WATER RESOURCES OF THE UPPER BIG WOOD RIVER BASIN, IDAHO

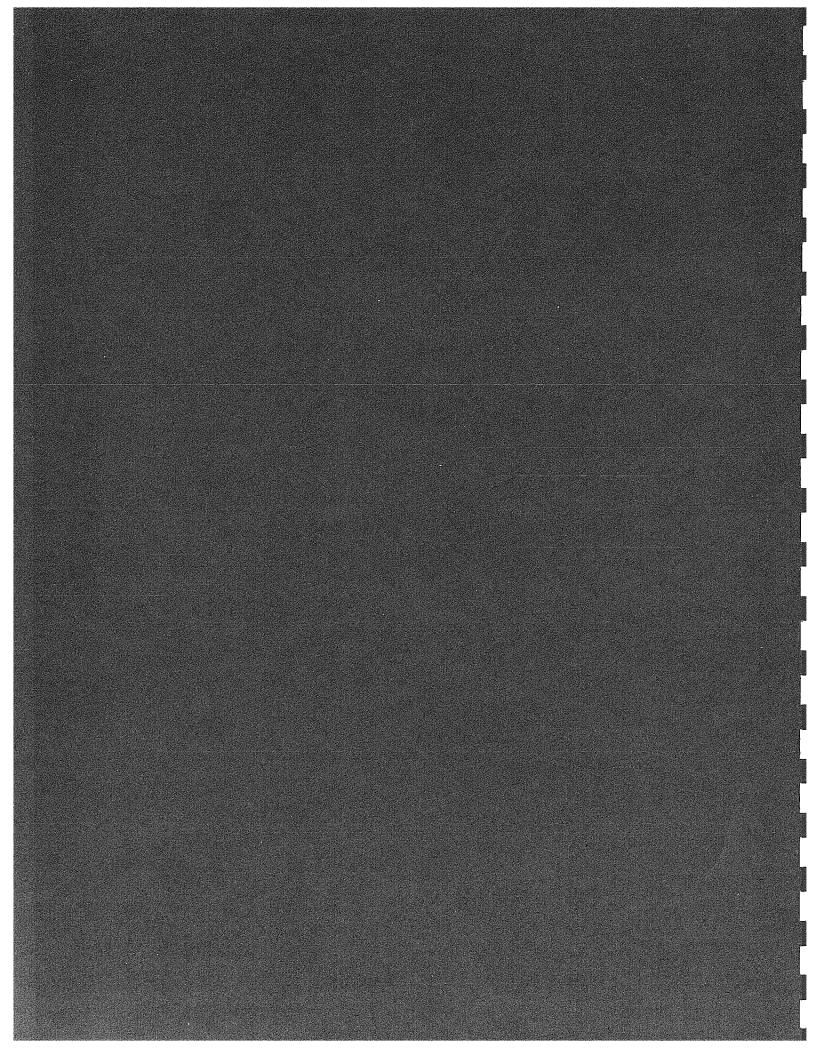
U.S. GEOLOGICAL SURVEY

Water-Resources Investigations Report 89-4018

Prepared in cooperation with

SUN VALLEY WATER AND SEWER DISTRICT





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By S.A. Frenzel

U.S. GEOLOGICAL SURVEY

Water-Resources Investigations Report 89-4018

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Boise, Idaho



1989

DEPARTMENT OF THE INTERIOR MANUEL LUJAN, JR., Secretary U.S. GEOLOGICAL SURVEY Dallas L. Peck, Director

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1

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CONVERSION FACTORS

For readers who prefer to use metric (International System) units, conversion factors for inch-pound units used in this report are listed below. Constituent concentrations are given in mg/L (milligrams per liter), or μ g/L (micrograms per liter), which are equal to parts per million or parts per billion, respectively. Specific conductance is expressed as μ S/cm (microsiemens per centimeter at 25 degrees Celsius.)

| Multiply inch-pound unit | <u>By</u> | <u>To obtain SI unit</u> |
|--|-----------|-------------------------------|
| acre | 4,047 | square meter |
| acre-foot (acre-ft) | 1,233 | cubic meter |
| cubic foot per second (ft ³ /s) | 0.028317 | cubic meter per second |
| foot (ft) | 0.3048 | meter |
| foot squared per day (ft ² /d) | 0.09290 | meter squared per day |
| gallon per minute (gal/min) | 0.06308 | liter per second |
| <pre>gallon per minute per foot [(gal/min)/ft]</pre> | 0.2070 | liter per second per meter |
| inch (in.) | 25.4 | millimeter |
| mile (mi) | 1.609 | kilometer |
| square foot (ft ²) | 0.09294 | square meter |
| square mile (mi ²) | 2.590 | square kilometer |

Temperature in °C (degrees Celsius) can be converted to °F (degrees Fahrenheit) as follows:

$$^{\circ}F = (^{\circ}C)(1.8) + 32$$

Water temperatures are reported to the nearest 0.5 °C.

<u>Sea level</u>: In this report, "sea level" refers to the National Geodetic Vertical Datum of 1929 (NGVD of 1929), which was derived from a general adjustment of the first-order level nets of both the United States and Canada, and formerly was called "Sea Level Datum of 1929."

WATER RESOURCES OF THE UPPER BIG WOOD RIVER BASIN, IDAHO

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ABSTRACT

The upper Big Wood River basin in south-central Idaho has undergone increases in urban development and sewage disposal that may impose stresses on the quantity and quality of the water resources.

Mean annual water yields for a base period from 1940 to 1979 were estimated using the water-budget method. Estimated yields for the upper Big Wood River basin above Glendale Road and for its major tributaries, Trail Creek, Warm Springs Creek, and East Fork Big Wood River, were 410,000, 50,000, 60,000, and 50,000 acrefeet, respectively. Mean annual water yield for the upper Big Wood River basin also was estimated using an empirical method. Results from the empirical method were similar to results from the water-budget method; however, the water-budget method is considered to be more accurate because of the large surface-water component, which is measured rather than estimated. Yields also were estimated for 1986 and 1987 water years when data were collected for comparison with long-term average values. During 1986, yields estimated for upper Big Wood River basin, Trail Creek, Warm Springs Creek, and East Fork Big Wood River were 580,000, 61,000, 83,000, and 60,000 acre-feet, respectively. During 1987, yields estimated for the respective basins were 230,000, 26,000, 32,000, and 28,000 acre-feet. Availability of surface and ground water varies seasonally; the greatest quantity is available during spring snowmelt, and the least is available during mid- to late winter.

Nutrient concentrations in sampled ground and surface water were near or below detection levels throughout the basin, which indicates that water quality has not been impaired by increased urban development and sewage disposal. Fluoride concentrations were elevated in Warm Springs Creek, probaby due to inflow of thermal water.

INTRODUCTION

Purpose and Scope

This report describes results of a study to evaluate water resources in the upper Big Wood River basin. Emphasis of the study was on determining water yield of the basin and some of its major tributaries. The scope of this study included:

- Collection of historical geologic, hydrologic, water-use, and water-quality data to determine average conditions of the water resources.
- (2) Measurement of ground-water levels and aquifer thickness near the basin outlet to determine volume of groundwater underflow from the basin.
- (3) Evaluation of ground-water and surface-water relations.
- (4) Collection of ground- and surface-water quality data to determine whether urban development and sewage disposal have affected water quality.
- (5) Estimation of water yield from the upper Big Wood River basin, Trail Creek, Warm Springs Creek, and East Fork Big Wood River.

Data were collected from February 1986 through November 1987.

Physical Setting

The upper Big Wood River basin is in Blaine County, north of Twin Falls, in south-central Idaho (fig. 1). For this study, only the area upstream (generally north) from Glendale Road (fig. 2) was considered. Generally, the upper Big Wood River valley is narrow and has a maximum width of about 2 mi at the southern boundary of the study area. Steep mountains surround the valley to the north, east, and west. Altitudes range from 5,060 ft above sea level at Glendale Road to 11,913 ft in the surrounding mountains, and the basin area above Glendale Road is 752 mi². Sun Valley, Ketchum, Hailey, and Bellevue are communities in the basin.

Climate of the upper Big Wood River basin is one of cold, wet winters and warm, dry summers. At Sun Valley, mean minimum temperatures of about -1 °F (-18 °C) are recorded in January, and mean maximum temperatures of about 82 °F (28 °C) are recorded in July. Mean annual precipitation at Sun Valley (1937-73) is 17.6 in. and, at Hailey (1917-82), is 15.0 in. Half the annual precipitation falls from November through February.

