 | 82 | X | X | X | X | X | X | X |
| 05N 06W 26CAA1 | 434430117012301 | 43.74167 | -117.0231 | 2210 | U/H | - | 34 | X | X | X | X | X | X | X |
| 05N 06W 35CAC1 | 434310117011201 | 43.725 | -117.0217 | 2275 | H | 42-43 | 43 | X | X | X | X | X | X | X |
| 06N 03W 22CBB1 | 435032116412801 | 43.84222 | -116.6911 | 2570 | H | - | 235 | X | X | X | X | X | X | X |
| 06N 03W 30DCC1 | 434920116442701 | 43.82222 | -116.7408 | 2440 | H | 206-216 | 216 | X | X | X | X | X | X | X |
| 06N 03W 33CBA1 | 434845116422901 | 43.8125 | -116.7081 | 2480 | H | - | 152 | X | X | X | X | X | X | |
| 06N 04W 28CDC1 | 434922116493301 | 43.82278 | -116.8258 | 2630 | I | 369-705 | 705 | X | X | | | | | |
| 06N 04W 34DDB1 | 434835116474301 | 43.80972 | -116.7953 | 2480 | H | 144-147 | 147 | X | X | X | X | X | X | X |
| 06N 04W 35ADC1 | 433858116463401 | 43.81611 | -116.7761 | 2620 | H | 352-362 | 362 | X | X | X | X | X | X | X |
| 06N 05W 30CDC1 | 434920116591701 | 43.82222 | -116.9881 | 2335 | H | 60-62 | 62 | | | X | X | X | X | X |
| 06N 05W 35BAC1 | 434910116542701 | 43.81944 | -116.9075 | 2520 | H | 298-322 | 322 | X | X | X | X | X | X | X |
| 06N 05W 36CDB1 | 434836116531201 | 43.81 | -116.8867 | 2500 | I | 308-385 | 385 | X | X | X | X | X | X | X |
| SUMMARY: Number of Wells | | | | | | | | 343 | 343 | 383 | 372 | 392 | 390 | 341 |

Appendix E. POTENTIOMETRIC SURFACE MAPS

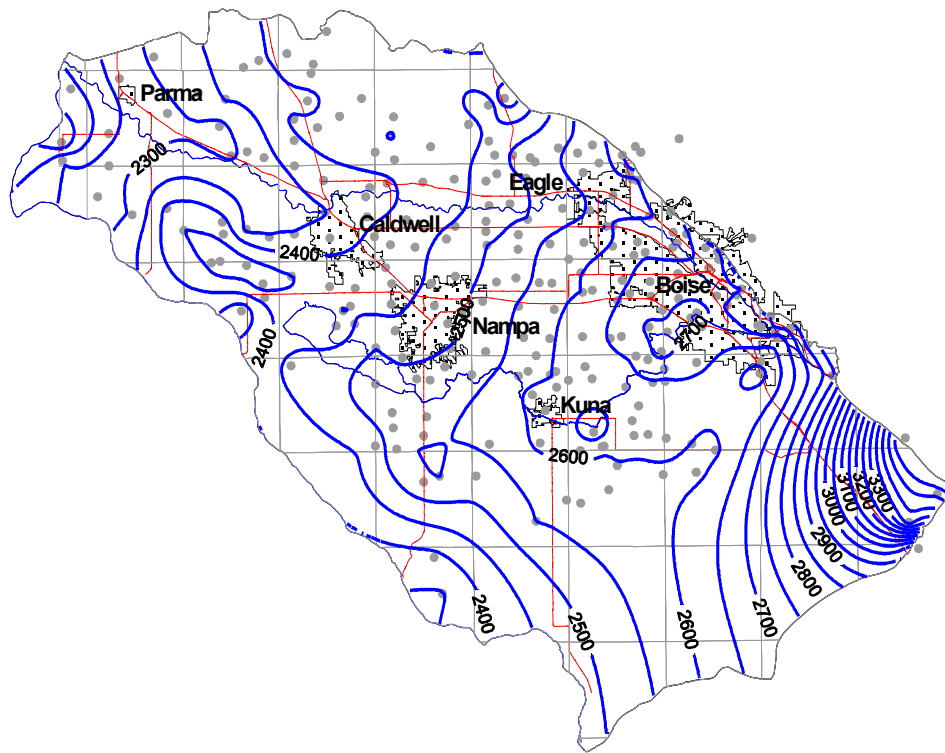


Figure E-1: Spring 1996, shallow zone (240 wells).

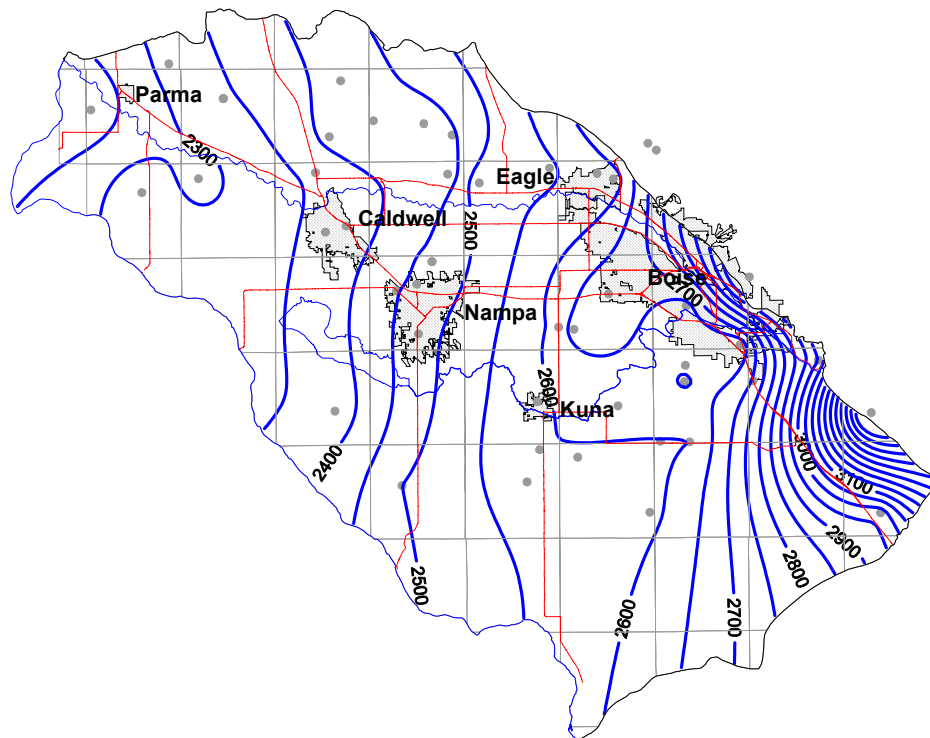


Figure E-2: Spring 1996, intermediate zone (49 wells).

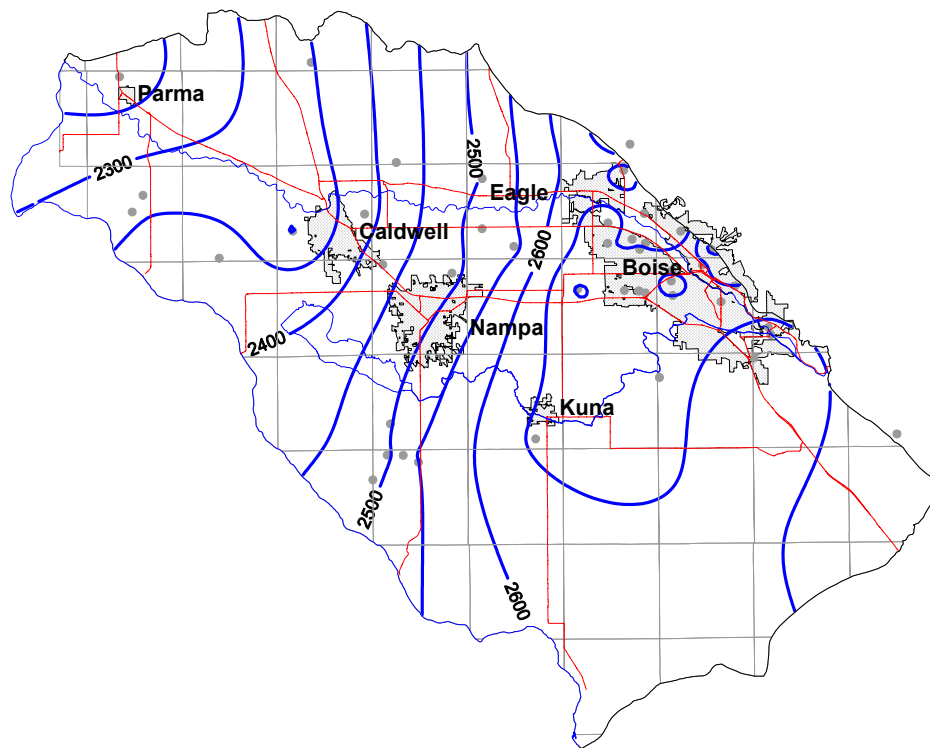


Figure E-3: Spring 1996, deep zone (45 wells).

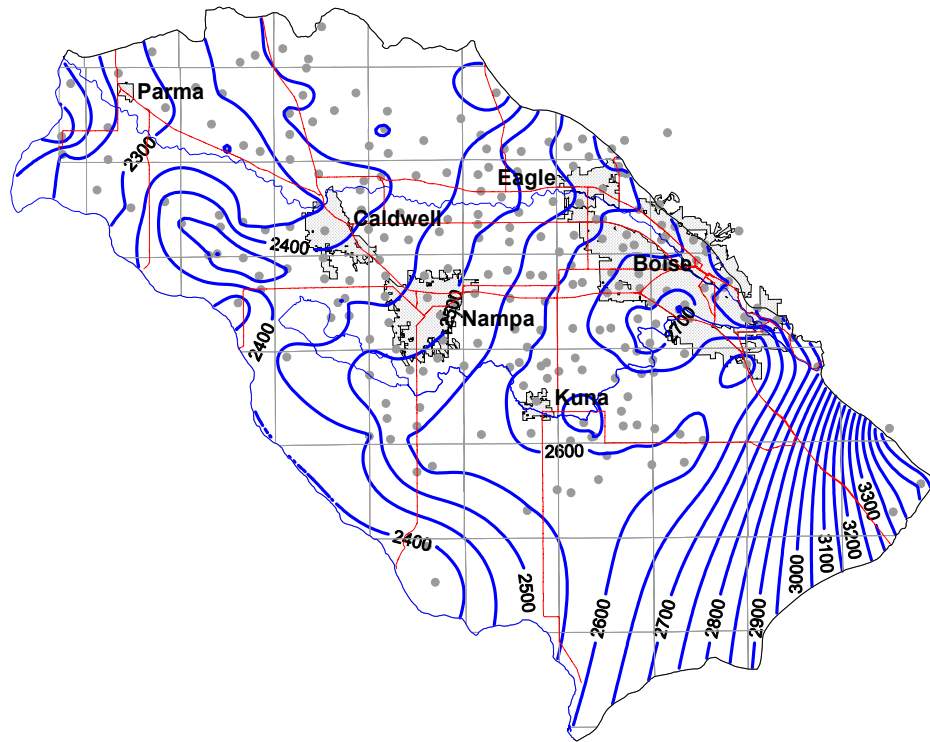


Figure E-4: Fall 1996, shallow zone (235 wells).

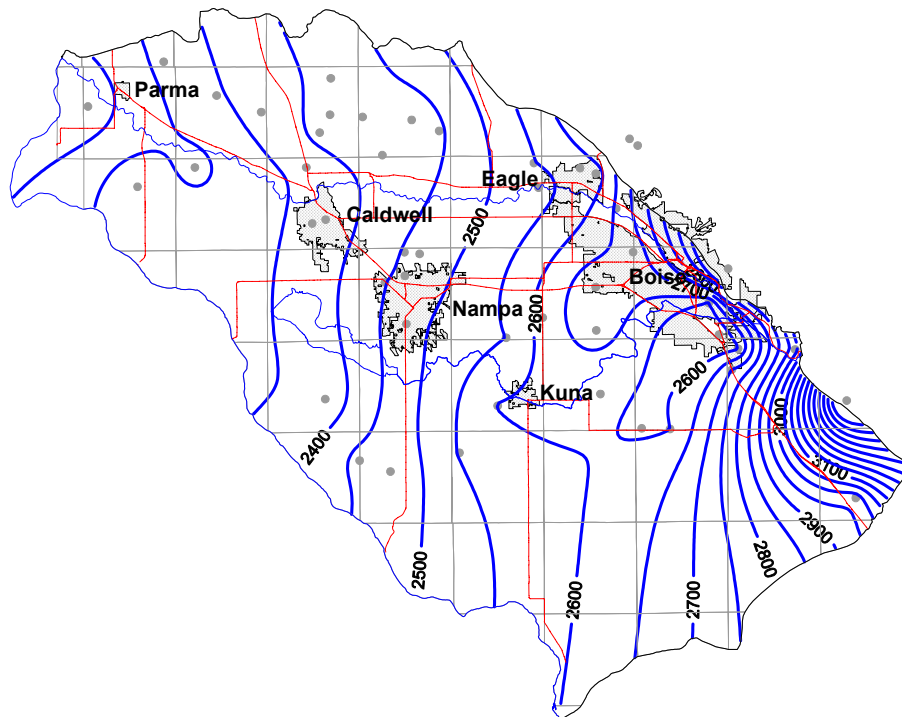


Figure E-5: Fall 1996, intermediate zone (49 wells).

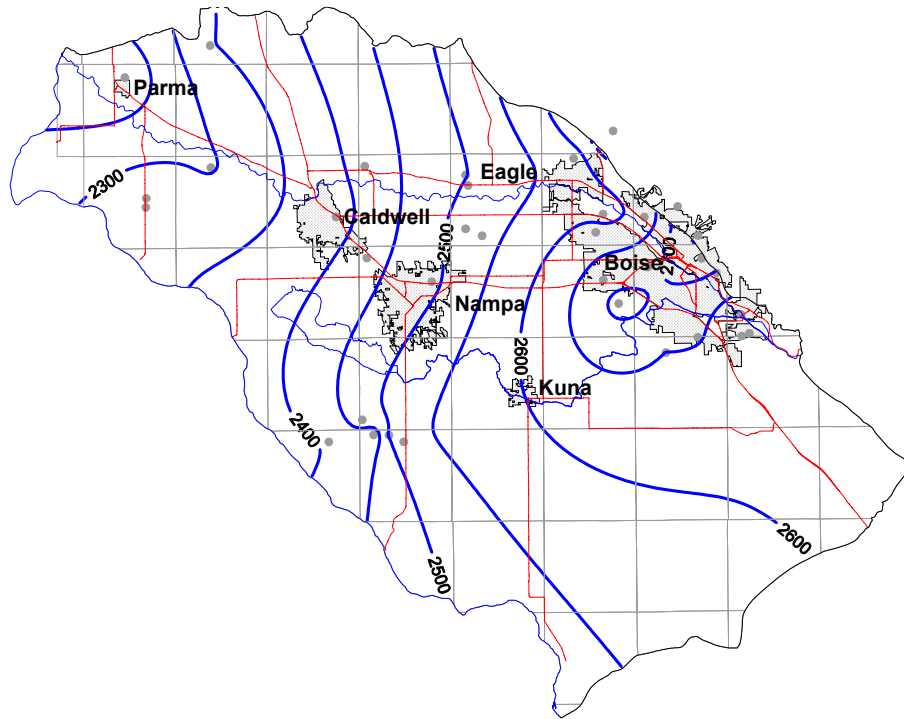


Figure E-6: Fall 1996, deep zone (35 wells).

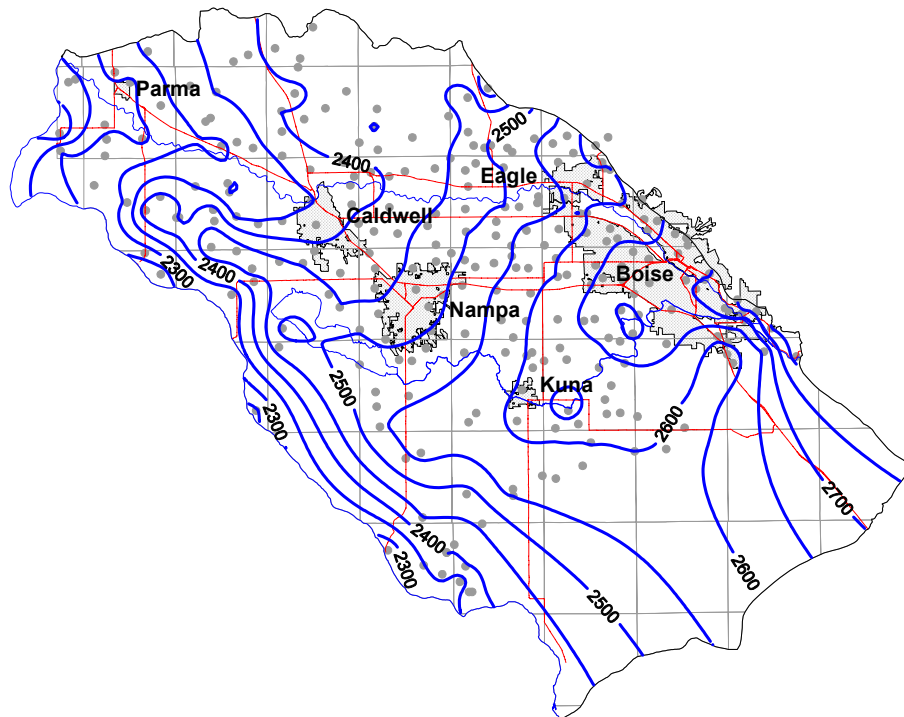


Figure E-7: Spring 1998, shallow zone (259 wells).

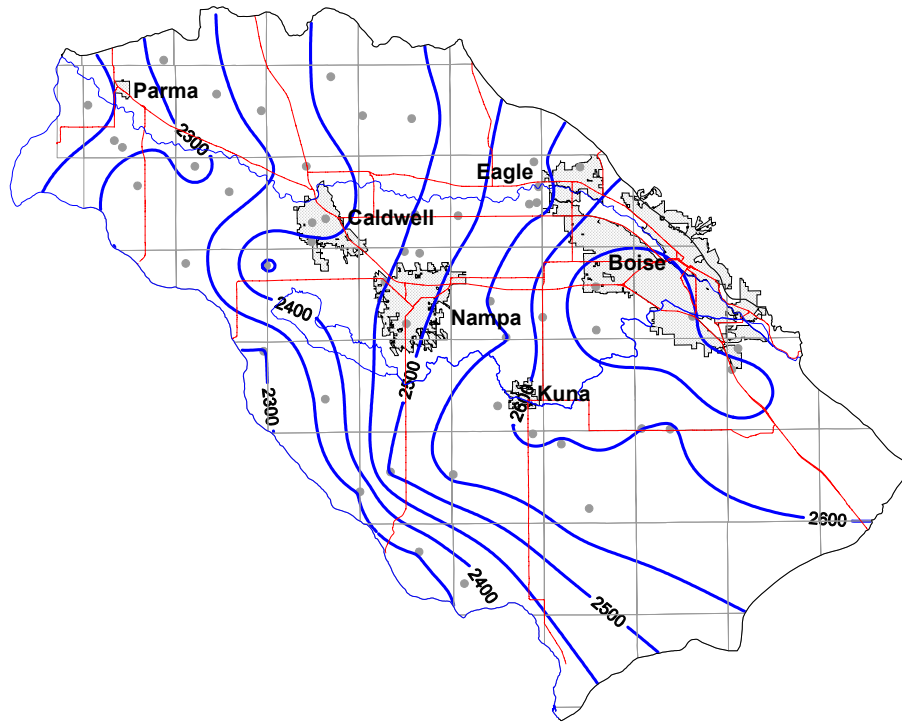


Figure E-8: Spring 1998, intermediate zone (50 wells).