Between 1970 and 1980, population in Blaine County increased from 5,749 to 9,841; population in the study area is about 90 percent of the total in Blaine County (Luttrell and Brockway, 1982, p. 8, 9). The 1990 population for the study area was projected to be about 15,000, and maximum population was estimated to be 22,000 (Luttrell and Brockway, 1982, p. 26, 27). In addition to the permanent residents, thousands of people annually visit the area for winter and summer recreation.

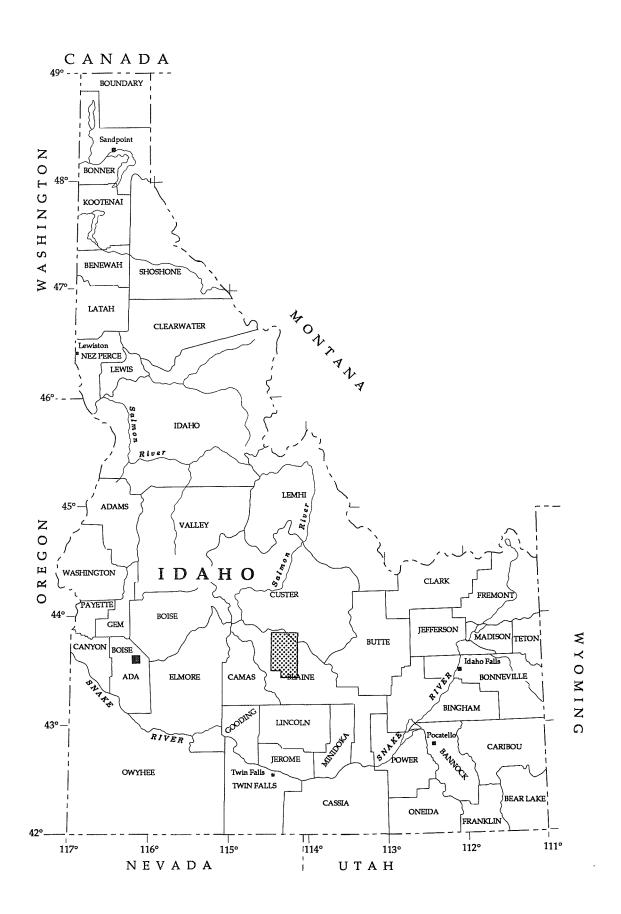


Figure 1.--Location of study area.

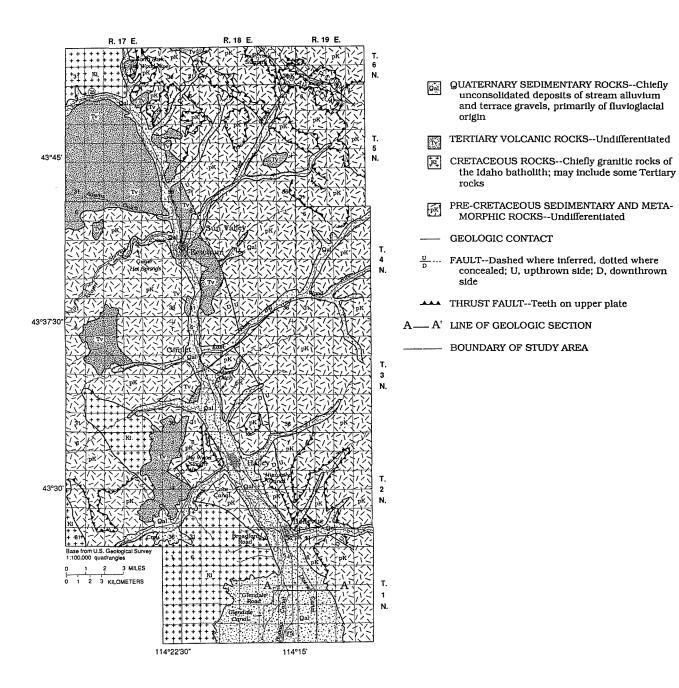


Figure 2.--Generalized geology.

Geologic Setting

Geology of the region was described in detail by Umpleby and others (1930) and is shown in figure 2 as modified from Rember and Bennett (1979). The mountains in the area are composed of Pre-Cretaceous sedimentary and metamorphic rocks, Cretaceous granitic rocks, and Tertiary volcanic rocks. Thickness of the sedimentary and igneous rocks totals about 32,000 ft (Umpleby and others, 1930, p. IX). Extensive faulting and folding have resulted in complex structure (Luttrell and Brockway, 1984, p. 10). Valleys are filled with Quaternary glacial and alluvial deposits that constitute the aquifer in the study area (Luttrell and Brockway, 1984, p. 13). Terraces in the study area are composed of alluvial deposits. Most of the valley fill is stream and delta clay, sand, and gravel deposited before the Wisconsin glaciation and is overlain by a thin sheet of fluvioglacial sediments (Smith, 1959, p. 16).

Previous Investigations

Work by Smith (1959) dealt with areas that partly overlap the upper Big Wood River basin. The primary objective of Smith's study was to determine the quantity of water available for additional irrigation in the middle Big Wood River area. Geology and mineral resources of the Hailey-Bellevue mining district and upper Big Wood River basin were studied by Anderson and others (1950). Jones (1952) examined discharge records in the Big Wood River basin with emphasis on identification of all diversions above gaging stations. Smith (1960) evaluated discharge records in the Big Wood River basin to determine whether the gaged discharges adequately represented basin yield.

Castelin and Chapman (1972) studied the water resources of the Big Wood River-Silver Creek area as far north as Hailey. Objectives of their study included: (1) Identification of relations between water-table, artesian, and regional (Snake River Plain) aquifers, (2) development of a water budget for the area, and (3) determination of reaches of gains and losses in Silver Creek. Moreland (1977) included the area around Bellevue in his study of ground-water and surface-water relations in the Silver Creek area.

Castelin and Winner (1975) studied the upper Big Wood River basin to: (1) Determine physical characteristics of local aquifers, (2) determine relations between ground and surface water, (3) describe the level of urbanization in terms of water use, (4) determine quality of ground and surface water, and (5) establish a hydrologic data base. Luttrell and Brockway (1982, 1984) studied impacts of onsite sewage-disposal systems on water quality in the upper Big Wood River basin to: (1) Evaluate waterquality problem areas on the basis of density of sewage-disposal sites, (2) establish a ground-water quality monitoring network and data base, (3) evaluate the ground-water flow system, and (4) determine river/aquifer hydraulic relations.

Well-Numbering System

The well-numbering system (fig. 3) used by the U.S. Geological Survey in Idaho indicates the location of wells within the official rectangular subdivision of public lands, with reference to the Boise base line and Meridian. The first two segments of the number designate the township (north or south) and range (east or west). The third segment gives the section number; three letters, which indicate the $^{1}/_{4}$ section (160-acre tract), $^{1}/_{4-1}$ section (40-acre tract), and $^{1}/_{4-1}/_{4-1}/_{4}$ section (10-acre tract); and serial number of the well within the tract.

Quarter sections are designated by the letters A, B, C, and D in counterclockwise order from the northeast quarter of each section. Within the quarter sections, 40-acre and 10-acre tracts are lettered in the same manner. For example, well 2N-18E-9BDC1is in the $SW^{1/4}SE^{1/4}NW^{1/4}$ sec. 9, T. 2 N., R. 18 E., and is the first well inventoried in that tract.

WATER RESOURCES

Average quantity of water in the upper Big Wood River basin was estimated by using data from 1940 to 1979 water years (October 1 to September 30). This base period was selected because the greatest quantity of pertinent data were available during those years. The type of data, location, and period of record for which data are available include:

- (1) Discharge, Big Wood River at Hailey, 1915-88.
- (2) Discharge, Warm Springs Creek, 1940-58.
- (3) Discharge, Big Wood River near Ketchum, 1948-71.
- (4) Precipitation, Hailey, 1917-82.
- (5) Precipitation, Sun Valley/Ketchum, 1937-88.
- (6) Snowpack, several locations, minimum record, 1961-88.

Precipitation

Precipitation data were collected at Hailey from 1917 to 1982 and at Sun Valley from 1937 to 1973, when the site was moved to its present (1988) location in Ketchum. Mean annual precipitation for the 1940-79 base period was 16.0 in. at Hailey and 17.5 in. at Sun Valley/Ketchum. During 20 of these years, precipitation at Hailey was greater than the mean for the period of record.

Hailey and Sun Valley/Ketchum precipitation sites are at relatively low altitudes in the basin and, because precipitation

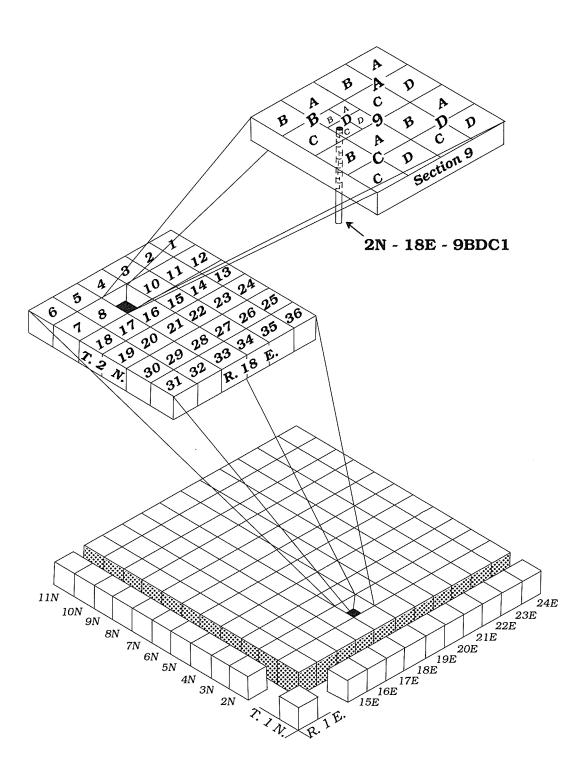


Figure 3.--Well-numbering system.

varies with altitude (Hanson, 1982, p. 875), it was necessary to estimate precipitation for higher altitudes. Mean annual precipitation at eight snow courses in the area as determined from a regional precipitation map was about $1^{1/2}$ times the mean April 1 water content measured at the snow courses. Four snow courses recently were equipped to measure annual precipitation, and these sites also show annual precipitation to be about $1^{1/2}$ times the April 1 water content. A precipitation-altitude relation (fig. 4) was determined by linear regression using estimated mean annual precipitation at the snow courses (eight sites) and measured annual precipitation (two sites).

The regression equation was used to determine mean annual precipitation for the average altitude of the upper Big Wood River basin. Annual precipitation for individual years from 1940 to 1979 was determined by adjusting mean annual precipitation by the same quantity that the annual precipitation at Hailey differed from the mean at Hailey. For example, the average altitude for Warm Springs Creek is 7,660 ft and the mean annual precipitation is 28 in. If, for a given year, precipitation at Hailey were 19 in. (3 in. greater than the mean), then precipitation for Warm Springs Creek is estimated to be 31 in.

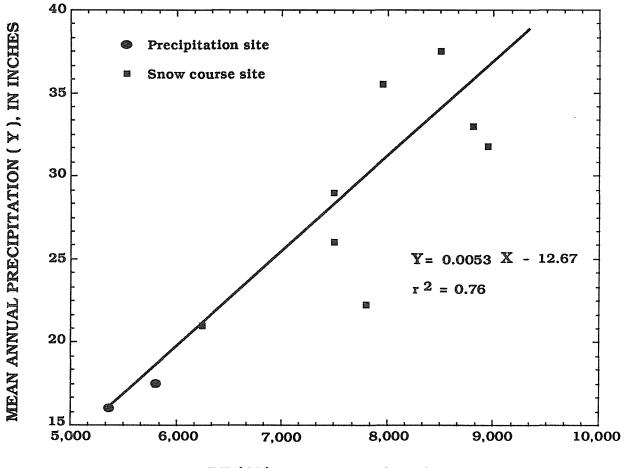
Because precipitation data no longer are collected at Hailey and because data from Ketchum do not correlate well with data from Hailey ($r^2 = 0.42$, using annual data from 1974 to 1982), annual precipitation for the upper Big Wood River basin for the 1986 and 1987 water years was estimated using data from the eight snow courses and the precipitation-altitude relation shown in figure 4.

Surface Water

A continuous record of discharge for the Big Wood River at Hailey has been collected since June 1915. Recording gaging stations also were located on the Big Wood River near Ketchum (0.25 mi above North Fork Big Wood River) from 1948 to 1971 and on Warm Springs Creek at Guyer Hot Springs from 1940 to 1958. Other surface-water data have been collected periodically.

Discharge at Hailey (combined flow of Big Wood River and Big Wood Slough) ranged from 15 to 6,150 ft³/s and averaged 460 ft³/s from 1916 to 1987 (U.S. Geological Survey, 1956, p. 234; Harenberg and others, 1988, p. 243). Mean discharge for 7 and 30 consecutive days were as low as 88 and 98 ft³/s, respectively, at intervals averaging 10 years (fig. 5).

Discharge of the Big Wood River near Ketchum ranged from 8.5 to 1,690 ft³/s and averaged 167 ft³/s for the period of record (U.S. Geological Survey, 1972, p. 163). Mean discharge for 7 and 30 consecutive days were as low as 35 and 37 ft³/s, respectively, at intervals averaging 10 years (fig. 5).



ALTITUDE (X), IN FEET ABOVE SEA LEVEL

Figure 4.--Relation of mean annual precipitation to altitude.

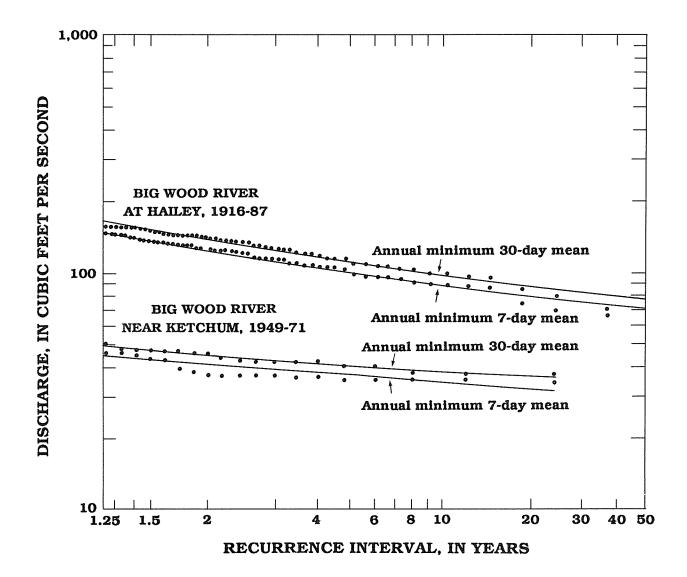


Figure 5.--Frequency curves of annual minimum 7-day and 30-day mean discharge for the Big Wood River at Hailey and near Ketchum.

Discharge of Warm Springs Creek at Guyer Hot Springs ranged from 6.0 to 961 ft³/s and averaged 87 ft³/s for the period of record (U.S. Geological Survey, 1963, p. 115). Typically, discharge in the study area was highest during spring snowmelt and lowest during the winter. Mean monthly discharge of the Big Wood River at Hailey from 1916 to 1987 was highest in June (1,500 ft³/s) and was lowest in February (154 ft³/s). More than half the annual discharge was during May and June.

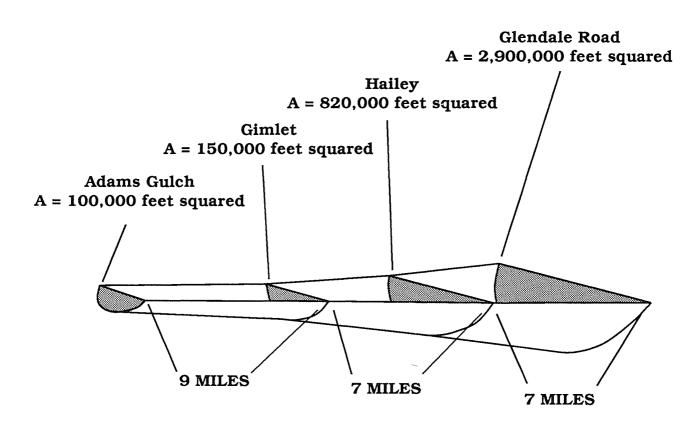
Major tributaries to the Big Wood River include North Fork Big Wood River, Trail Creek, Warm Springs Creek, and East Fork Big Wood River (fig. 2). Discharge of Trail Creek, Warm Springs Creek, and East Fork Big Wood River was measured monthly from February 1986 through November 1987.

Ground Water

Water exists in the alluvial deposits under water-table conditions. Significance and water-bearing capacity of pre-Cretaceous sedimentary and metamorphic rocks were not determined; however, water yield from these rocks is probably low. Recharge to the aquifer is from precipitation and from percolation of surface water from streams, canals, and irrigated fields. The rate of movement and volume of ground water discharged from the basin depends on the hydraulic gradient, hydraulic conductivity, and cross-sectional area of the aquifer.