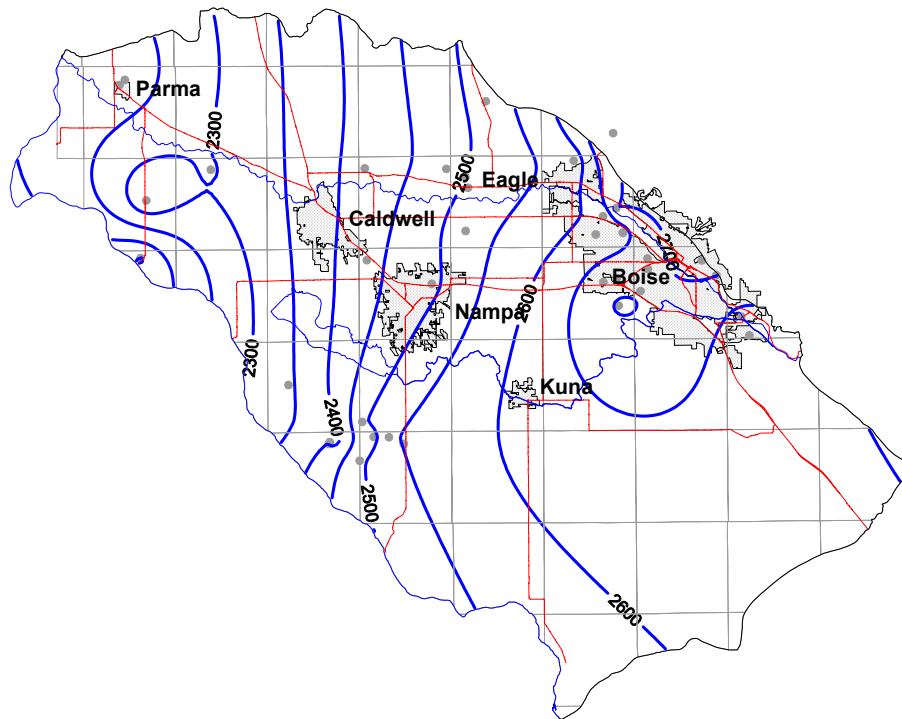


Figure E-9: Spring 1998, deep zone (38 wells).

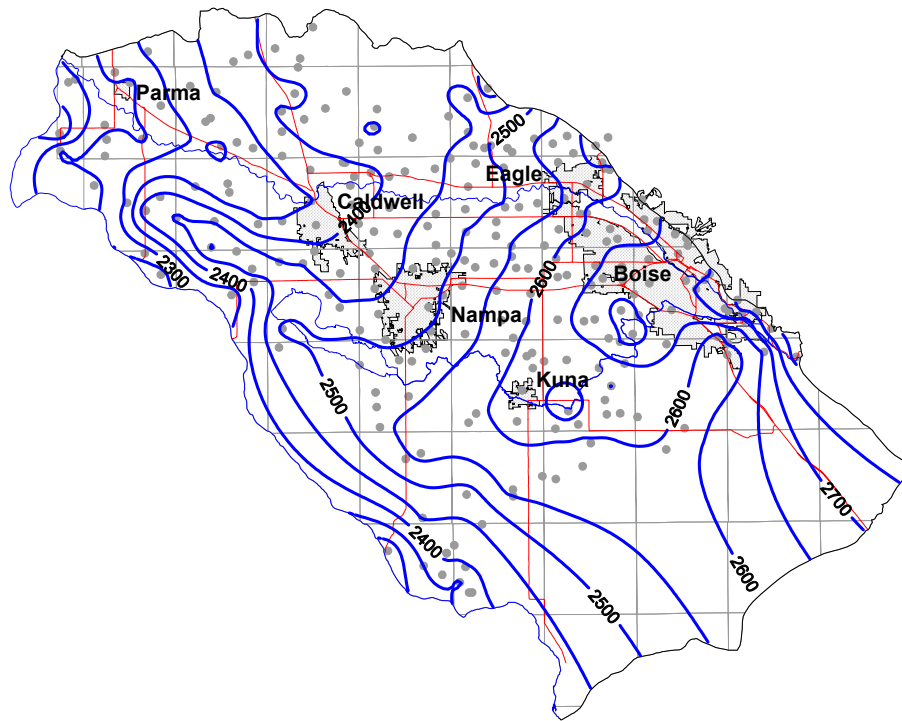


Figure E-10: Fall 1998, shallow zone (245 wells).

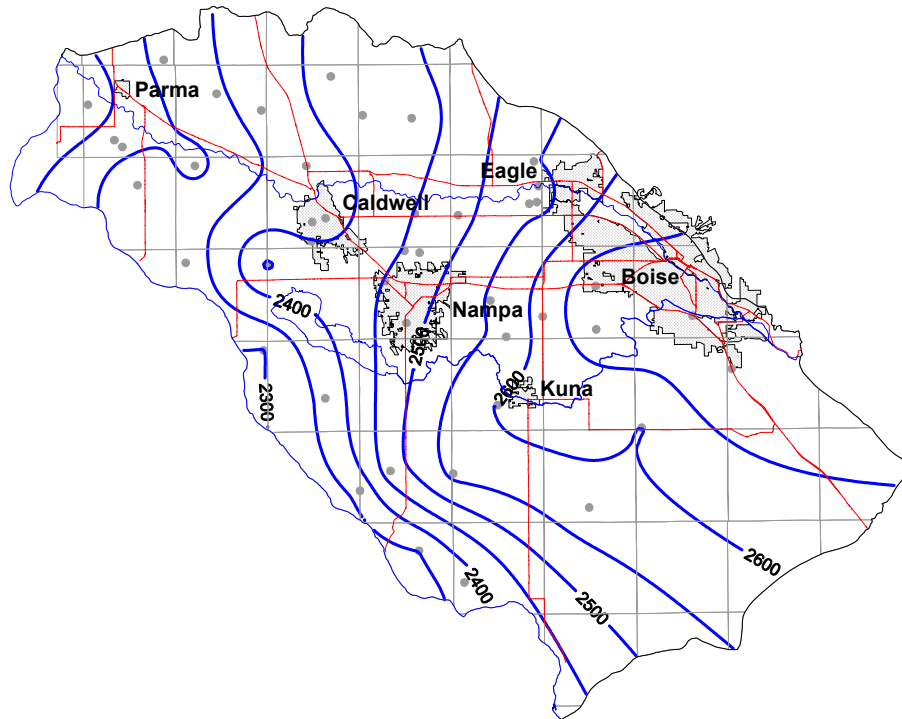


Figure E-11: Fall 1998, intermediate zone (44 wells).

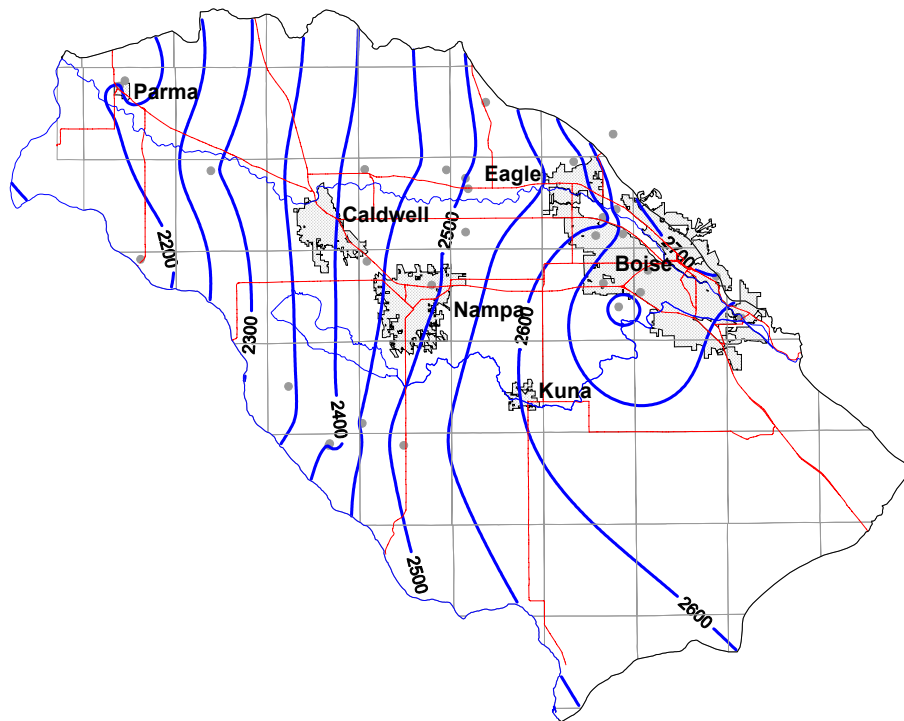


Figure E-12: Fall 1998, deep zone (29 wells).

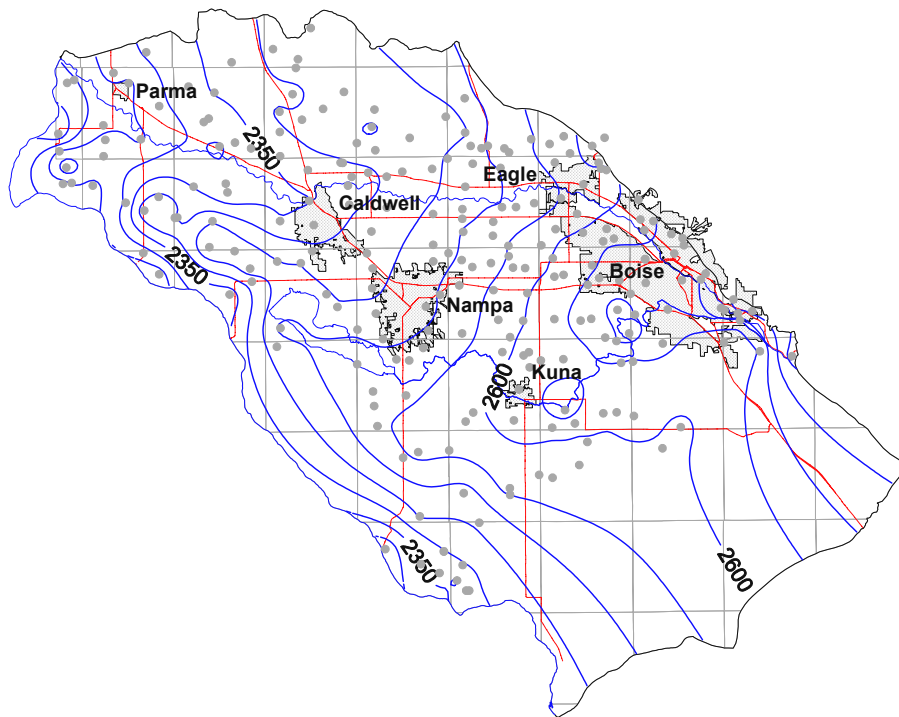


Figure E-13: Spring 2000, shallow zone (238 wells).

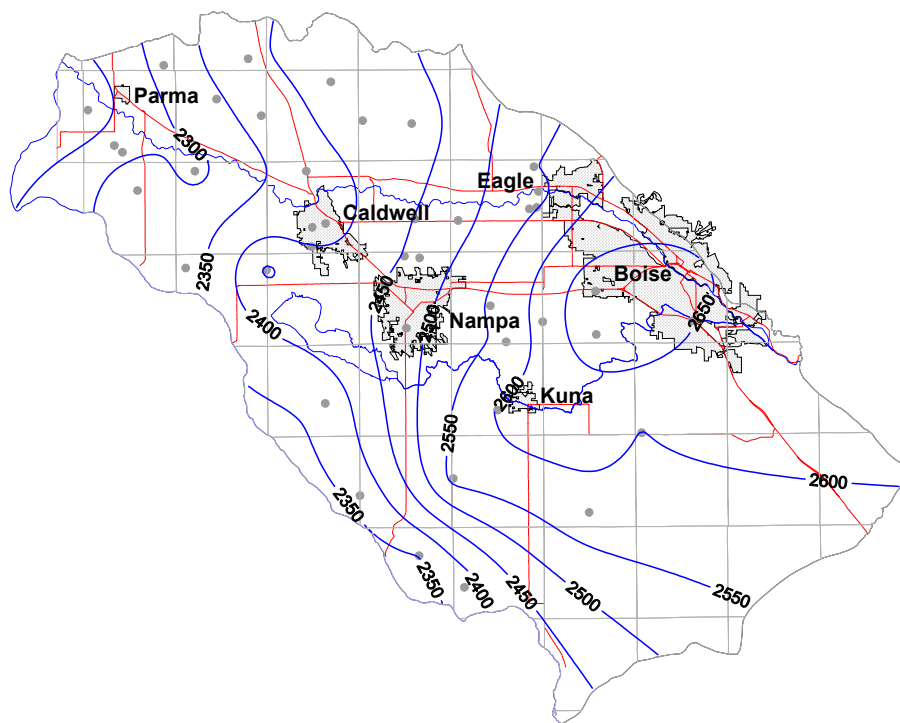


Figure E-14: Spring 2000, intermediate zone (42 wells).

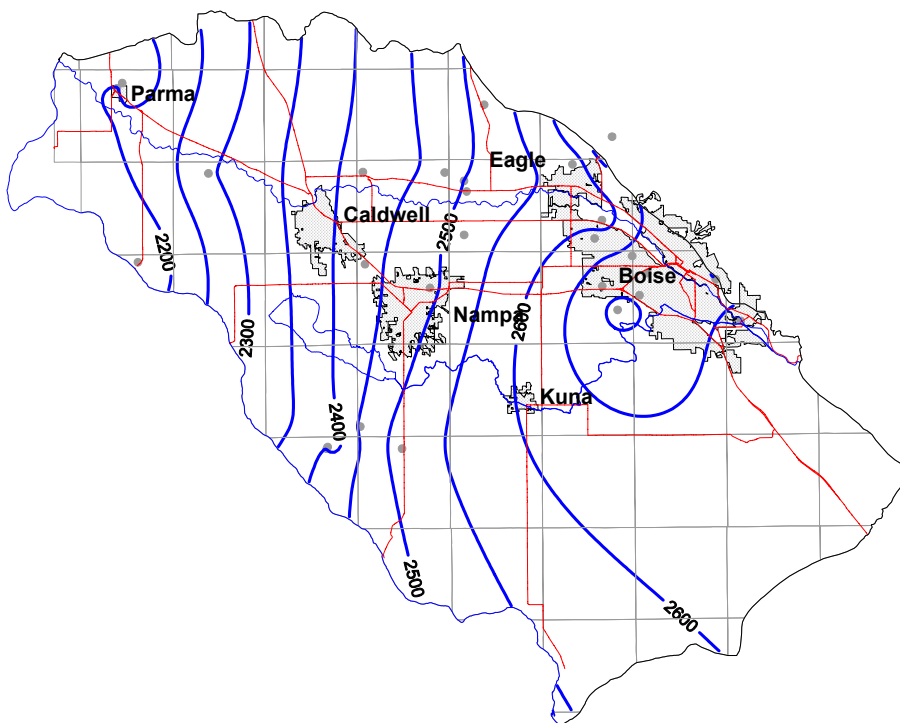


Figure E-15: Spring 2000, deep zone (27 wells).

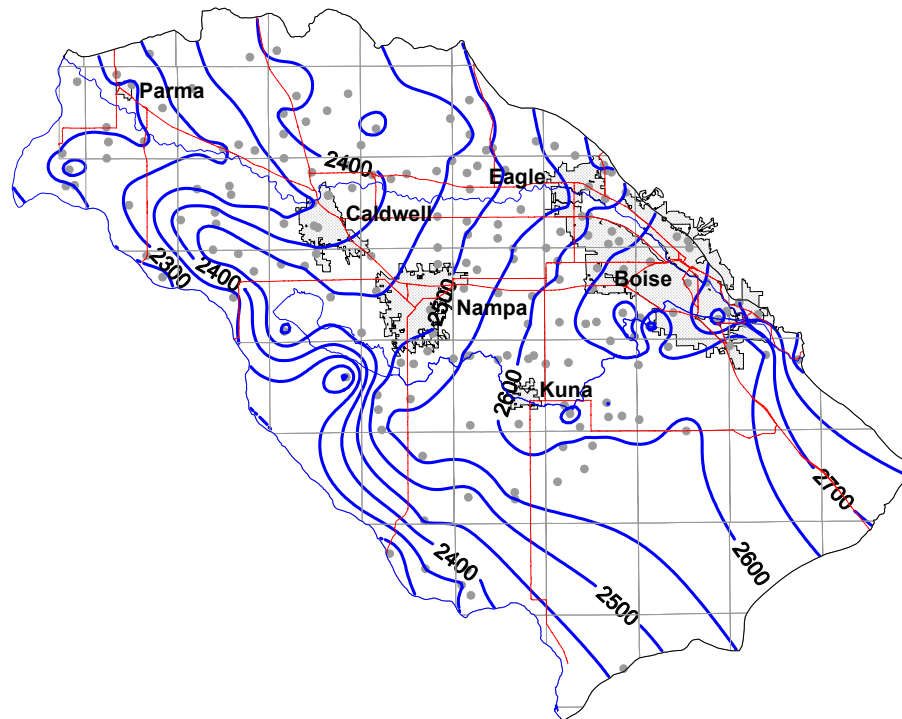


Figure E-16: Fall 2000, shallow zone (16 wells).