Storage of ground water in any given location in the study area is largely a function of the areal extent and thickness of the aquifer at that location. The quantity of ground water in storage depends on the volume of aquifer material and specific Specific yield (Sy) is the ratio of (1) the volume of yield. water which saturated rock will yield by gravity to (2) the volume of rock (Lohman and others, 1972, p. 12). The volume of aquifer material was estimated by subdividing the aquifer and representing each part as a half-conical section (fig. 6). Cross-sectional areas of the aquifer at Adams Gulch, Gimlet, and Hailey were estimated on the basis of the basin width and aquifer thickness determined from well-drillers' logs and from data reported by Luttrell and Brockway (1984, p. 14-15). Cross-sectional area of the aquifer at Glendale Road was determined from seismic refraction work during this study. Specific yield was estimated as 0.2, which was about the average for unconsolidated alluvium reported by Johnson (1967, p. D68). The quantity of ground water in storage from Adams Gulch to Glendale Road was estimated to be about 400,000 acre-ft. Storage of ground water also varies seasonally; the greatest quantity is available during spring snowmelt, and the least quantity is available during mid- to late winter.

Withdrawals vary seasonally; the greatest quantities are withdrawn during the summer and winter recreation period:



A = Cross-sectional area perpendicular to direction of ground-water flow

VERTICAL EXAGGERATION X 26

Figure 6.--Conceptual block diagram showing cross-sectional areas of the alluvial aquifer from Adams Gulch to Glendale Road.

Municipal wells normally withdraw 3,500 to 4,500 acre-ft of water annually to supply the Sun Valley/Ketchum area from well fields near Trail Creek and the Big Wood River (J.T. Brown, Sun Valley Water and Sewer District, written commun., 1987; S.A. Hansen, City of Ketchum, written commun., 1988).

Water levels were measured in 84 wells in April 1986 (table 1) to define the water table prior to diversion of surface water into irrigation canals. Water-level data were used to construct a water-table contour map (fig. 7) to show direction of ground-water movement and to determine hydraulic gradients. Direction of ground-water flow is perpendicular to water-table contours and is generally southward, parallel to the long axis of the upper Big Wood River basin. Hydraulic gradients were used to compute ground-water discharge.

Aquifer Characteristics and Estimates of Ground-Water Discharge

Hydraulic conductivity (K) is a measure of the ability of aquifer material to conduct water, is dependent on the nature of the pore space, and is expressed in feet per day (Lohman and others, 1972, p. 4). Transmissivity (T) is a measure of the rate at which water moves through a unit width of the aquifer under a unit hydraulic gradient and is expressed in feet squared per day (Lohman and others, 1972, p. 13). Transmissivity is equal to K multiplied by the saturated thickness (b) of the aquifer. Specific capacity (C) of a well is the rate of discharge, in gallons per minute, divided by the water-level drawdown in the well, in feet.

Specific capacity was determined from driller's logs for six wells that met the arbitrary criteria of a minimum pumping rate of 500 gal/min and a minimum pumping time of 2 hours. Specific capacity was used to estimate T by two empirical methods. The first method (Theis, 1963, p. 335) used the equation:

$$T' = 0.134$$
 (C) (F) (1,300 - 264log 5Sy + 264log t) (1)

where

| Т' | <pre>= estimate of transmissivity, in feet squared per day;</pre> |
|-------|--|
| 0.134 | <pre>= constant to convert gallons per foot per day to feet squared per day;</pre> |
| С | = specific capacity of pumped well, in gallons per minute per foot of drawdown; |
| F | <pre>= factor to adjust for well radius and degree of well development (1.0 for 6-in. radius, 0.9 for 8- in. radius, and 0.8 for 10-in. radius wells were used);</pre> |
| Sy | = specific yield0.2 (Johnson, 1967) was used as an average value for coarse alluvial material; and |
| t | = pumping time, in days, |

| Well number | Well location (fig. 7) | Altitude of land surface (feet above sea level) | Day measured | Depth of water below land surface (feet) |
|-----------------------|------------------------------|--|-----------------|---|
| 1 | 5N-17E-25BCA1 | 6,038 | 9 | 16.68 |
| 1 2 3 4 5 | 36DBD1 | 5,970 | 9 9 9 | 1.84 |
| 3 | 4N-17E- 1DCD1 | 5,872 | 9 | 2.85 |
| 4 | 11CDA1 | 5,845 | 9 | 24.88 |
| 5 | 12ADB1 | 5,853 | 10 | 10.00 |
| 6 | 12CDD1 | 5,848 | 10 | 51.68 |
| 7 8 9 | 13AAB1 | 5,813 | 10 | 12.83 |
| 8 | 13ABA1 | 5,815 | 10 | 10.83 |
| | 13ACA1 | 5,791 | 10 | 12.07 |
| 10 | 4N-18E-18CCB1 | 5,810 | 10 | 45.23 |
| 11 | 19DBB1 | 5,751 | 10 | 25.02 |
| 12 | 19DBB2 | 5,738 | 10 | 16.68 |
| 13 | 19DBD1 | 5,738 | 10 | 15.72 |
| 14 | 19DCD1 | 5,718 | 9 | 8.56 |
| 15 | 19DCD2 | 5,718 | 9 | 11.38 |
| 16 | 30ADB3 | 5,680 | 10 | 7.68 |
| 17 | 31DBD1 | 5,640 | 10 | 12.45 |
| 18 | 3N-18E- 6ABA1 | 5,630 | 11 | 6.36 |
| 19 | 6ADA1 | 5,605 | 12 | 12.62 |
| 20 | 6DDA1 | 5,590 | 12 | 20.55 |
| 21 | 7DAB1 | 5,570 | 7 | 7.72 |
| 22 | 7DBA1 | 5,600 | 8 | 45.48 |
| 23 | 7DDD1 | 5,556 | 7 | 19.38 |
| 24 | 8BBC1 | 5,582 | 7 | 20.33 |
| 25 | 8CBC3 | 5,573 | 7 | 16.17 |
| 26 | 17BCC1 | 5,520 | 8 | 10.81 |
| 27 | 17CCD1 | 5,545 | 8 | 37.29 |
| 28 | 18AAB1 | 5,558 | 12 | 18.65 |
| 29 | 18DAA1 | 5,515 | 12 | 7.79 |
| 30 | 20BDA1 | 5,520 | 8 | 38.85 |
| 31 | 20DCC1 | 5,475 | 8 | 27.58 |
| 32 | 29BDA1 | 5,438 | 8 8 | 10.38 |
| 33 | 29DCC1 | 5,415 | 12 | 4.15 |
| 34 | 32ABA1 | 5,416 | 8 | 10.08 |
| 35 | 32DBA1 | 5,388 | 12 | 6.58 |
| | | | | |

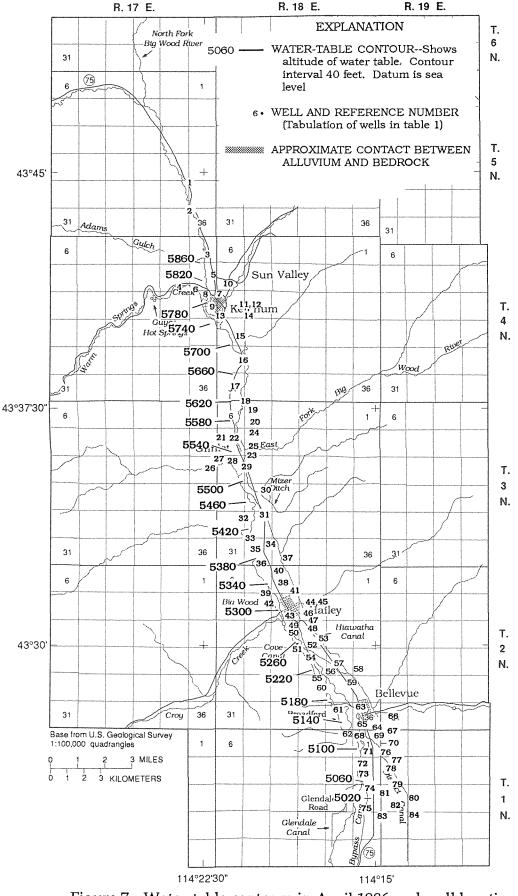
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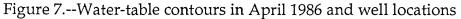
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | Well number | Well location | Altitude of land surface (feet above sea level) | Day measured | Depth of water below land surface (feet) |
|---|----------------|------------------|--|-----------------|---|
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 36 | 3N-18E-32DDD1 | 5,375 | 8 | 9.39 |
| 39 $4CCB1$ $5,340$ 8 $9,79$ 40 $5AAA1$ $5,370$ 11 16.54 41 $9ABA1$ $5,370$ 8 48.87 42 $9BDC1$ $5,324$ 7 37.25 44 $10BAC1$ $5,358$ 9 54.06 45 $10BAC2$ $5,355$ 11 51.88 46 $10DCB1$ $5,334$ 7 47.41 47 $15BAB1$ $5,322$ 9 34.09 48 $15BAC1$ $5,303$ 12 25.52 50 $15CB1$ $5,303$ 12 25.52 50 $15CB1$ $5,270$ 9 17.13 52 $15CB1$ $5,275$ 9 20.30 53 $15DBC1$ $5,275$ 9 20.30 53 $15DBC1$ $5,223$ 9 5.93 56 $23DCC1$ $5,234$ 9 34.14 57 $23DBE1$ $5,222$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $26CBB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCE1$ $5,195$ 11 62.14 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,250$ 11 43.03 69 $1N-18E-1ABC1$ $5,153$ <td></td> <td></td> <td></td> <td></td> <td></td> | | | | | |
| 405AAA15,3701116.54419ABA15,370848.87429BDC15,324716.74439DDA15,324737.254410BAC15,358954.064510BAC25,3551151.884610DCB15,334747.414715BAB15,322934.094815BAC15,315934.204915BCB15,3031225.525015CBA15,275920.305115CCA15,275920.305215CDB15,275920.305315DBC15,287931.585422BDB15,25598.685522DDB15,22395.935623DCC15,232740.255823DC15,232740.255926ABA15,219736.256026CBB15,19794.506135BAB15,17894.996235DCD15,158104.436436DAC15,1951162.146536DCA15,173942.49662N-19E-31CAB15,235990.806731CCD15,2001175.29681N-18E-1ABC15,1531036.54691ACA15,25011 <t< td=""><td></td><td></td><td></td><td></td><td></td></t<> | | | | | |
| 419ABA1 $5,370$ 8 48.87 429BDC1 $5,324$ 7 16.74 439DDA1 $5,324$ 7 37.25 4410BAC1 $5,388$ 9 54.06 4510BAC2 $5,355$ 11 51.88 4610DCB1 $5,334$ 7 47.41 4715BAB1 $5,322$ 9 34.09 4815BAC1 $5,315$ 9 34.20 4915BCB1 $5,303$ 12 25.52 5015CBA1 $5,288$ 11 17.79 5115CCA1 $5,270$ 9 20.30 5315DBC1 $5,287$ 9 31.58 5422BDB1 $5,255$ 9 8.68 5522DDB1 $5,232$ 7 40.25 5823DC1 $5,232$ 7 45.55 5926ABA1 $5,197$ 9 4.50 6135BAB1 $5,178$ 9 4.99 6235DCD1 $5,158$ 10 4.43 6436DAC1 $5,197$ 9 4.50 6135BAB1 $5,178$ 9 4.99 6236DCA1 $5,173$ 9 42.49 662N-19E-31CAB1 $5,235$ 9 90.80 67 $31CCD1$ $5,255$ 9 90.80 662N-19E-31CAB1 $5,255$ 9 90.80 67 $31CCD1$ $5,255$ 11 62.14 662N-19E-31CAB1 $5,255$ 10 43.03 67 <td></td> <td></td> <td></td> <td></td> <td></td> | | | | | |
| 42 $9BDC1$ $5,324$ 7 16.74 43 $9DDA1$ $5,324$ 7 37.25 44 $10BAC1$ $5,358$ 9 54.06 45 $10BAC2$ $5,355$ 11 51.88 46 $10DCB1$ $5,334$ 7 47.41 47 $15BAB1$ $5,322$ 9 34.09 48 $15BAC1$ $5,315$ 9 34.20 49 $15BCB1$ $5,303$ 12 25.52 50 $15CBA1$ $5,288$ 11 17.79 51 $15CCA1$ $5,270$ 9 17.13 52 $15CB1$ $5,275$ 9 20.30 53 $15DEC1$ $5,287$ 9 31.58 54 $22BDB1$ $5,255$ 9 8.68 55 $22DDB1$ $5,223$ 9 5.93 56 $23DC1$ $5,234$ 9 34.14 57 $23DDB1$ $5,240$ 7 40.25 58 $23DC1$ $5,232$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $2CCBB1$ $5,187$ 9 4.99 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36DCA1$ $5,173$ 9 4.249 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E-1ABC1$ <td< td=""><td>40</td><td>5AAA1</td><td>5,370</td><td>11</td><td>16.54</td></td<> | 40 | 5AAA1 | 5,370 | 11 | 16.54 |
| 439DDA1 $5,324$ 7 37.25 4410BAC1 $5,358$ 954.064510BAC2 $5,355$ 1151.884610DCB1 $5,334$ 747.414715BAB1 $5,322$ 934.094815BAC1 $5,315$ 934.204915BCB1 $5,303$ 1225.525015CBA1 $5,288$ 1117.795115CCA1 $5,270$ 917.135215CDB1 $5,275$ 920.305315DBC1 $5,287$ 931.585422BDB1 $5,223$ 95.935623DCC1 $5,234$ 934.145723DDB1 $5,240$ 740.255823DDC1 $5,232$ 745.555926ABA1 $5,219$ 736.256026CBB1 $5,178$ 94.506135BAB1 $5,178$ 94.996235DCD1 $5,188$ 104.436436DAC1 $5,195$ 1162.146536CCA1 $5,173$ 990.806731CCD1 $5,250$ 1143.03 | | 9ABA1 | 5,370 | 8 | 48.87 |
| 4410BAC1 $5,358$ 9 54.06 4510BAC2 $5,355$ 11 51.88 4610DCB1 $5,334$ 7 47.41 4715BAB1 $5,322$ 9 34.09 4815BAC1 $5,315$ 9 34.20 4915BCB1 $5,303$ 12 25.52 5015CBA1 $5,288$ 11 17.79 5115CCA1 $5,275$ 9 20.30 5215CDB1 $5,275$ 9 20.30 5315DBC1 $5,287$ 9 31.58 5422BDB1 $5,223$ 9 5.93 5623DC1 $5,234$ 9 34.14 5723DDB1 $5,220$ 7 45.55 5926ABA1 $5,219$ 7 36.25 6026CBB1 $5,197$ 9 4.50 6135BAB1 $5,178$ 9 4.99 6235DCD1 $5,147$ 11 6.77 6336BCB1 $5,158$ 10 4.43 6436DAC1 $5,173$ 9 42.49 662N-19E-31CAB1 $5,235$ 9 90.80 67 $31CCD1$ $5,250$ 11 43.03 | | | | 7 | |
| 4510BAC2 $5,355$ 11 51.88 4610DCB1 $5,334$ 7 47.41 4715BAB1 $5,322$ 9 34.09 4815BAC1 $5,315$ 9 34.20 4915BCB1 $5,303$ 12 25.52 5015CBA1 $5,288$ 1117.795115CCA1 $5,270$ 917.135215CDB1 $5,275$ 920.305315DBC1 $5,287$ 931.585422BDB1 $5,223$ 95.935623DC1 $5,234$ 934.145723DDB1 $5,240$ 740.255823DC1 $5,232$ 745.555926ABA1 $5,219$ 736.256026CBB1 $5,197$ 94.506135BAB1 $5,178$ 94.996235DCD1 $5,147$ 116.776336BCB1 $5,195$ 1162.146536DCA1 $5,173$ 942.49662N-19E-31CAB1 $5,235$ 990.806731CCD1 $5,200$ 1175.29681N-18E-1ABC1 $5,153$ 1036.54691ACA1 $5,250$ 1143.03 | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | |
| 4715BAB15,322934.09 48 15BAC15,315934.20 49 15BCB15,3031225.52 50 15CBA15,2881117.79 51 15CCA1 $5,275$ 920.30 53 15DBC1 $5,287$ 931.58 54 22BDB1 $5,255$ 98.68 55 22DDB1 $5,223$ 95.93 56 23DCC1 $5,234$ 934.14 57 23DDB1 $5,223$ 745.55 59 26ABA1 $5,219$ 736.25 60 26CBE1 $5,197$ 94.50 61 35BAB1 $5,178$ 94.99 62 35DCD1 $5,147$ 11 6.77 63 36BCB1 $5,195$ 11 62.14 65 36DCA1 $5,173$ 942.49 66 2N-19E-31CAB1 $5,235$ 990.80 67 31CCD1 $5,200$ 1175.29 68 1N-18E-1ABC1 $5,250$ 1143.03 | 45 | 10BAC2 | 5,355 | 11 | 51.88 |