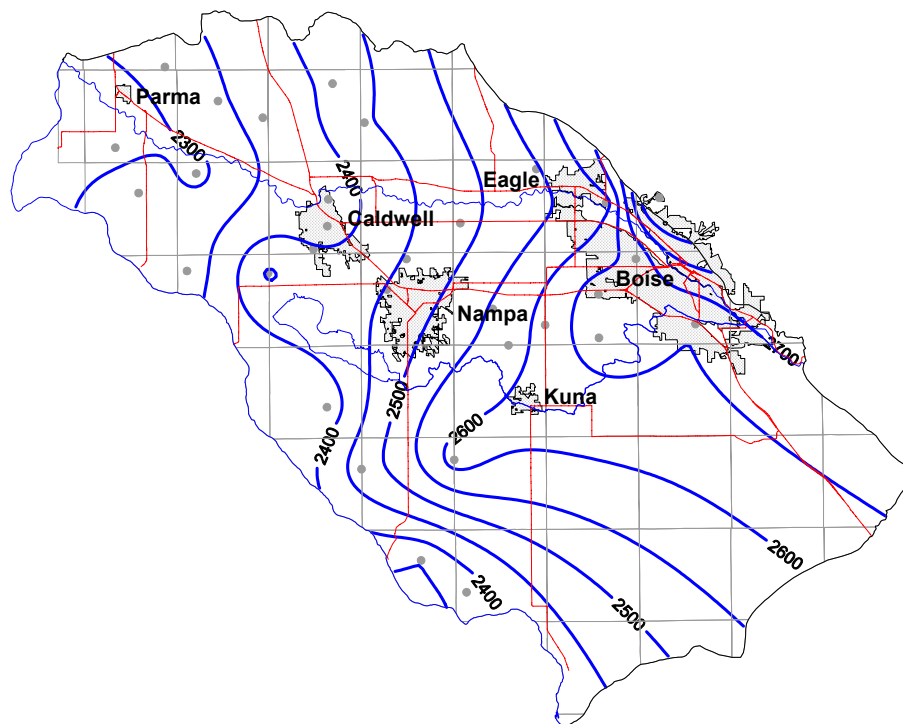


Figure E-17: Fall 2000, intermediate zone (34 wells).

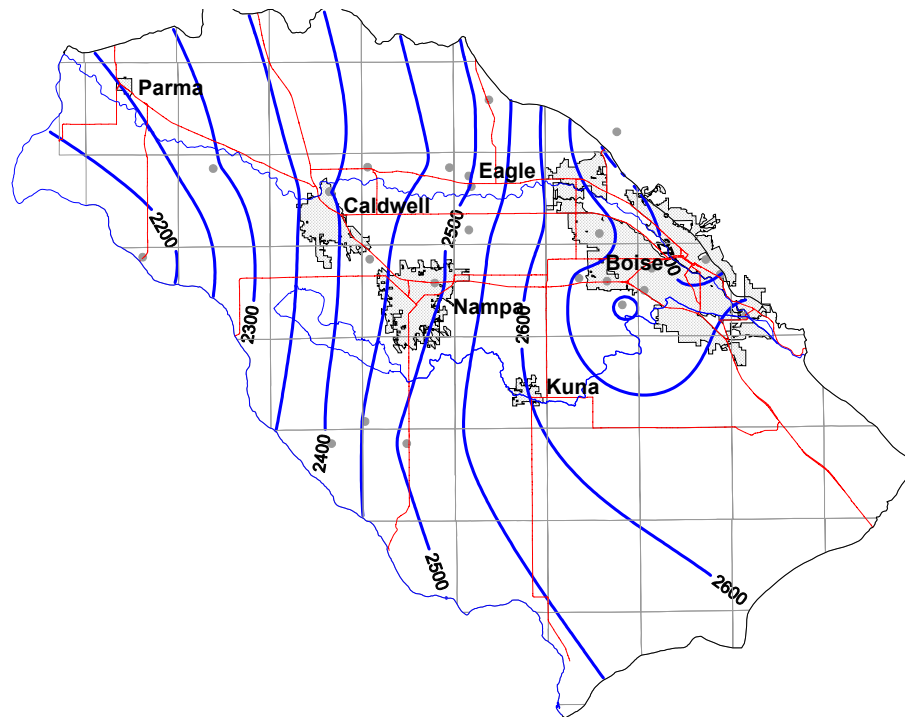


Figure E-18: Fall 2000, deep zone (26 wells).

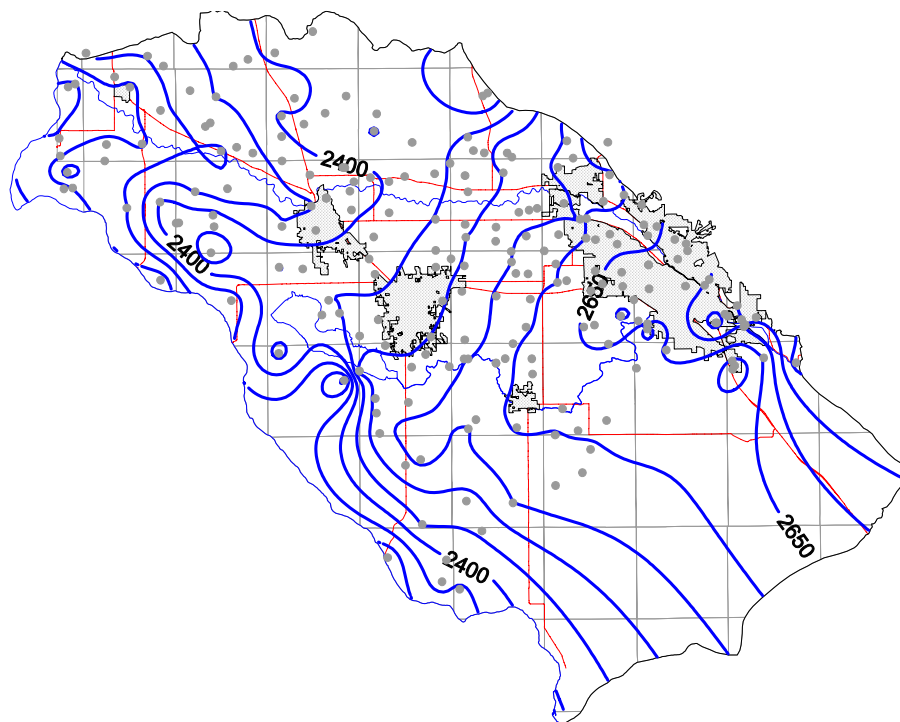


Figure E-19: Fall 2001, shallow zone (212 wells).

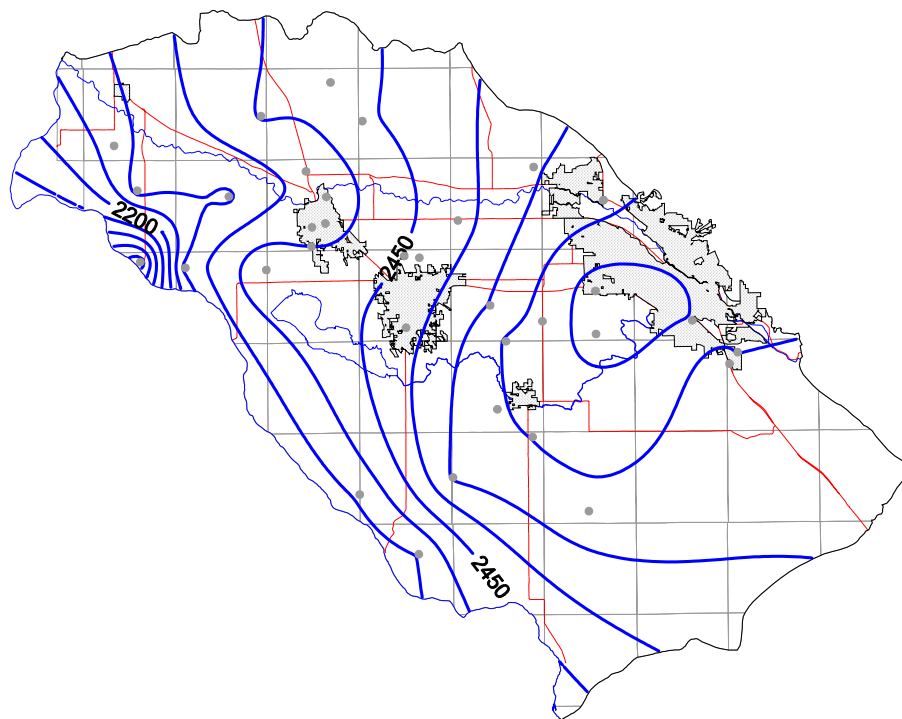


Figure E-20: Fall 2001, intermediate zone (35 wells).

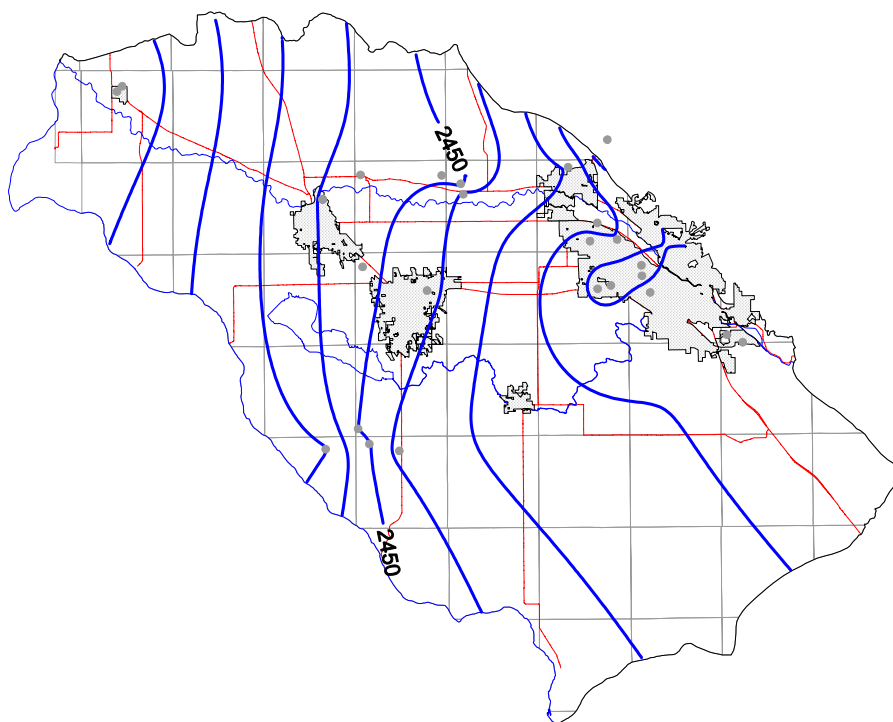
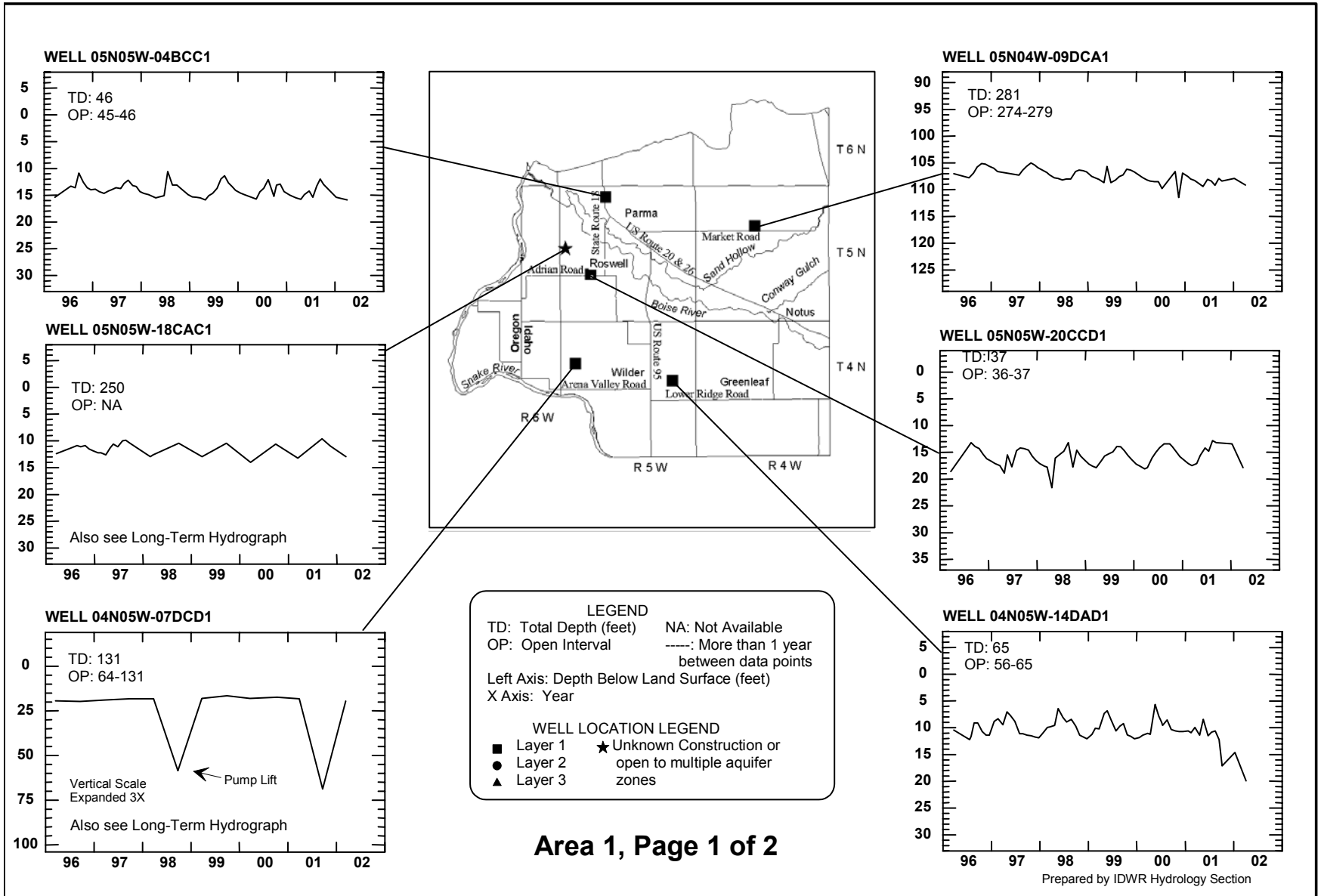
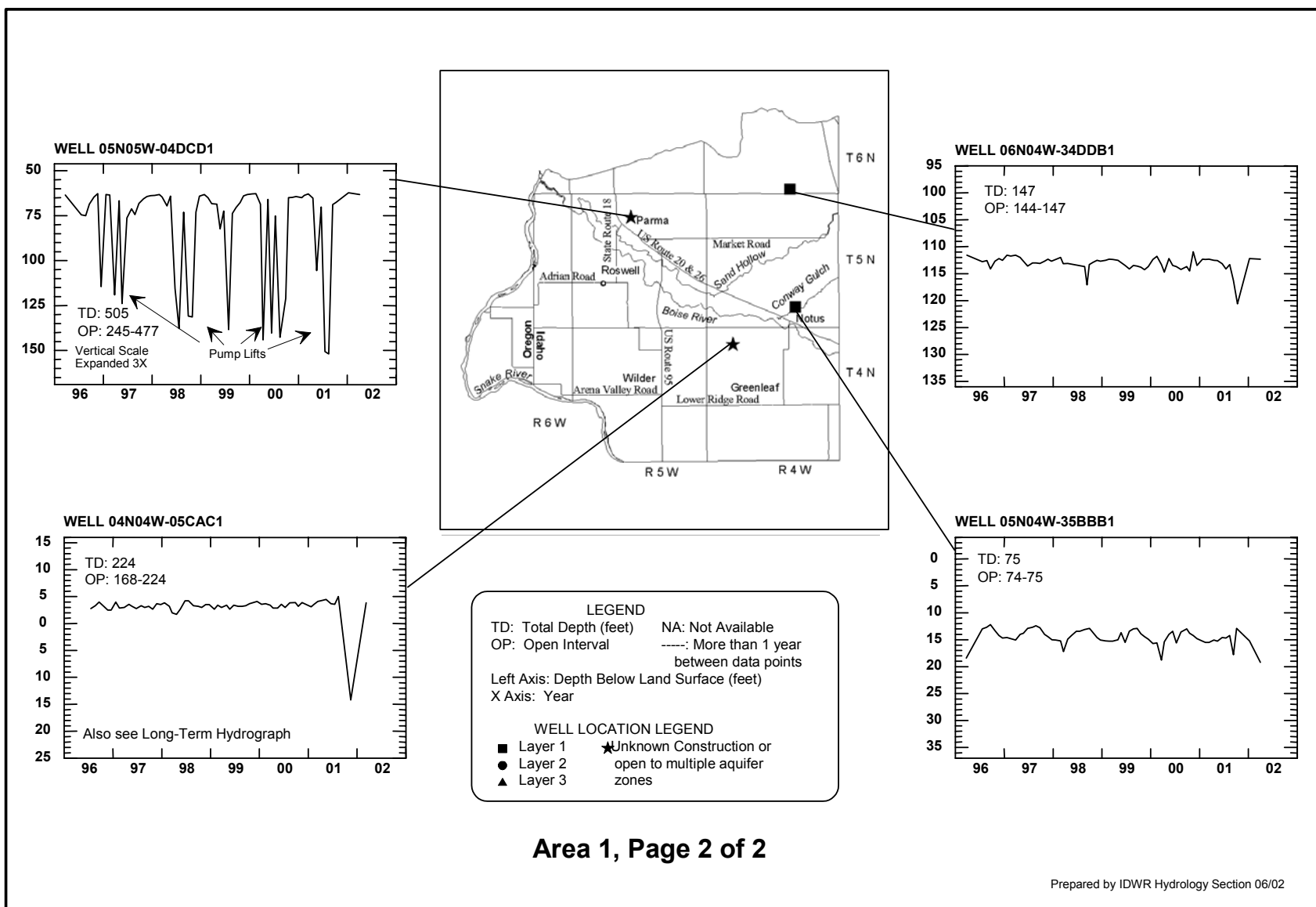
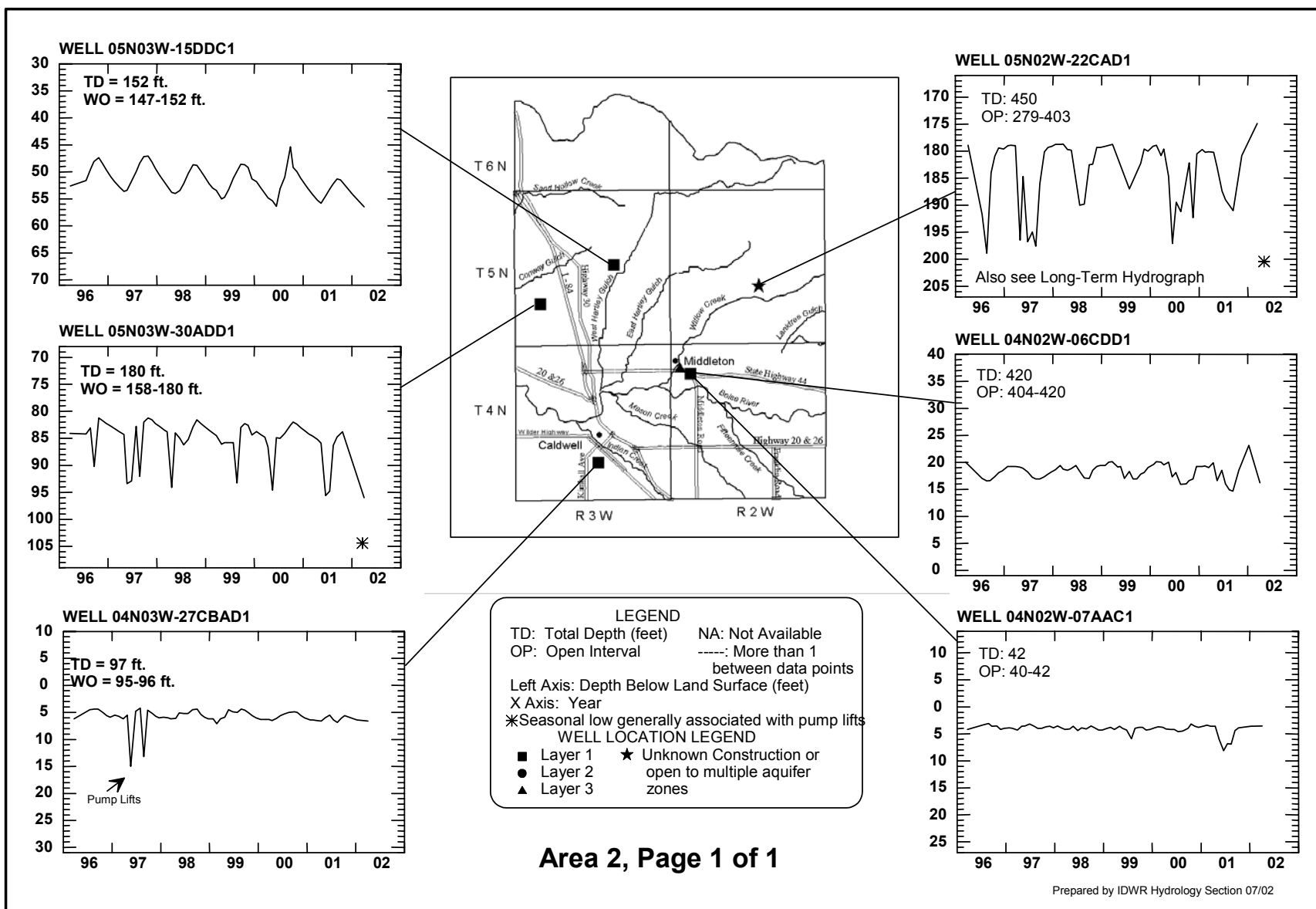


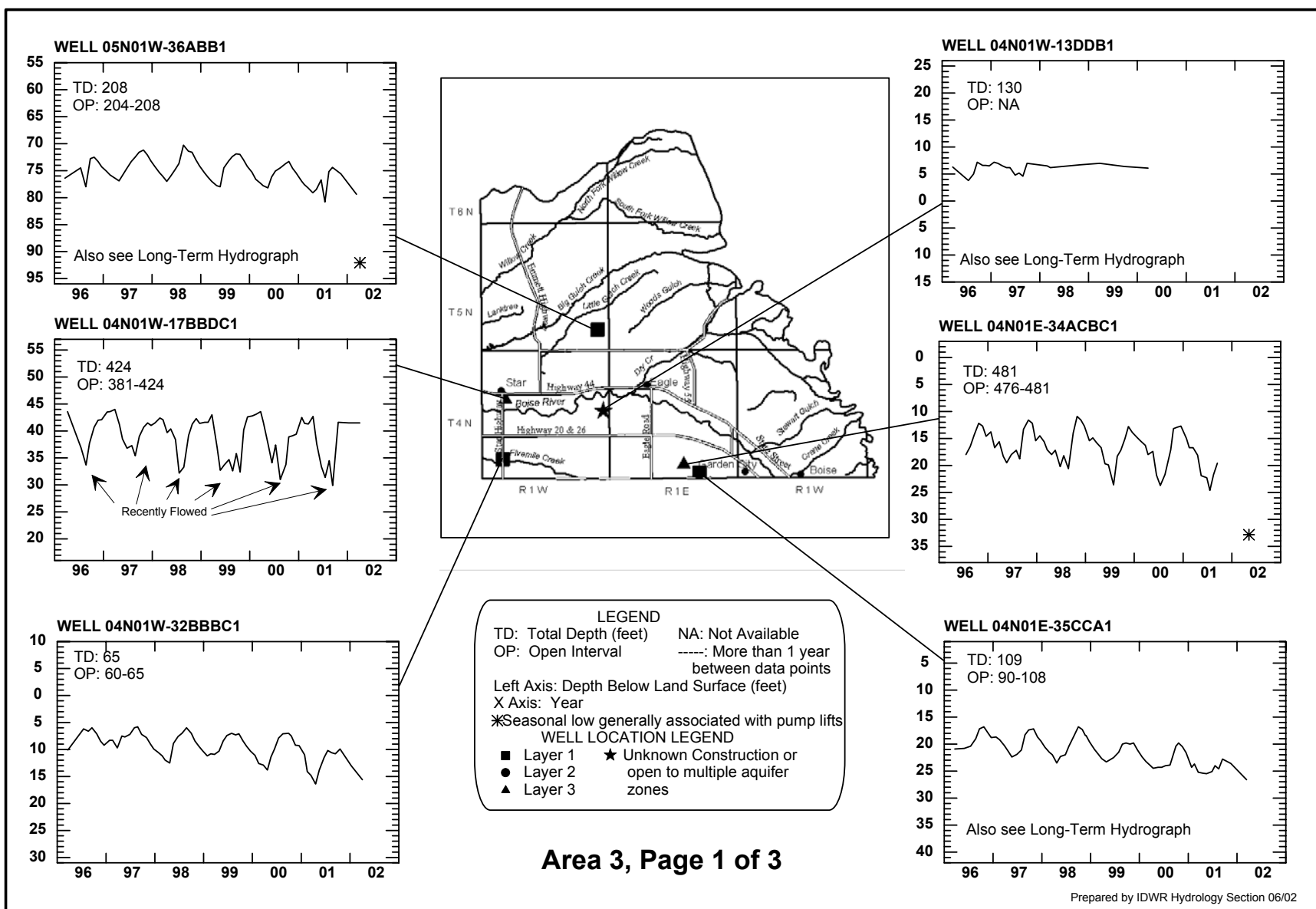
Figure E-21: Fall 2001, deep zone (27 wells).

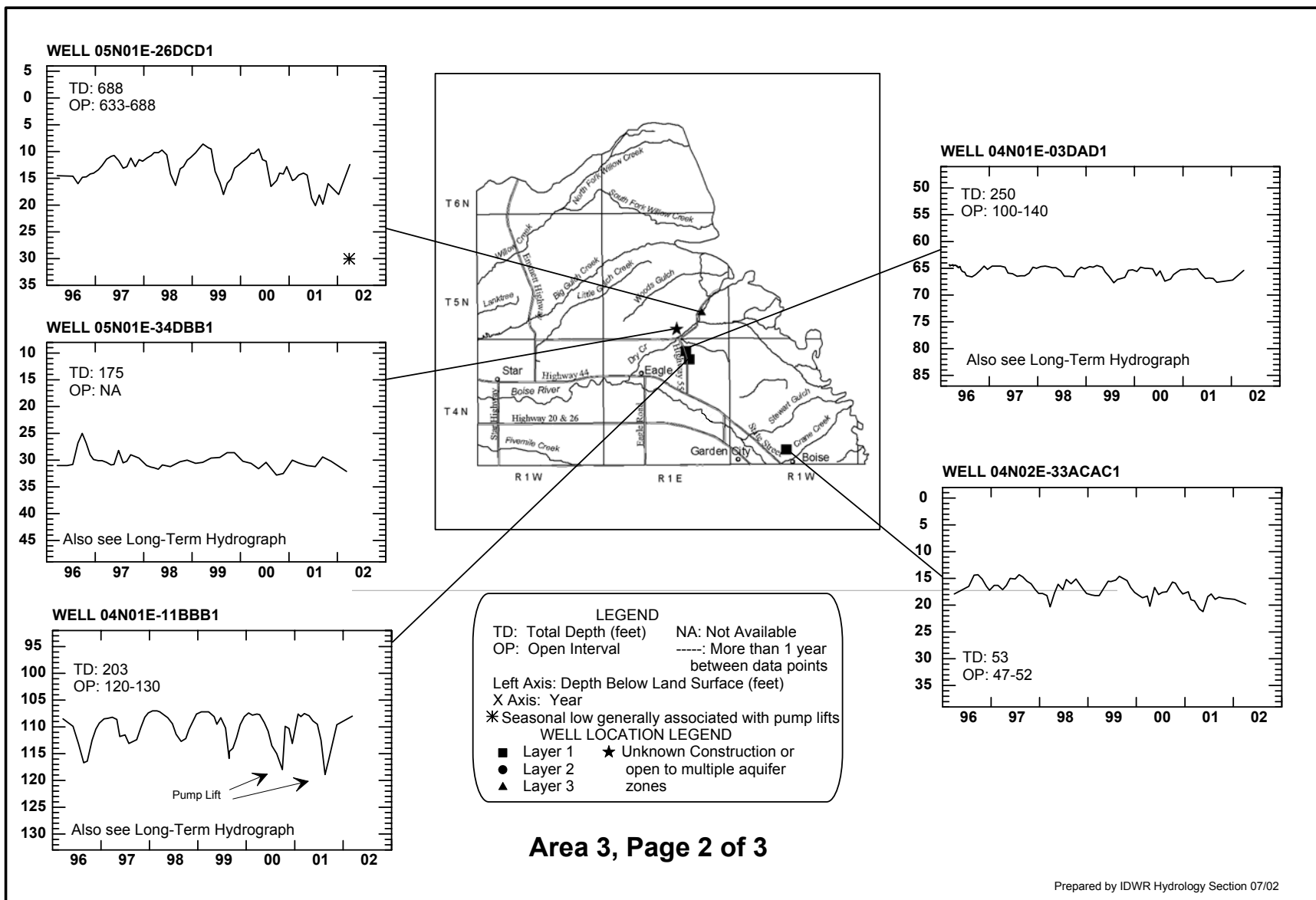
Appendix F. HYDROGRAPHS

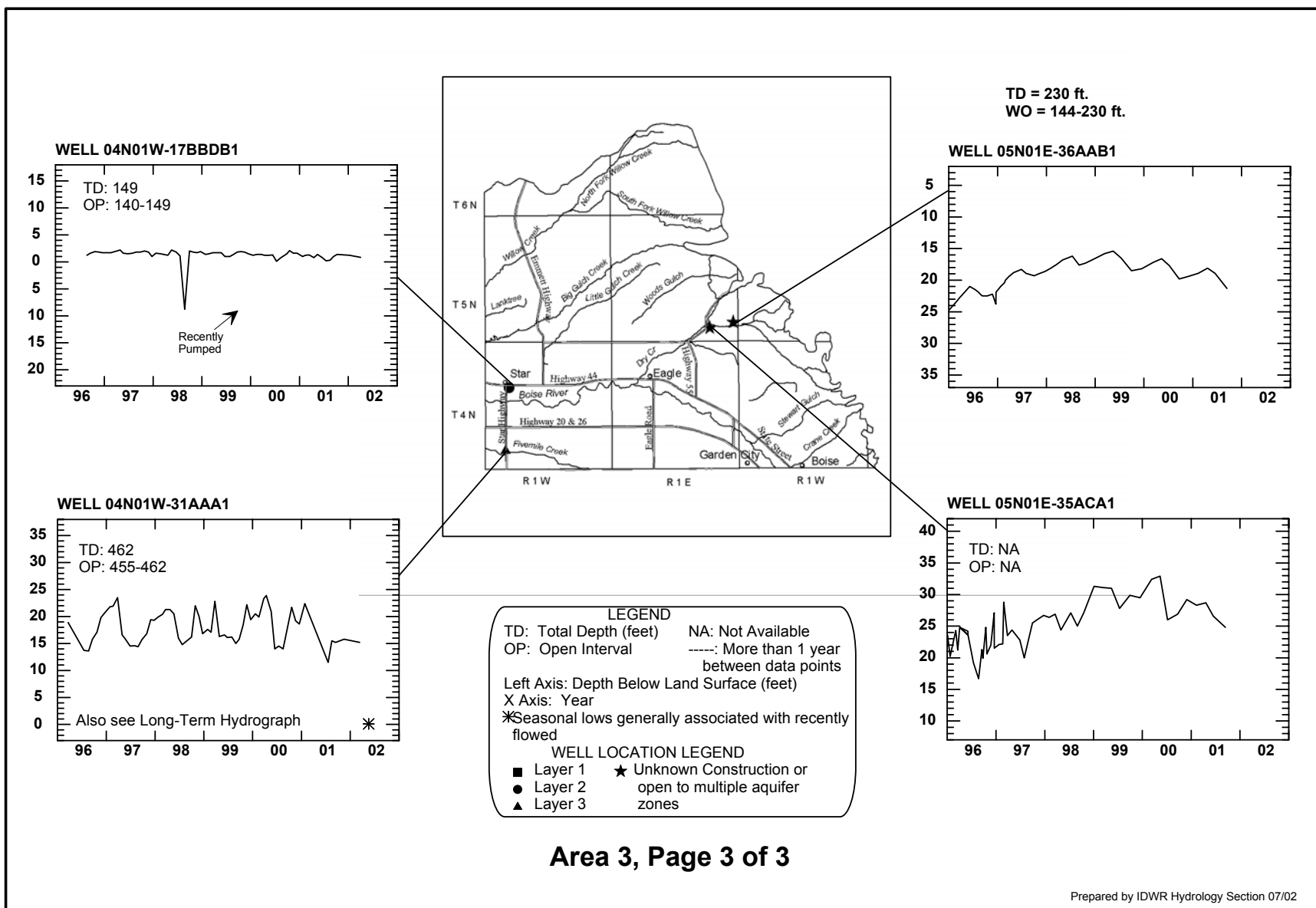


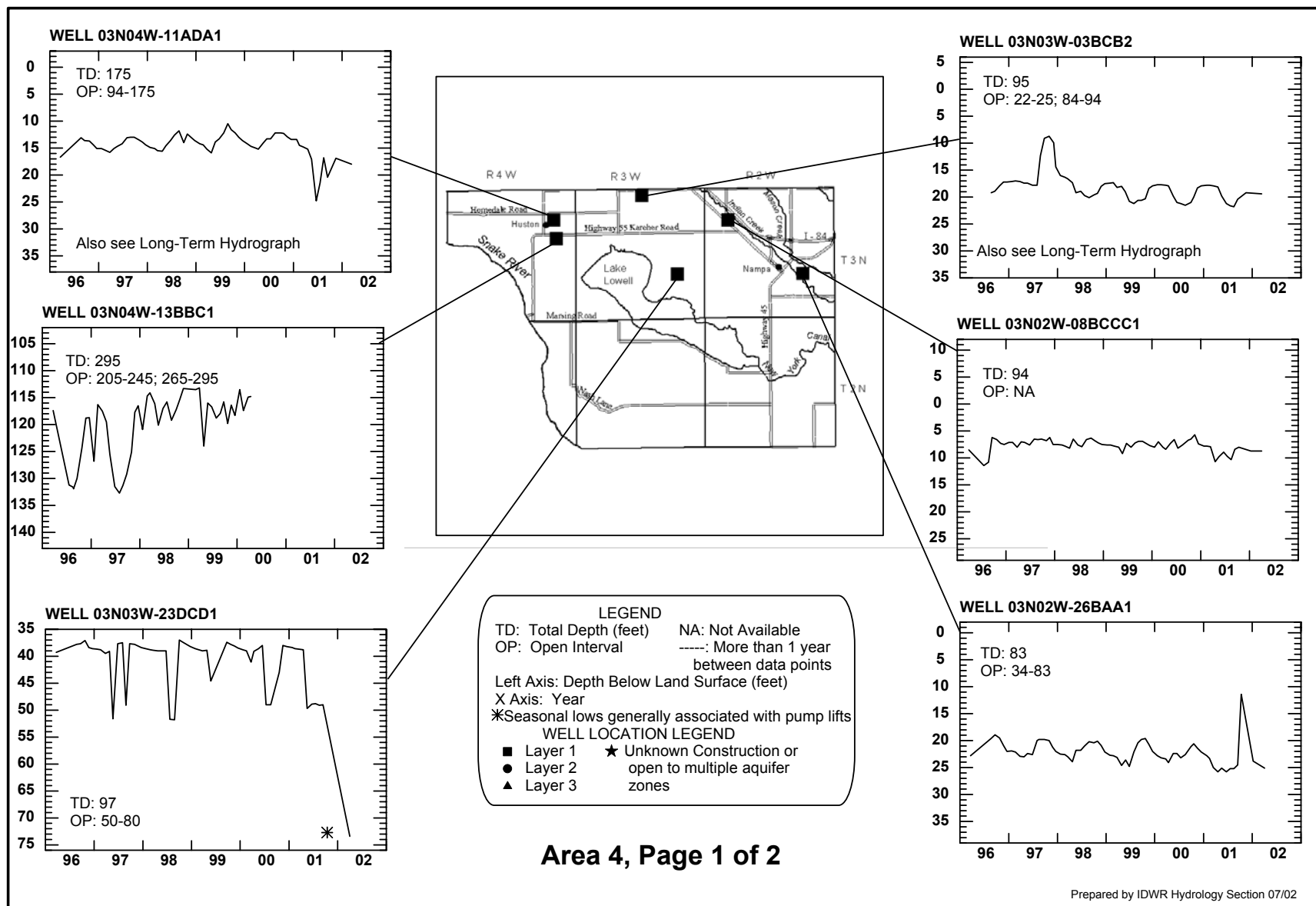


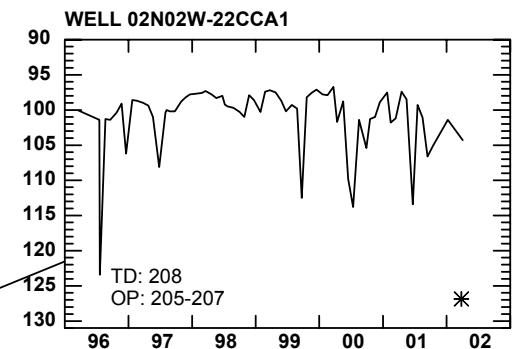
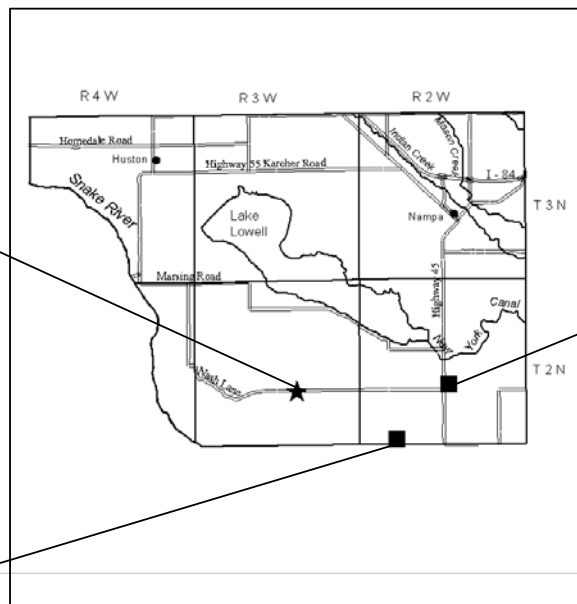
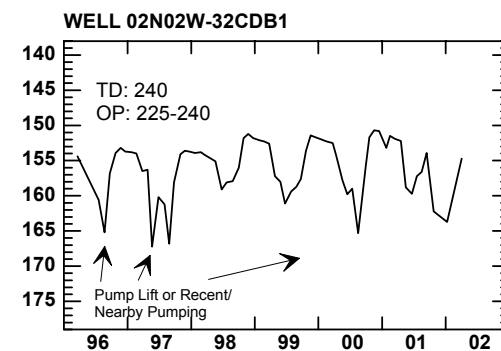