| 4815BAC1 $5,315$ 9 34.20 49 15BCB1 $5,303$ 12 25.52 50 15CBA1 $5,288$ 11 17.79 51 15CCA1 $5,270$ 9 17.13 52 15CDB1 $5,275$ 9 20.30 53 15DBC1 $5,287$ 9 31.58 54 22BDB1 $5,255$ 9 8.68 55 22DDB1 $5,223$ 9 5.93 56 23DCC1 $5,234$ 9 34.14 57 23DDB1 $5,223$ 7 45.55 59 26ABA1 $5,219$ 7 36.25 60 26CBB1 $5,197$ 9 4.50 61 35BAB1 $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E 1AEC1$ $5,153$ 10 36.54 69 $1ACA1$ $5,250$ 11 43.03 | 46 | 10DCB1 | 5,334 | 7 | 47.41 |
| 4815BAC1 $5,315$ 9 34.20 49 15BCB1 $5,303$ 12 25.52 50 15CBA1 $5,288$ 11 17.79 51 15CCA1 $5,270$ 9 17.13 52 15CDB1 $5,275$ 9 20.30 53 15DBC1 $5,287$ 9 31.58 54 22BDB1 $5,255$ 9 8.68 55 22DDB1 $5,223$ 9 5.93 56 23DCC1 $5,234$ 9 34.14 57 23DDB1 $5,223$ 7 45.55 59 26ABA1 $5,219$ 7 36.25 60 26CBB1 $5,197$ 9 4.50 61 35BAB1 $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E 1AEC1$ $5,153$ 10 36.54 69 $1ACA1$ $5,250$ 11 43.03 | 47 | 15BAB1 | 5,322 | 9 | 34.09 |
| 50 $15CBA1$ $5,288$ 11 17.79 51 $15CCA1$ $5,275$ 9 20.30 53 $15DBC1$ $5,275$ 9 31.58 54 $22BDB1$ $5,255$ 9 8.68 55 $22DDB1$ $5,223$ 9 5.93 56 $23DC1$ $5,234$ 9 34.14 57 $23DDB1$ $5,240$ 7 40.25 58 $23DDC1$ $5,232$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $26CBB1$ $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,250$ 11 75.29 68 $1N-18E-1ABC1$ $5,153$ 10 36.54 69 $1ACA1$ $5,250$ 11 43.03 | | 15BAC1 | 5,315 | 9 | 34.20 |
| 51 $15CCA1$ $5,270$ 9 17.13 52 $15CDB1$ $5,275$ 9 20.30 53 $15DBC1$ $5,287$ 9 31.58 54 $22BDB1$ $5,255$ 9 8.68 55 $22DDB1$ $5,223$ 9 5.93 56 $23DCC1$ $5,234$ 9 34.14 57 $23DDB1$ $5,223$ 9 34.14 57 $23DDE1$ $5,232$ 7 40.25 58 $23DDC1$ $5,232$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $26CBB1$ $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,195$ 11 62.14 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E 1AEC1$ $5,153$ 10 36.54 69 $1ACA1$ $5,250$ 11 43.03 | | 15BCB1 | 5,303 | 12 | 25.52 |
| 52 $15CDB1$ $5,275$ 9 20.30 53 $15DBC1$ $5,287$ 9 31.58 54 $22BDB1$ $5,255$ 9 8.68 55 $22DDB1$ $5,223$ 9 5.93 56 $23DCC1$ $5,234$ 9 34.14 57 $23DDB1$ $5,240$ 7 40.25 58 $23DDC1$ $5,232$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $26CBB1$ $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E 1ACA1$ $5,250$ 11 43.03 | 50 | 15CBA1 | 5,288 | 11 | 17.79 |
| 52 $15CDB1$ $5,275$ 9 20.30 53 $15DBC1$ $5,287$ 9 31.58 54 $22BDB1$ $5,255$ 9 8.68 55 $22DDB1$ $5,223$ 9 5.93 56 $23DCC1$ $5,234$ 9 34.14 57 $23DDB1$ $5,240$ 7 40.25 58 $23DDC1$ $5,232$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $26CBB1$ $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E 1ACA1$ $5,250$ 11 43.03 | 51 | 15CCA1 | 5,270 | 9 | 17.13 |
| 5315DBC1 $5,287$ 9 31.58 54 22BDB1 $5,255$ 9 8.68 55 22DDB1 $5,223$ 9 5.93 56 23DCC1 $5,234$ 9 34.14 57 23DDB1 $5,240$ 7 40.25 58 23DDC1 $5,232$ 7 45.55 59 26ABA1 $5,219$ 7 36.25 60 26CBB1 $5,197$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36CA1$ $5,235$ 9 90.80 67 $31CCD1$ $5,235$ 9 90.80 67 $31CCD1$ $5,250$ 11 75.29 68 $1N-18E 1ABC1$ $5,250$ 11 43.03 | | 15CDB1 | 5,275 | 9 | 20.30 |
| 56 $23DCC1$ $5,234$ 9 34.14 57 $23DDB1$ $5,240$ 7 40.25 58 $23DDC1$ $5,232$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $26CBB1$ $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E 1ABC1$ $5,250$ 11 43.03 | | 15DBC1 | | 9 | 31.58 |
| 56 $23DCC1$ $5,234$ 9 34.14 57 $23DDB1$ $5,240$ 7 40.25 58 $23DDC1$ $5,232$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $26CBB1$ $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E 1ABC1$ $5,250$ 11 43.03 | | | | 9 | |
| 57 $23DDB1$ $5,240$ 7 40.25 58 $23DDC1$ $5,232$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $26CBB1$ $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E-1ABC1$ $5,250$ 11 43.03 | 55 | 22DDB1 | 5,223 | 9 | 5.93 |
| 58 $23DDC1$ $5,232$ 7 45.55 59 $26ABA1$ $5,219$ 7 36.25 60 $26CBB1$ $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E 1ABC1$ $5,153$ 10 36.54 69 $1ACA1$ $5,250$ 11 43.03 | | 23DCC1 | 5,234 | 9 | 34.14 |
| 5926ABA1 $5,219$ 7 36.25 6026CBB1 $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,153$ 10 36.54 68 $1N-18E 1ABC1$ $5,250$ 11 43.03 | | 23DDB1 | 5,240 | | 40.25 |
| 60 $26CBB1$ $5,197$ 9 4.50 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E-1ABC1$ $5,153$ 10 36.54 69 $1ACA1$ $5,250$ 11 43.03 | | 23DDC1 | 5,232 | | 45.55 |
| 61 $35BAB1$ $5,178$ 9 4.99 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E-1ABC1$ $5,153$ 10 36.54 69 $1ACA1$ $5,250$ 11 43.03 | | 26ABA1 | 5,219 | 7 | 36.25 |
| 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E-1ABC1$ $5,153$ 10 36.54 69 $1ACA1$ $5,250$ 11 43.03 | 60 | 26CBB1 | 5,197 | 9 | 4.50 |
| 62 $35DCD1$ $5,147$ 11 6.77 63 $36BCB1$ $5,158$ 10 4.43 64 $36DAC1$ $5,195$ 11 62.14 65 $36DCA1$ $5,173$ 9 42.49 66 $2N-19E-31CAB1$ $5,235$ 9 90.80 67 $31CCD1$ $5,200$ 11 75.29 68 $1N-18E-1ABC1$ $5,153$ 10 36.54 69 $1ACA1$ $5,250$ 11 43.03 | 61 | 35BAB1 | 5,178 | 9 | 4.99 |
| 64 36DAC1 5,195 11 62.14 65 36DCA1 5,173 9 42.49 66 2N-19E-31CAB1 5,235 9 90.80 67 31CCD1 5,200 11 75.29 68 1N-18E- 1ABC1 5,153 10 36.54 69 1ACA1 5,250 11 43.03 | 62 | 35DCD1 | 5,147 | 11 | 6.77 |
| 65 36DCA1 5,173 9 42.49 66 2N-19E-31CAB1 5,235 9 90.80 67 31CCD1 5,200 11 75.29 68 1N-18E- 1ABC1 5,153 10 36.54 69 1ACA1 5,250 11 43.03 | 63 | 36BCB1 | 5,158 | 10 | 4.43 |
| 662N-19E-31CAB15,235990.806731CCD15,2001175.29681N-18E-1ABC15,1531036.54691ACA15,2501143.03 | 64 | 36DAC1 | 5,195 | 11 | 62.14 |
| 6731CCD15,2001175.29681N-18E-1ABC15,1531036.54691ACA15,2501143.03 | 65 | 36DCA1 | | 9 | 42.49 |
| 6731CCD15,2001175.29681N-18E-1ABC15,1531036.54691ACA15,2501143.03 | 66 | 2N-19E-31CAB1 | 5,235 | 9 | 90.80 |
| 681N-18E-1ABC15,1531036.54691ACA15,2501143.03 | | 31CCD1 | | | |
| 69 1ACA1 5,250 11 43.03 | | | | | |
| | 69 | | | | |
| | 70 | 1DAA1 | | 10 | 43.54 |