LEGEND

TD: Total Depth (feet) NA: Not Available
OP: Open Interval -----: More than 1 year between data points

Left Axis: Depth Below Land Surface (feet)
X Axis: Year

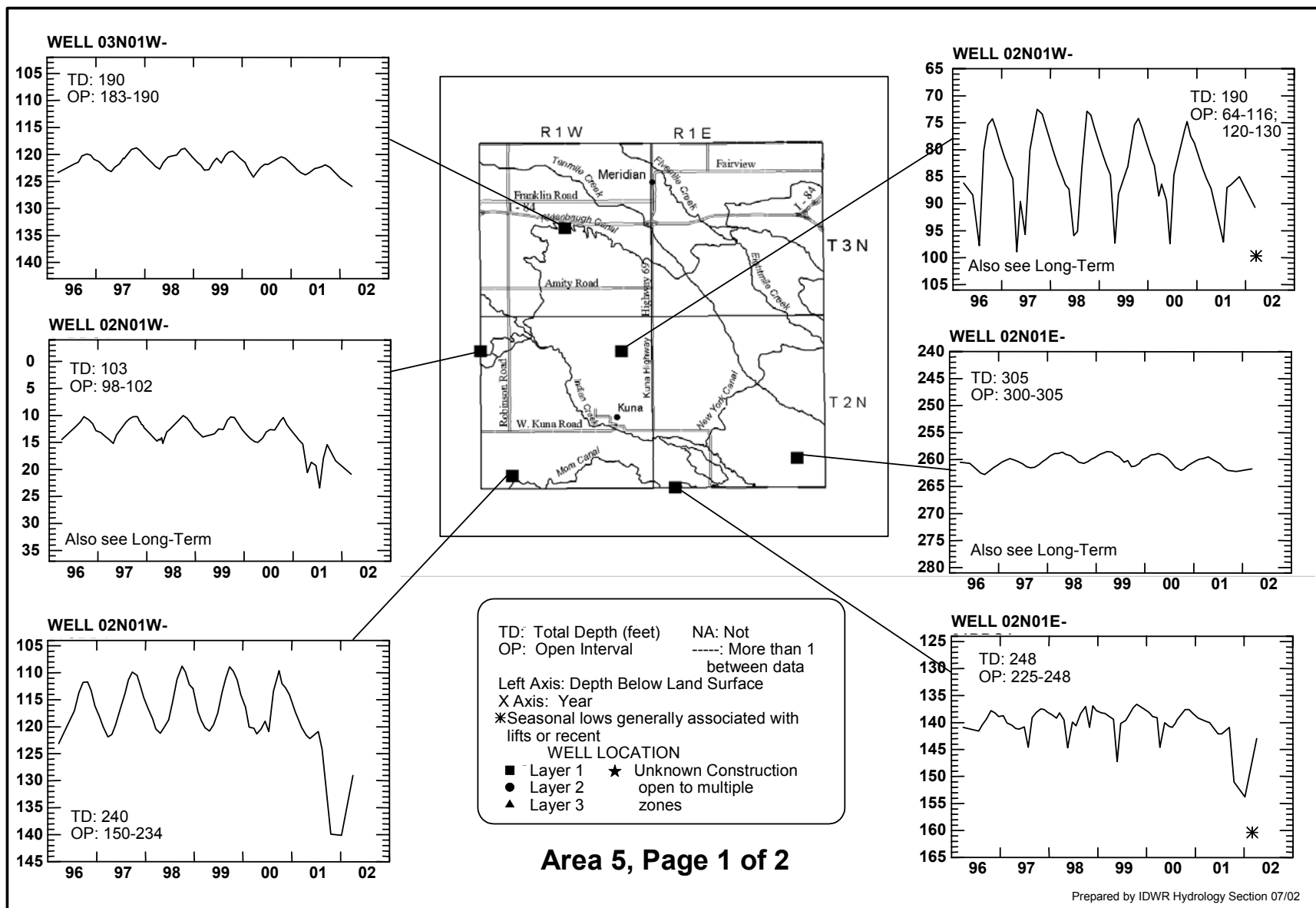
*Seasonal lows generally associated with recent pumping

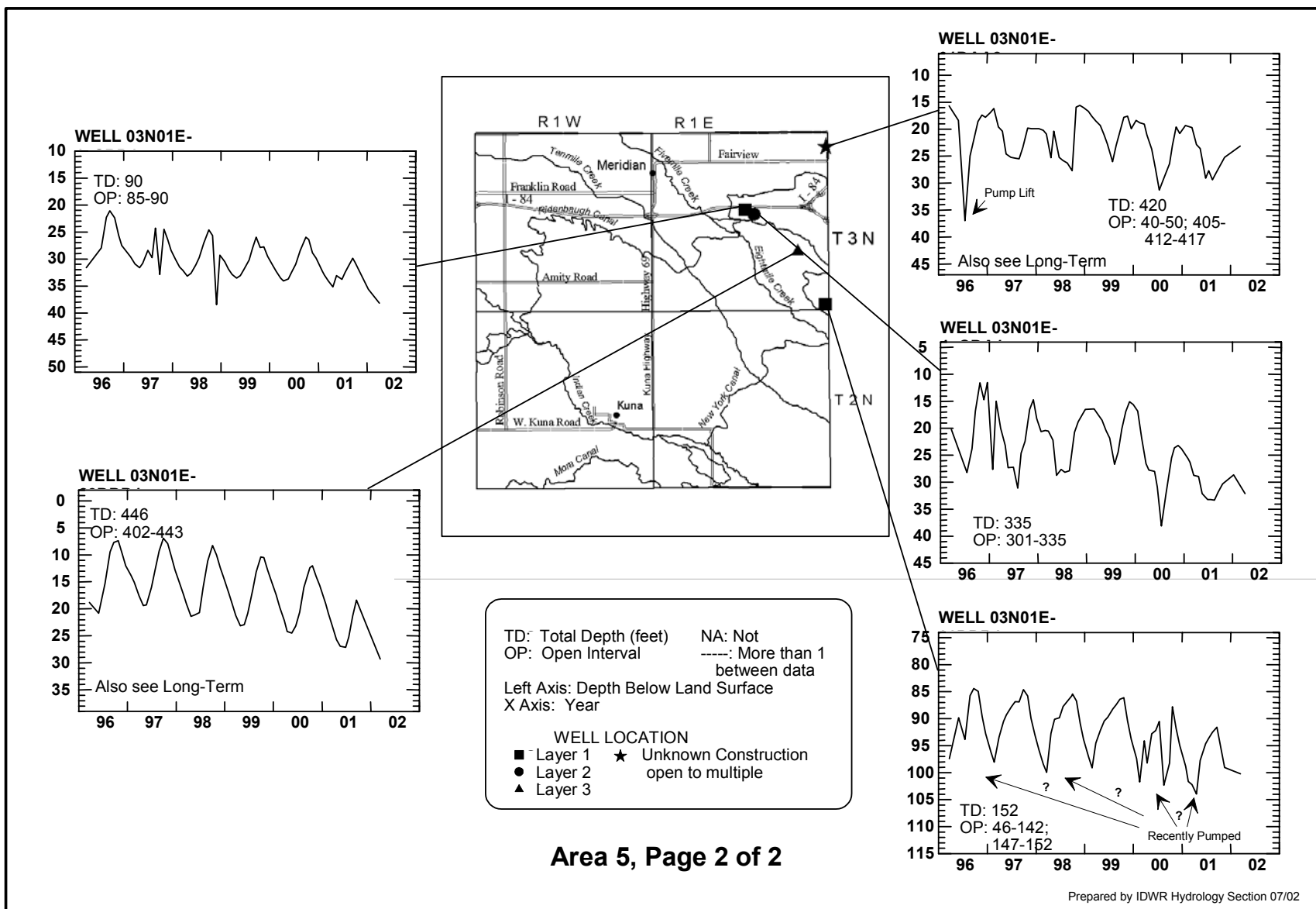
WELL LOCATION LEGEND

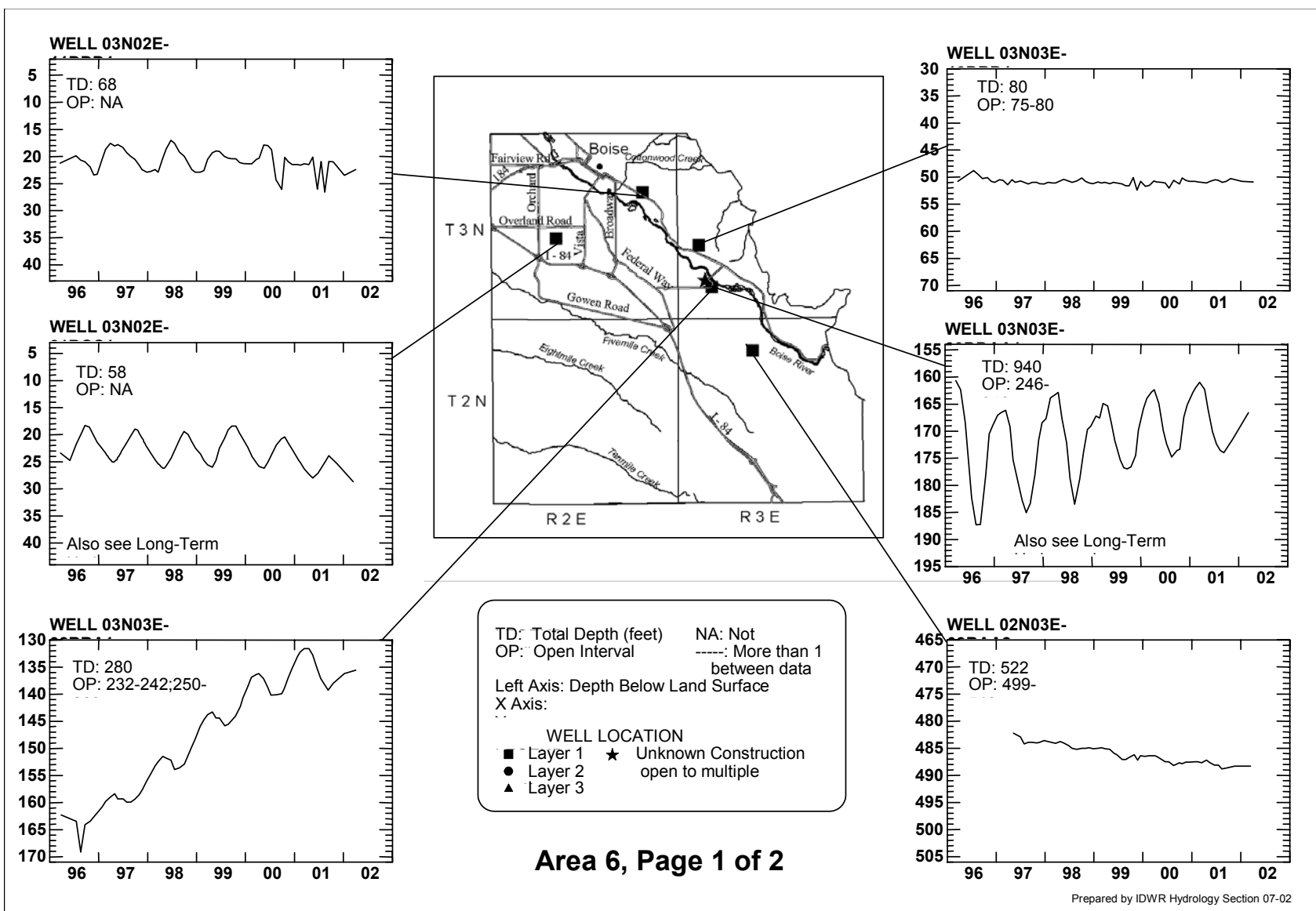
■ Layer 1 ★ Unknown Construction or open to multiple aquifer zones
● Layer 2
▲ Layer 3

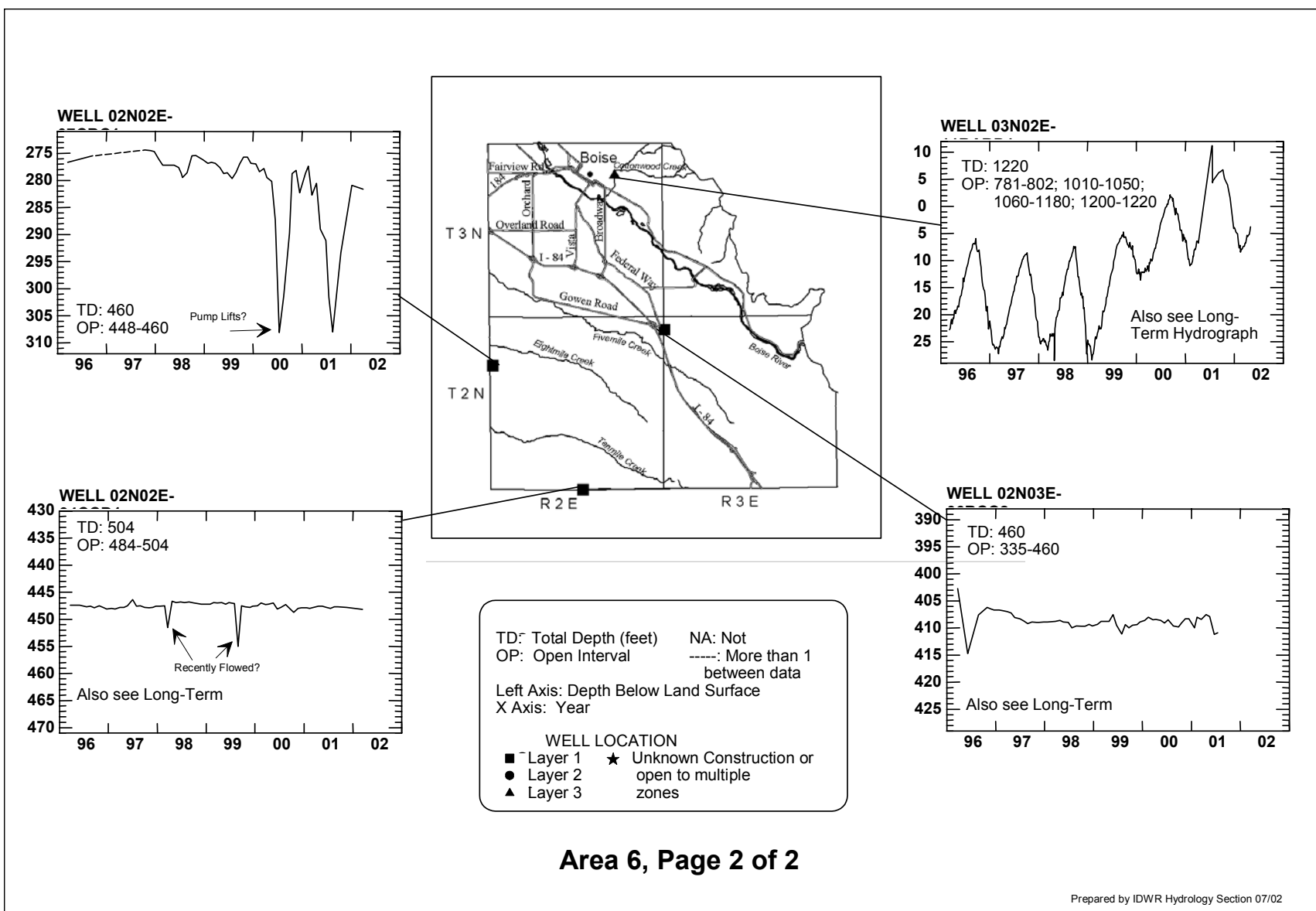
Area 4, Page 2 of 2

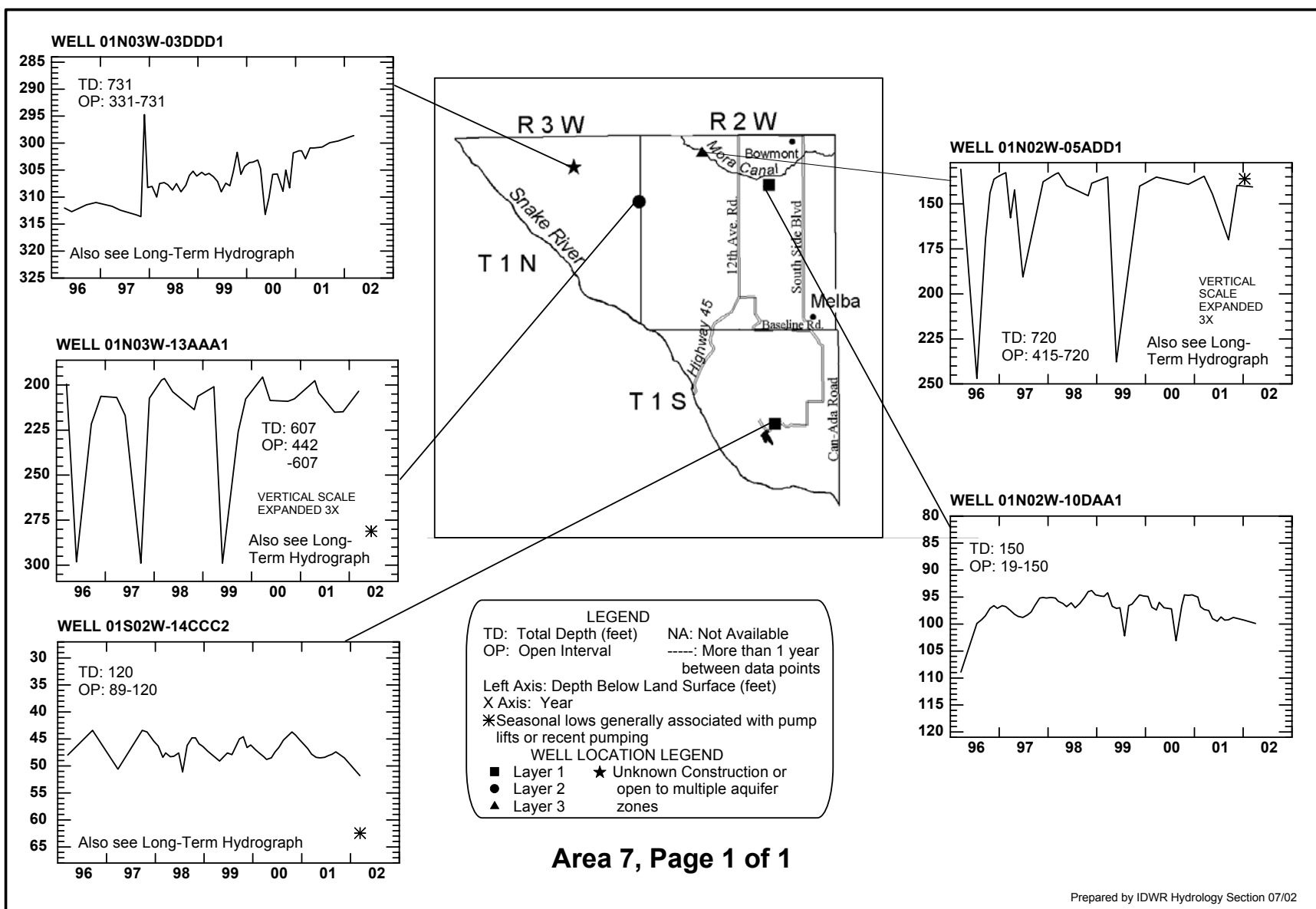
Prepared by IDWR Hydrology Section 07/02

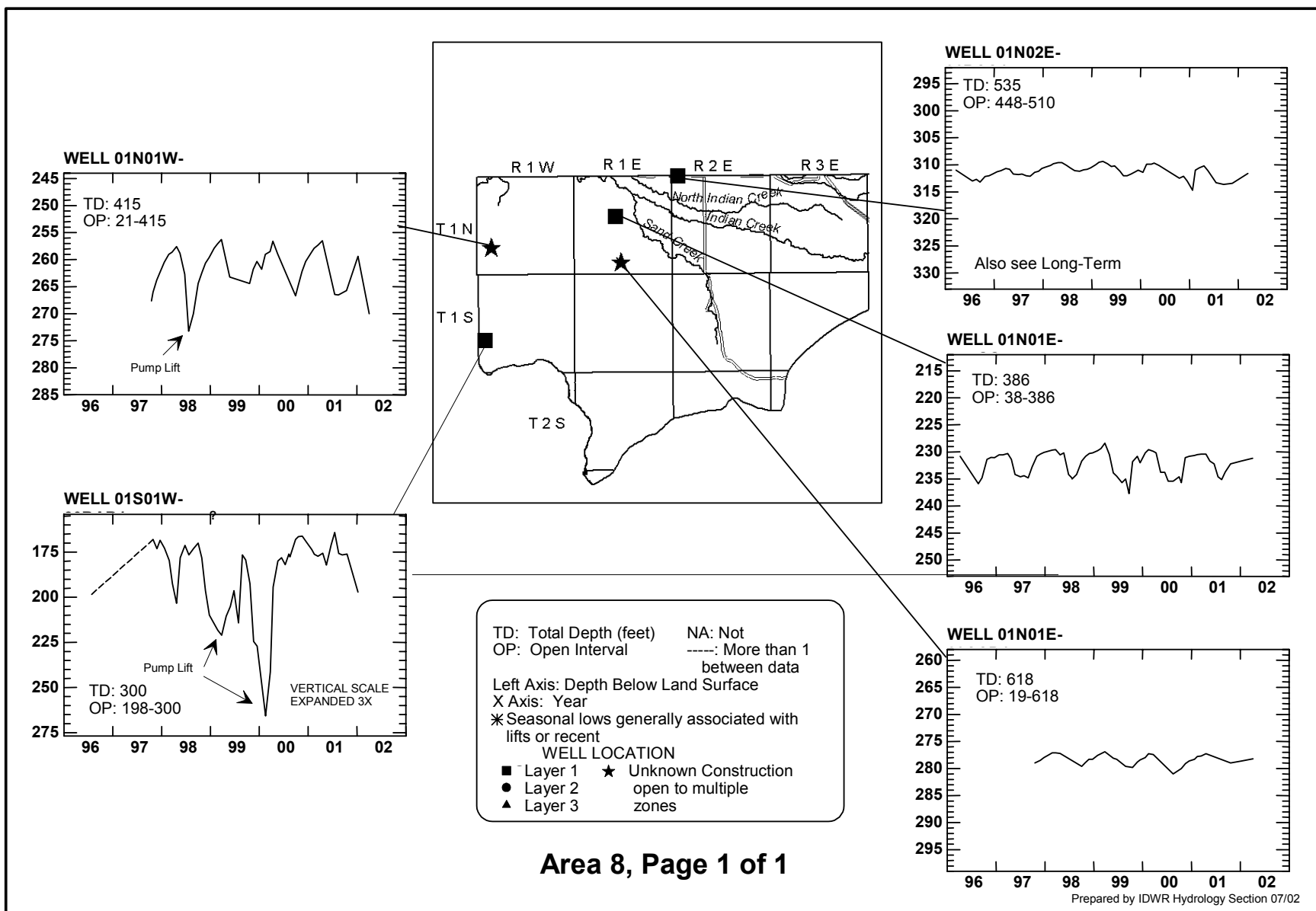


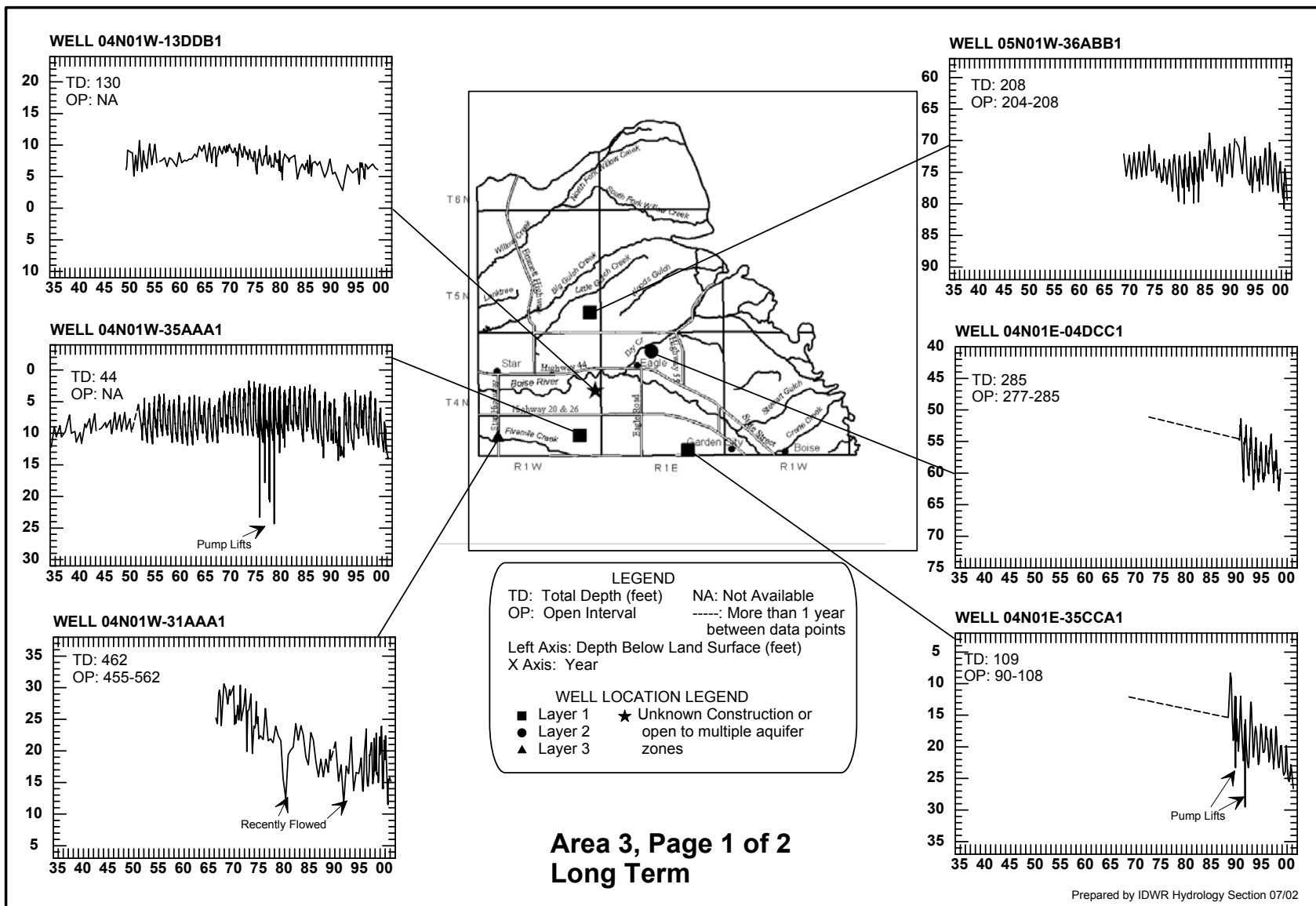


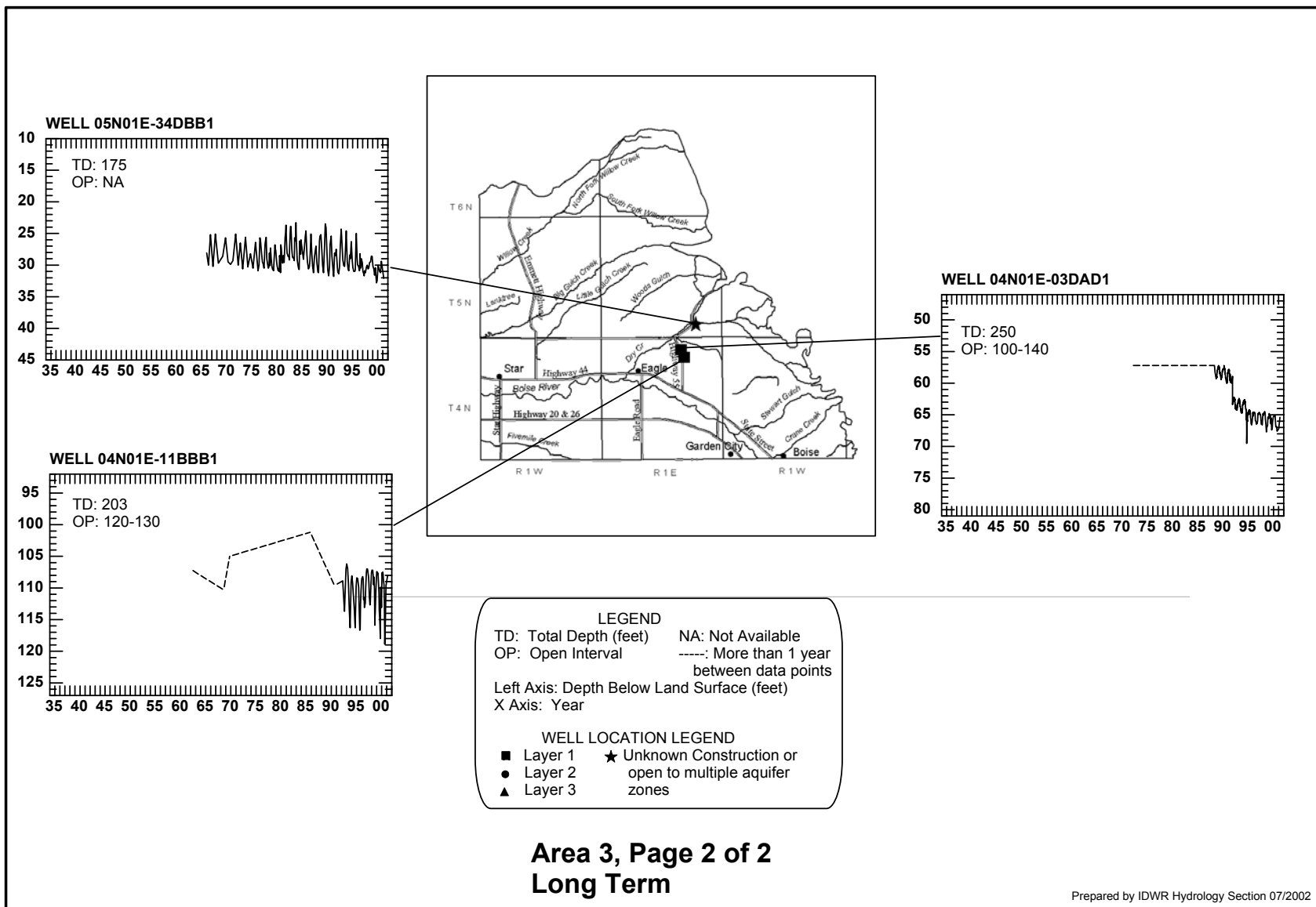




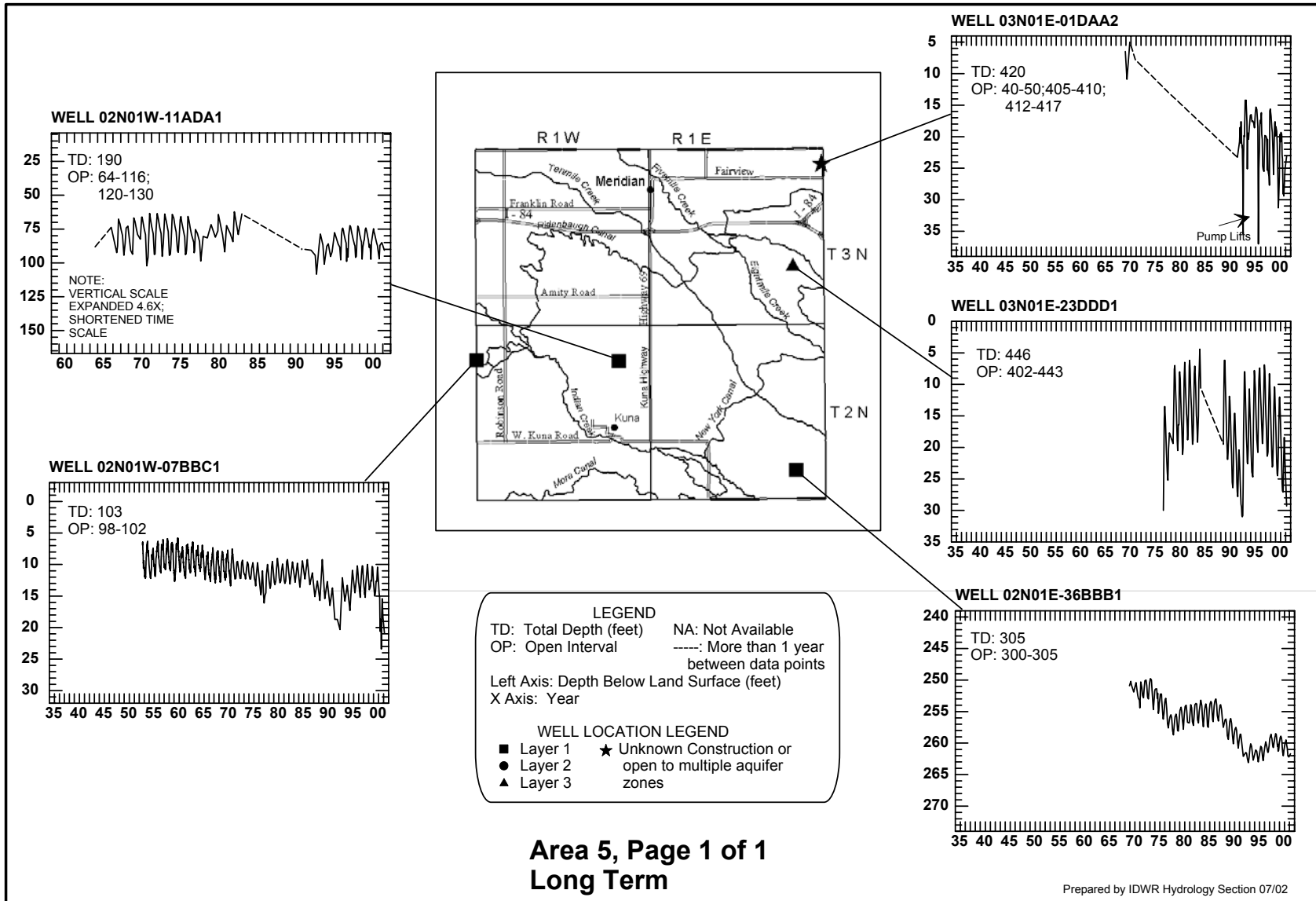


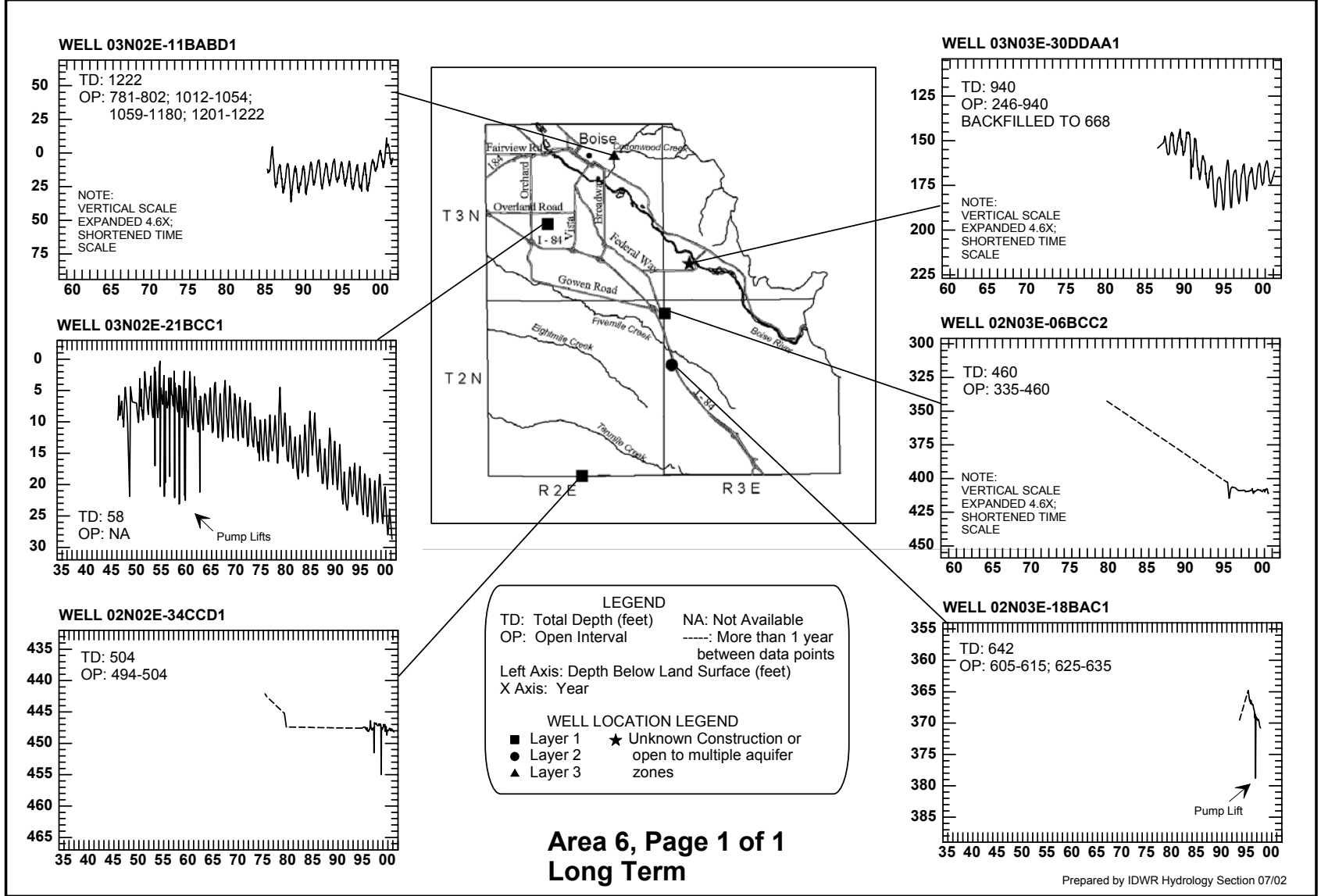


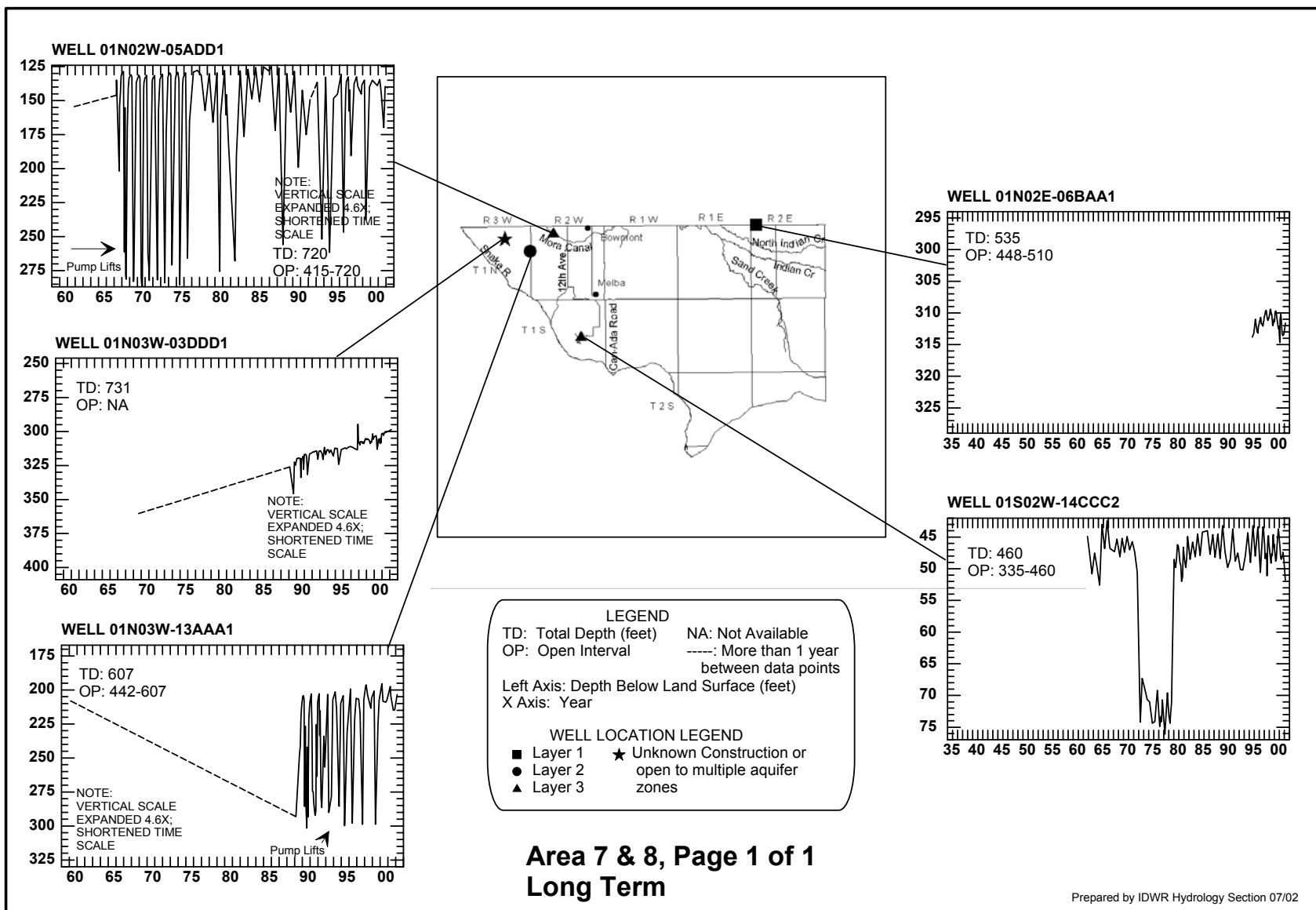






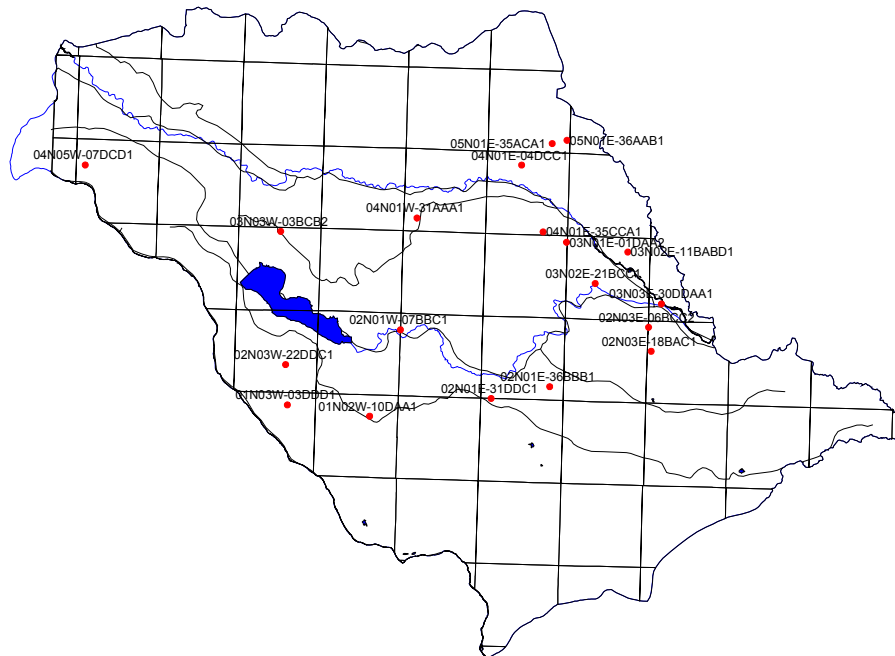




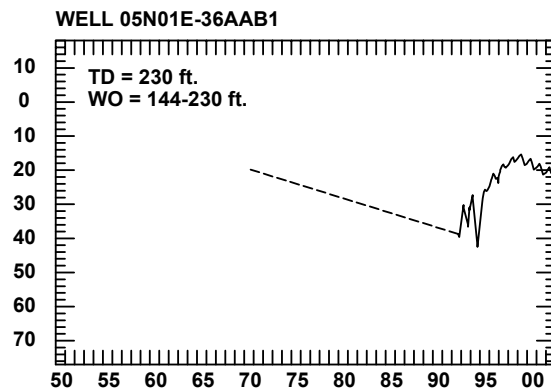
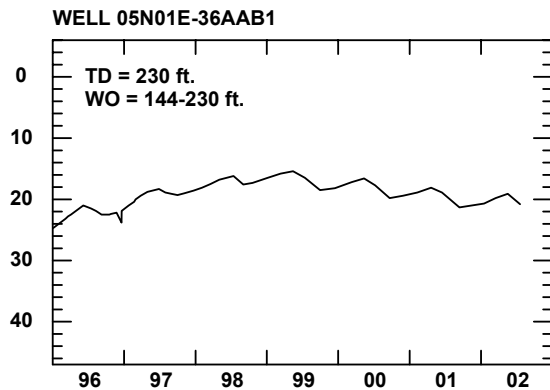


Appendix G. SELECTED HYDROGRAPHS SHOWING CHANGES

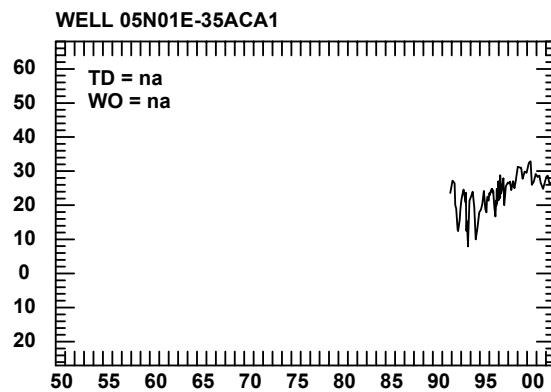
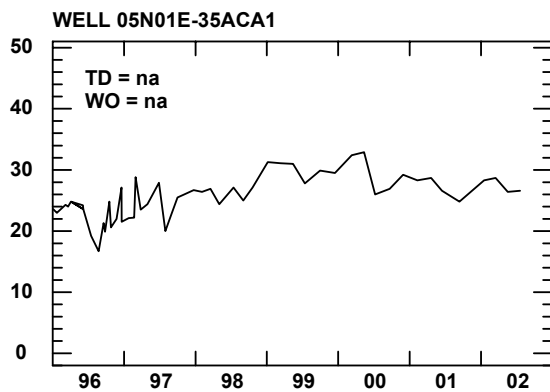
This section repeats selected hydrographs that were shown in the previous appendices, but the discussion regarding water level has changed. Locations of the hydrographs included in this appendix are shown below.



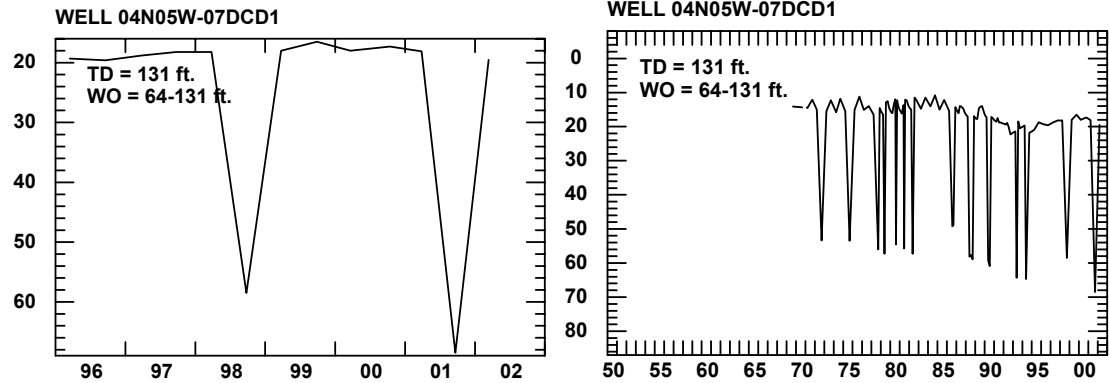
Location of Wells



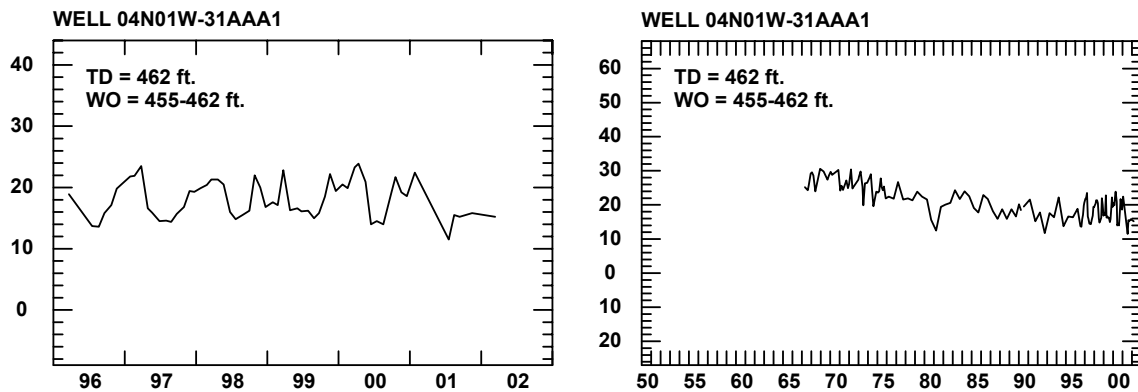
NORTHEAST OF EAGLE, Jeker geothermal well. Per Ken Neely, the increasing shut-in pressures are a result of decreasing production within the geothermal aquifer during the period between 1995 and 1999.



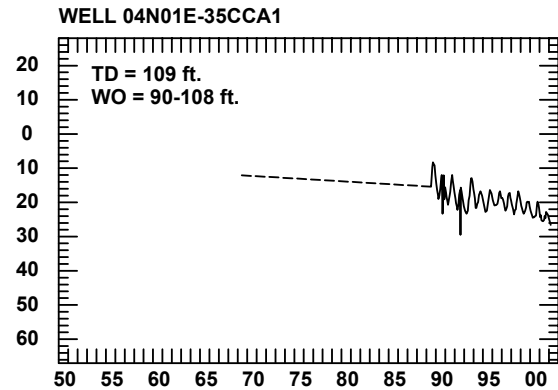
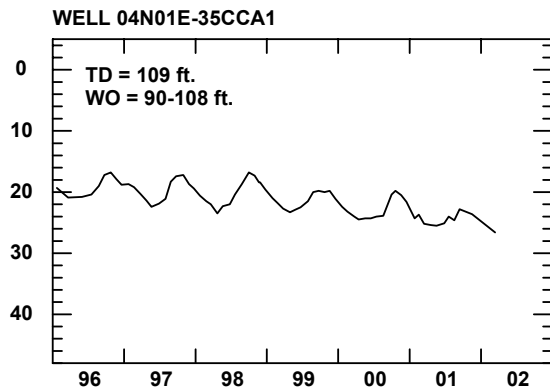
NORTHEAST OF EAGLE (no well log available). Geothermal well showed rises in the shut-in pressuring during the period 1994-1999. From 2000 to present, slight declines have been shown.