Table 1.--Ground-water levels during April 1986--Continued

| Well number | Well location | Altitude of land surface (feet above sea level) | - | Depth of water below land surface (feet) |
|----------------|------------------|--|----|---|
| 71 | 1N-18E- 1DBB1 | 5,127 | 10 | 24.60 |
| 72 | 12ACA1 | 5,090 | 10 | 17.69 |
| 73 | 12DBD1 | 5,100 | 10 | 44.00 |
| 74 | 12DDC1 | 5,100 | 11 | 46.03 |
| 75 | 13DDB1 | 5,078 | 11 | 75.29 |
| 76 | 1N-19E- 6CBB1 | 5,137 | 10 | 43.58 |
| 77 | 7BAC1 | 5,115 | 10 | 51.19 |
| 78 | 7BCD1 | 5,115 | 11 | 49.11 |
| 79 | 18AAC1 | 5,078 | 10 | 59.77 |
| 80 | 18ADA1 | 5,070 | 10 | 61.85 |
| 81 | 18BBD1 | 5,095 | 11 | 47.34 |
| 82 | 18CAA1 | 5,082 | 10 | 108.73 |
| 83 | 19BAB1 | 5,065 | 11 | 69.18 |
| 84 | 20BAA1 | 5,041 | 10 | 79.35 |

Table 1.--Ground-water levels during April 1986--Continued





to estimate T in water-table aquifers of unconsolidated sediments. Theis (1963, p. 334) noted that where calculated T' values were greater than 13,300 ft²/d, the actual T was greater than the estimated value.

The second empirical method is that of Thomasson and others (1960, p. 222), who noted that transmissivity of valley-fill sediments in California averaged 267 times specific capacity.

Estimates of hydraulic conductivity for the alluvial aquifer were obtained by dividing T by the saturated thickness of the aquifer. In the upper Big Wood River basin, K averaged 150 ft/d by use of Theis' method and 300 ft/d by use of Thomasson and others' method (table 2). Moreland (1977, p. 11) noted that transmissivity near Bellevue ranged from 30,000 to 70,000 ft²/d (K ranged from 200 to 470 ft/d); his estimates were obtained by multiplying specific capacity by 267.

During this study, two Hailey City wells were pumped by the Idaho Department of Water Resources to determine pump efficiencies, and discharge and water-level drawdown were measured. Data from the pump efficiency tests were used in an image well analysis for an infinite strip aquifer with a recharge boundary and a barrier boundary. Hydraulic conductivity determined with this procedure was 310 ft/d at well 2N-18E-9BDC1 and 490 ft/d at well 2N-18E-9DDA1. Because of the limited quantity of data used to estimate hydraulic conductivity, a range of K values from 150 to 500 ft/d was used. Heath (1983, p. 13) showed that hydraulic conductivity values from 150 to 500 ft/d commonly were associated with coarse sand aquifers.

Ground-water discharge from a basin may be computed from the equation:

$$Q = 365/43,560 \text{ KAh}$$
 (2)

where

| Q | = annual ground-water discharge, in acre-feet per |
|---------------------|--|
| 365/43 , 560 | <pre>year; = constant to convert cubic feet per day to acre-</pre> |
| | feet per year; |
| K | = hydraulic conductivity, in feet per day; |
| A | = cross-sectional area of aquifer, in feet |
| | squared; and |
| h | = hydraulic gradient, in feet per mile. |

Thickness of alluvial deposits at Glendale Road was estimated using seismic refraction techniques. The cross section (fig. 8) constructed with the seismic data is not perpendicular to the direction of ground-water flow. Estimates of flow through this cross section must be multiplied by the sine of 60 degrees to correct for the flow angle. Total saturated area of the cross

Table 2.--Characteristics of wells and estimated hydraulic conductivity (K)

| Well location | Radius (in.) | Saturated thickness (ft) | Discharge (gal/min) | Drawdown (ft) | Pumping time (days) | Specific capacity [(gal/min)/ft] | K (Theis 1963) (ft/d) | K (Thomasso and others 1960) (ft/d) |
|------------------|-----------------|--------------------------------|------------------------|------------------|---------------------------|--|--------------------------------|---|
| 4N-18E-19 | 8 | 40 | 1,840 | 14 | 0.42 | 131 | 480 | 880 |
| 2N-18E- 9 | 6 | 150 | 2,240 | 32 | .21 | 70 | 70 | 120 |
| 2N-18E- 9 | 8 | 150 | 2,000 | 60 | .25 | 33 | 30 | 60 |
| 1N-18E- 1 | 10 | 190 | 3,300 | 49 | .12 | 67 | 40 | 90 |
| 1N-19E- 7 | 10 | 190 | 2,600 | 8 | .17 | 325 | 200 | 460 |
| 1N-19E-17 | 10 | 190 | 1,890 | 13 | .25 | 145 | 90 | 200 |
| | | | | | | | 150 | 300 |

[Estimated values are rounded]

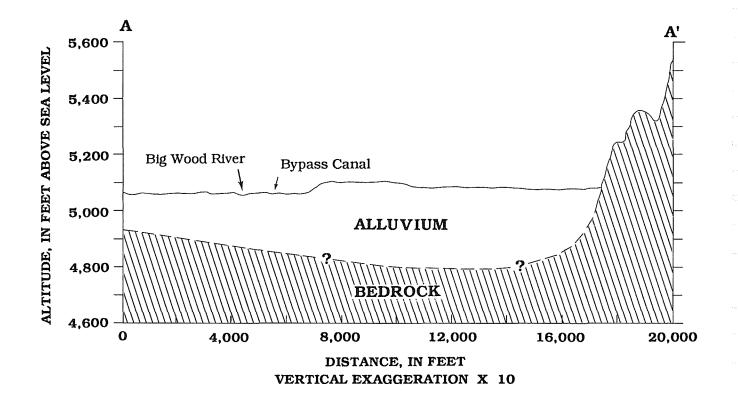


Figure 8.--Geologic section near Glendale Road. (Location of section on figure 2)

section, which was estimated using the water-table altitude from April 1986, was 3,300,000 ft². Average annual ground-water discharge from the study area estimated by using K = 300 ft/d and h = 43 ft/mi (determined from April 1986 water-level measurements) is 59,000 acre-ft/yr. Ground-water discharge at Hailey was estimated for use in water-budget calculations. Average annual ground-water discharge at Hailey, estimated using K = 300 ft/d, A = 820,000 ft², and h = 33 ft/mi, is 13,000 acre-ft/yr. This This estimated ground-water discharge is substantially smaller than the 34,000 acre-ft/yr estimated by Smith (1959, p. 21) and the 40,000 acre-ft/yr estimated by Luttrell and Brockway (1984, p. 58). Smith's (1959) analysis did not include effects of recharge from the Big Wood River on results of aquifer tests; therefore, his estimated K value of about 900 ft/d is probably high. Luttrell and Brockway (1984, p. 58) determined underflow by subtracting the average discharge for the Big Wood River at Hailey (not including the Big Wood Slough) from an empirically calculated water yield; therefore, their underflow value includes evapotranspiration from phreatophytes, crops, and rangeland, and surface water that bypasses the gaging station at Hailey.

Surface-Water and Ground-Water Relations

Surface-water and ground-water systems are interconnected in the upper Big Wood River basin. The Big Wood River gains or loses water with respect to the ground-water system, depending on local conditions. Where the altitude of the ground-water surface is higher than the altitude of the stream, some ground water may enter the stream channel, and discharge in the stream will increase. If the altitude of the ground-water surface is below that of the stream channel, discharge in the stream may decrease as a result of seepage losses.