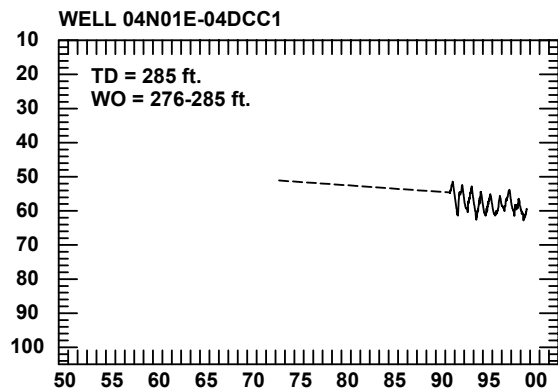
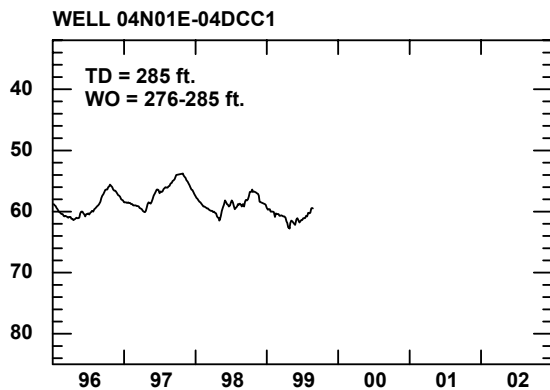
NORTHWEST OF NOTUS, NORTH OF GREENLEAF. Decline from 1985 to 1993–1994, which coincides with below normal precipitation. Increases from 1995 to present coincide with increased precipitation. Hydrograph curves prior to 1985 generally correspond with the precipitation curve.



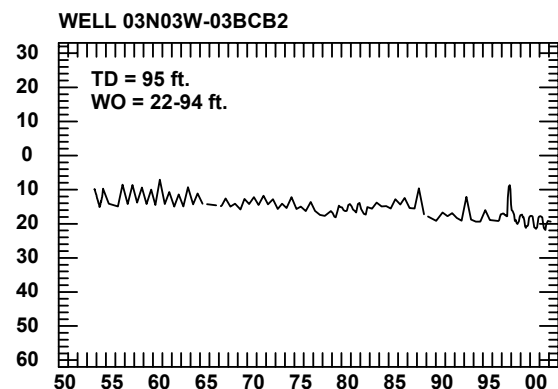
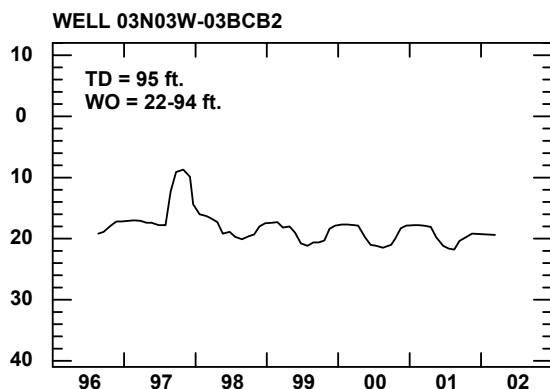
SOUTH OF STAR. Flowing well, apparent decrease in pressure from early 1970s to 1990. Water levels from 1990 to 1998 appear stable to increasing. Well is 5 miles down gradient from Meridian, 2 miles north of I-84 corridor. Land use change map does not indicate major decrease in irrigated lands, but some changes have occurred locally. Water levels may have come to equilibrium. Five-foot decline over past 3 years beginning in 1999 may indicate a renewed period of decline.



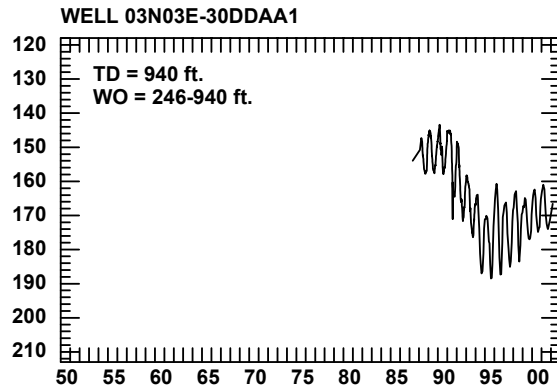
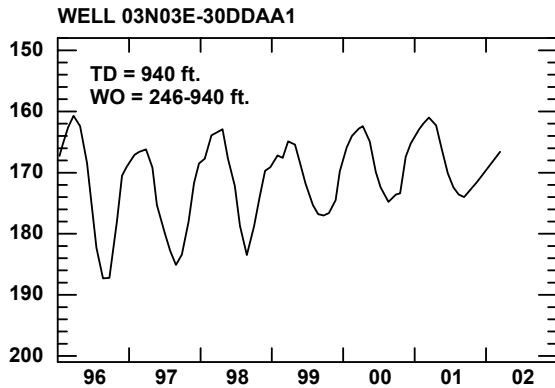
WEST OF GARDEN CITY, 3 miles. Vicinity of Ustick & Five Mile Road. Suburban development since late 1980s or early 1990s. Formerly irrigated farmlands. Levelled off 1996–1998. Has been declining since 1998.



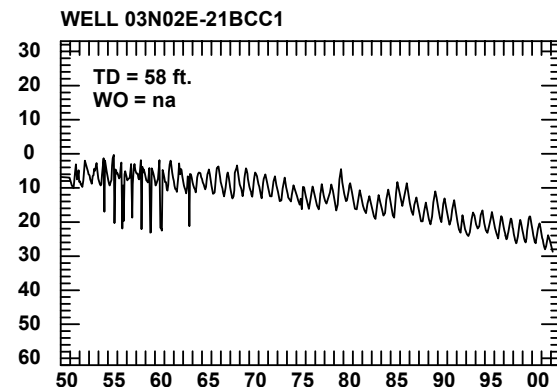
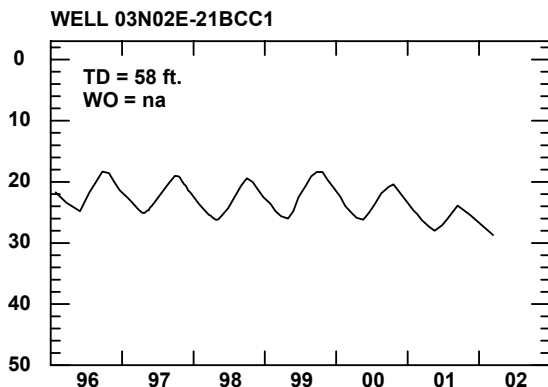
NORTH OF EAGLE. Suburban development since late 1980s to present. Formerly irrigated farmland. Slight declines continue.



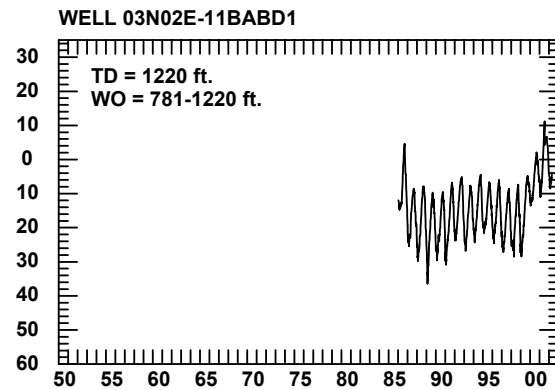
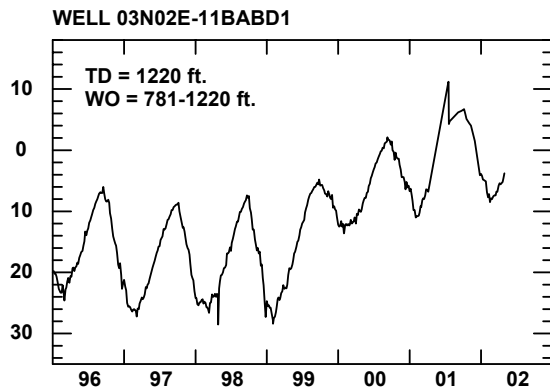
Field visit shows current high density housing construction surrounded by flood-irrigated lands and older residential tracts. Long-term decline probably resulting from gradual increase in housing throughout this area.



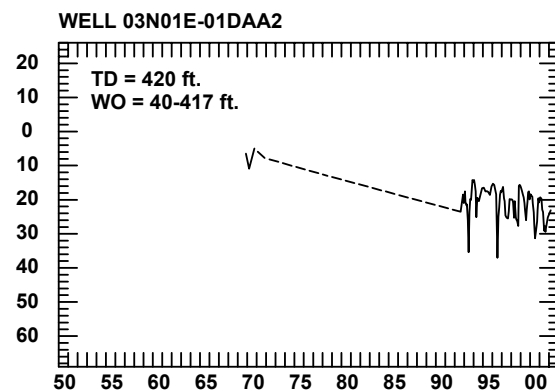
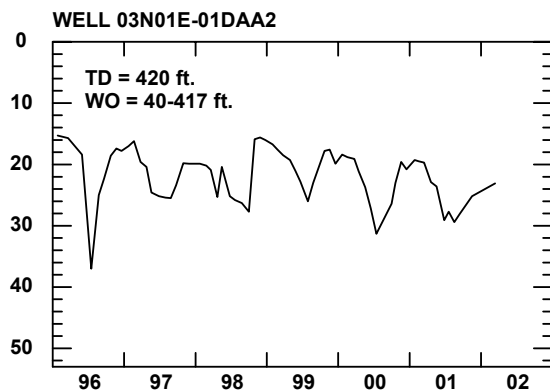
EAST BOISE TEST WELL. Water levels are indicative of the declining water levels and subsequent increasing trends since 1999 in the southeast Boise area surrounding the Micron facility.



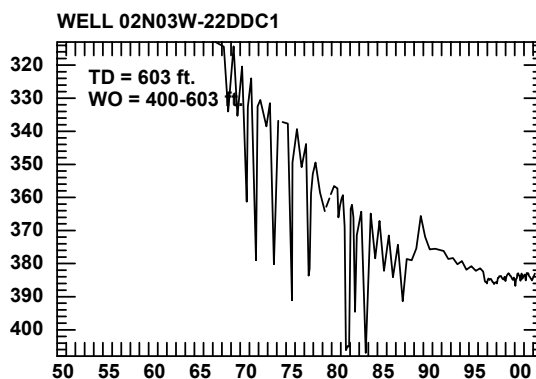
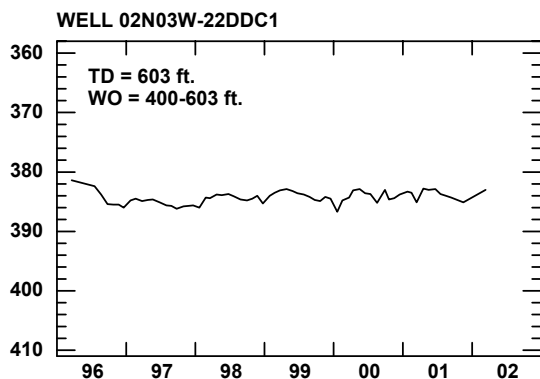
BOISE, NEAR HILLCREST GOLF COURSE. The golf course was built around 1962; the neighborhood looks to be 1945+ era. Water level increased until 1955, when a steady decline of 1-2' per year began and has continued. Also, New York Canal is within 1 mile south of the site but has been lined since approx 1907 (D. Dyke, pers. comm.). Decline may be result of nearby (?) residential well use.



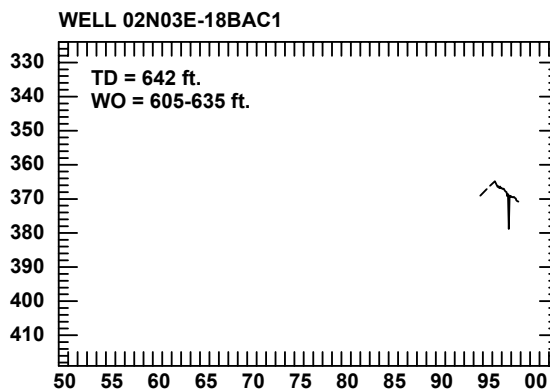
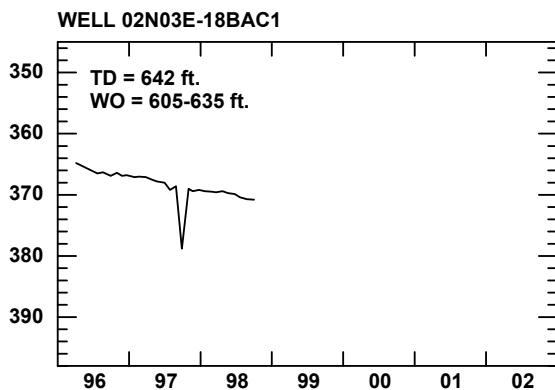
BLM GEOTHERMAL WELL. Declines in pressures correspond to other wells in the geothermal aquifer. Declines appear to have stabilized through the aquifer. Increasing water levels since 1999 may be influenced by the injection of spent geothermal water from the Boise City geothermal system. Injection began in 1999.



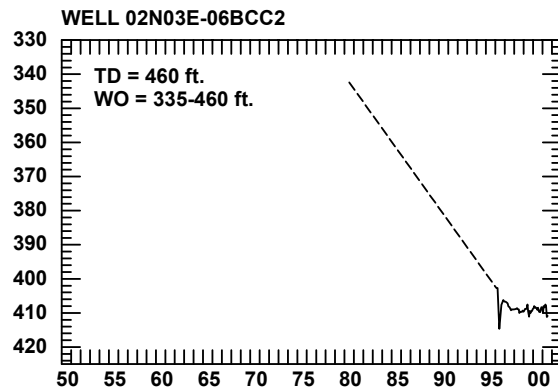
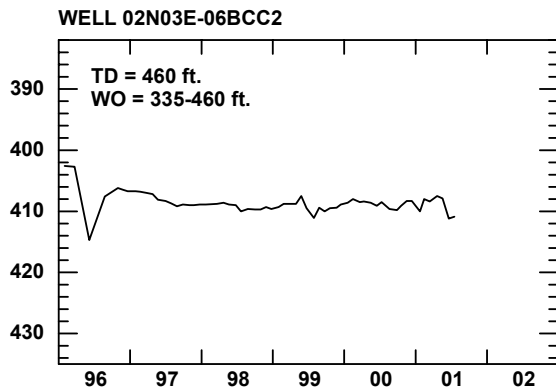
EAST OF MERIDIAN, NORTH OF FAIRVIEW. Reduction in flood irrigation combined with increased urbanization is most likely cause of water level decline.



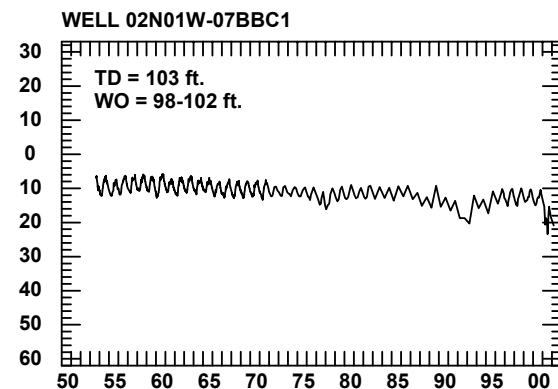
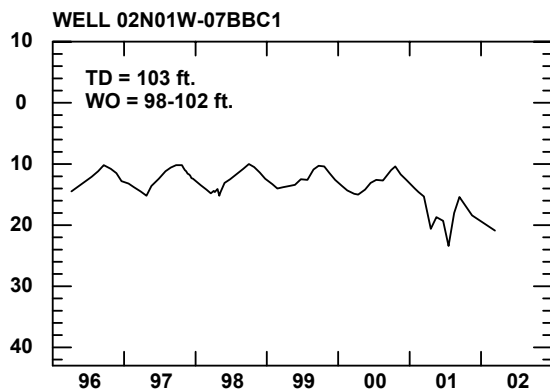
SOUTH OF LAKE LOWELL. Sprinkle irrigated farmland; mostly with ground water (per land use mapping). Fallow land to north and west, no flood irrigation available. Decline from mid-1960s to mid-1990s probably resulting from steady ground water over use coupled with low recharge rates. Water levels stabilized since mid-1990s.



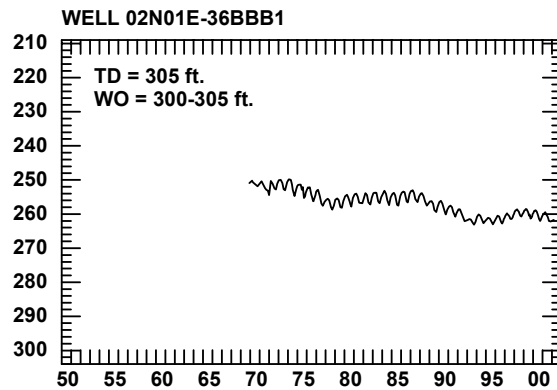
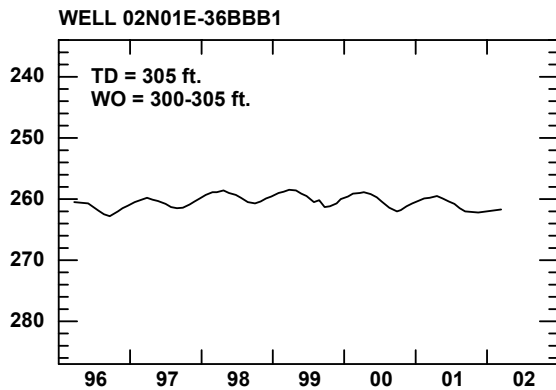
SOUTH OF BOISE, SOUTH OF FIVE MILE CREEK. Knox well, located on hill near Micron. Limited data, and no new data since 1998. Declines possibly resulting from increased water use in Micron vicinity or use at the well site itself.



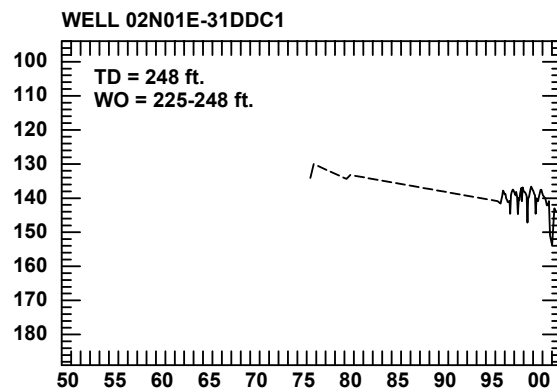
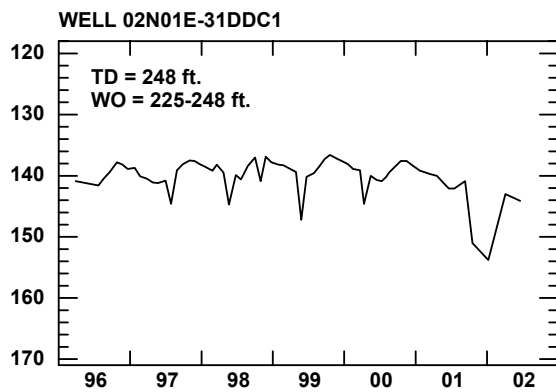
GOWEN ROAD & FEDERAL WAY, KOA well. Located near SE Boise GWMA. Major declines have been observed throughout this area. This decline probably resulted from major increase in water use in the Micron vicinity. Water levels have stabilized since 1996.



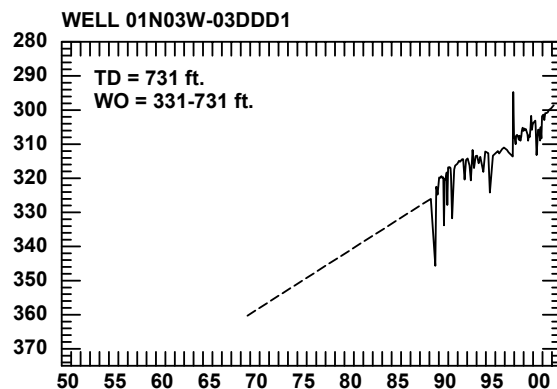
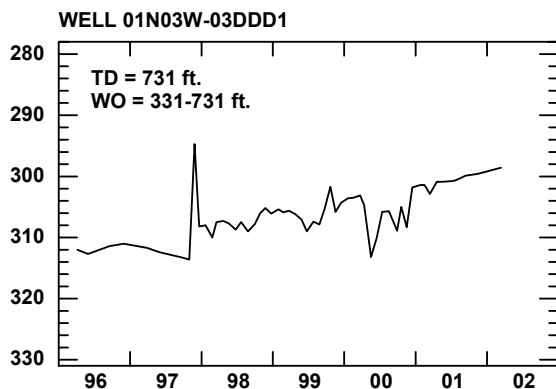
NORTHWEST OF KUNA, WEST OF ROBINSON ROAD. This section is mostly flood-irrigated farmland with houses along the perimeter. Age of houses range from pre-1940 to present. Gradual decline of water level probably result of gradual increase in residential construction. Sharp declines in 1990 and 2001, probably drought related.



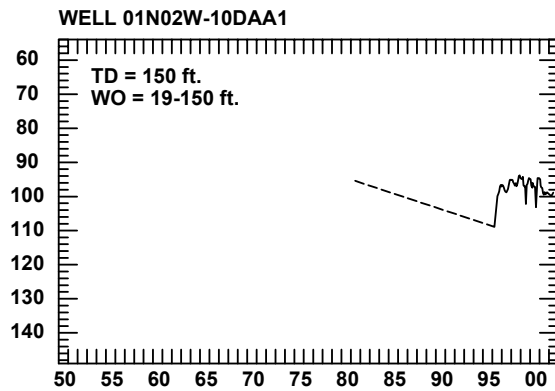
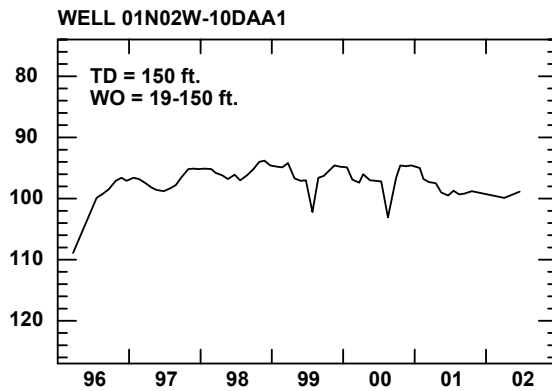
EAST OF KUNA 6 MILES, SOUTH OF NEW YORK CANAL. General long-term decline, punctuated by period of recovery that coincide with years of above normal precipitation.



SOUTHEAST OF KUNA. Fairly stable from 1996 through 2000. Data are too limited to determine cause of declines prior to 1996.



NEAR SNAKE RIVER, WEST OF MORA CANAL. Unclear reason for sharp increase in water level. Several injection wells (total depths approximately 100-150') are used for disposal of field runoff nearby.



NORTH OF MELBA, NEXT TO MORA CANAL. Short record of data. Relative to 1980 USGS measurement, current water levels have not changed substantially. Continued increases may be due to above average precipitation during mid- to late-1990s. Recent levels appear to reflect drier-than-normal conditions.

Costs associated with this publication are available from the Idaho Department of Water Resources in accordance with Section 60-202, *Idaho Code*. IDWR-21000-20-03/2004.