During August 1986, a seepage study was made on the Big Wood River immediately upstream from Ketchum to Glendale Road. Discharge of the Big Wood River was measured below Adams Gulch, above the mouth of the East Fork Big Wood River, at the upper crossing of Broadford Road near Hailey, and at Glendale Road. Inflows to the river and diversions from the river were located and measured during the study. Inflows were measured as close to the mouth as possible, and diversions were measured below any spillback to the river. Gain from or loss to ground water in a given reach was calculated by adding diversions from the reach to the final river discharge and subtracting inflows to the reach and the initial river discharge. A positive result shows that the reach gained flow from ground water. During this seepage study, the river gained water from above Ketchum to between Hailey and Bellevue and lost from that point to Glendale Road (table 3). Hydrographs for four wells measured monthly from April 1986 through November 1987 and for the Big Wood River at Hailey are shown in figure 9; well locations are shown in figure 10. Seasonal variations in ground-water levels are similar to

Table 3. -- Inflows and diversions of the Big Wood River from above Ketchum to Glendale Road, August 1986

[Values in cubic feet per second; gain or loss rounded]

| Location | Big Wood River | Inflows | Diversions | Gain from ground water | Loss to ground water |
|--------------------------------|--|---------|------------|---------------------------|-------------------------|
| Below Adams Gulch | 181 | | | | |
| Unnamed tributary, left bank | | 0.2 | | | |
| Unnamed tributary, right bank | | 1.5 | | | |
| Unnamed tributary, left bank | | 13.2 | | | |
| Warm Springs Creek | | 48.1 | | | |
| Trail Creek | | 25.6 | | | |
| Subtotal for reach | · · · · · · · · · · · · · · · · · · · | 88.6 | 0 | | |
| Above East Fork Big Wood River | 309 | | | 39 | |
| East Fork Big Wood River | | 42.6 | | | |
| Mizer Ditch | | | .5 | | |
| Unnamed tributary, left bank | | .6 | | | |
| Hiawatha Canal | | 2 | 50.5 | | |
| Unnamed tributary, right bank | | .3 | | | |
| Unnamed tributary, left bank | | .9 | | | |
| Croy Creek Cove Canal | | 4.8 | 11.7 | | |
| | | | 23.3 | | |
| Unnamed diversion, right bank | | | 23.3 | | |
| Subtotal for reach | • | 49.2 | 86 | | |
| Jpper crossing, Broadford Road | 308 | | | 36 | |
| Unnamed diversion, left bank | | | 5.7 | | |
| District Canal | | | 172 | | |
| Bypass Canal | | | 58.6 | | |
| Glendale Canal | | | 22.2 | | |
| Subtotal for reach | · · · · · <i>· ·</i> · · · · · · · · · · · · | 0 | 258 | | |
| Glendale Road | .7 | | | | 49 |

.

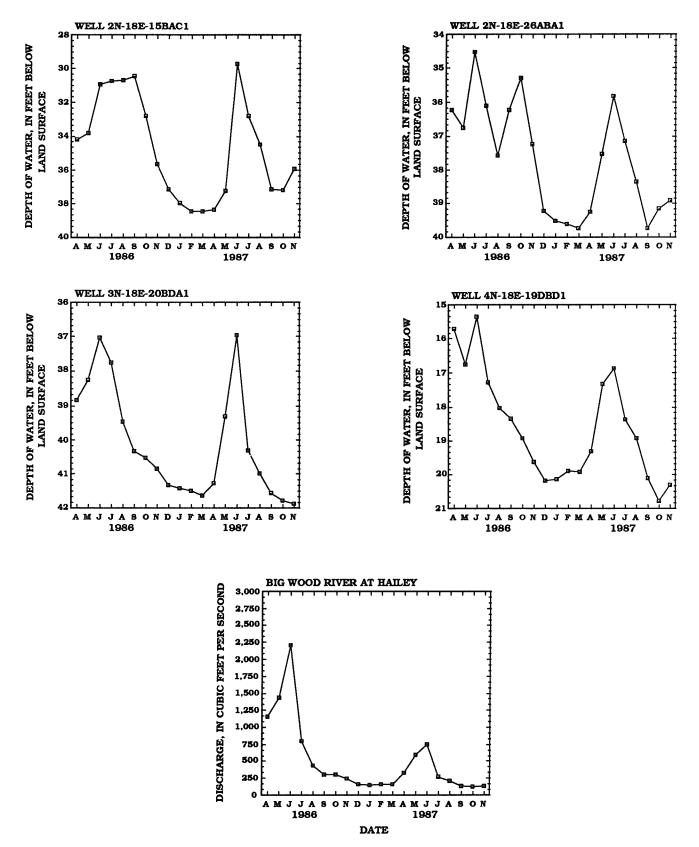


Figure 9.--Water levels for selected observation wells and discharge of the Big Wood River at Hailey. (Locations shown in figure 10)

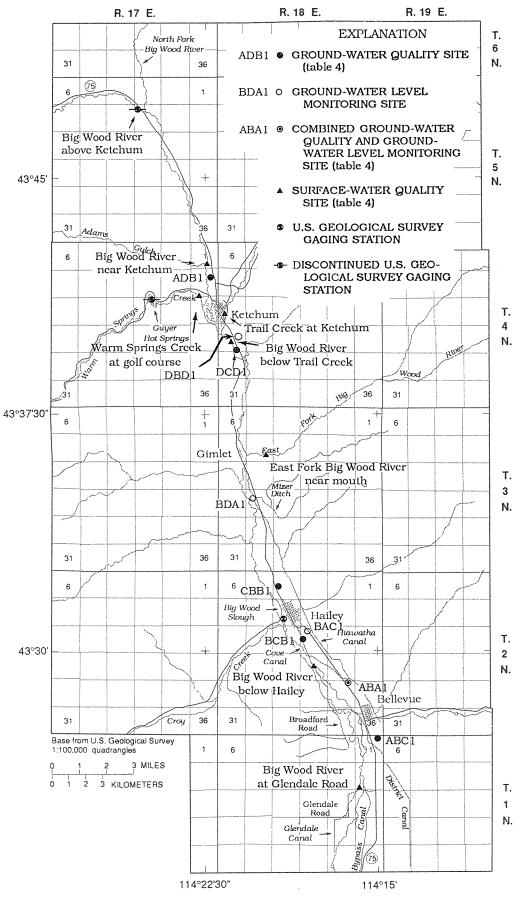


Figure 10.--Locations of water-quality and ground-water level monitoring sites.

variations in discharge of the Big Wood River and indicate a hydraulic connection between the systems. Ground-water levels are elevated by recharge from water seeping from canals, river channels, and irrigated fields. Water levels in wells 4N-18E-19DBD1 and 3N-18E-20BDA1 and the Big Wood River respond to the spring snowmelt and relatively dry summers. Water levels in well 2N-18E-15BAC1 are affected by surface-water diversions into a lateral from Hiawatha Canal, within 600 ft of the well. The sustained high water level during summer 1986 coincides with the period of diversions into Hiawatha Canal. During 1987, more water was diverted into Hiawatha Canal than during 1986 (Water District #37 and Water District #37M, 1986, p. 31; 1987, p. 41). However, because of below-normal runoff during 1987, most of the water was allocated to downstream users (Water District #37 and Water District #37M, 1986, p. 10; 1987, p. 7), and little water probably was diverted into the lateral near well 2N-18E-15BAC1. Water levels in well 2N-18E-26ABA1 also are affected by surface-water diversions. Cove Canal is within 700 ft of the well, and an adjacent field is surface-water irrigated.

Water Ouality

Water-quality data were collected during November 1986, March 1987, and August 1987 at seven surface-water sites and six groundwater sites above and below population centers (fig. 10). Sampling represented times when seasonal population was low, October through November, and when seasonal population was high, January through March. Samples were analyzed for nutrients (NO_2 , NO_2+NO_3 , and PO_4) and chloride to determine effects of upstream urban development and sewage disposal on ground- and surface-water quality, and for cadmium, lead, and zinc because of historical intensive mining in the region.

Specific conductance, pH, alkalinity, water temperature, and dissolved oxygen (surface water only) were measured onsite. Surface-water samples were collected by using cross-sectional and depth-integrating methods described by Guy and Norman (1970, p. Ground-water samples were collected using methods 30-32). described by Wood (1976, p. 4). Samples for laboratory analysis were filtered onsite through a 0.45-micrometer filter. Filters were rinsed with 250 mL (milliliters) of distilled water and 50 mL of sample water before being used to filter water to be analyzed. Samples for metals analysis were preserved with nitric acid. Samples for nutrient analysis were placed in an opaque bottle, preserved with mercuric chloride, and chilled. Water-quality data are shown in table 4. In general, concentrations of most constituents increased downgradient as a result of dissolution of minerals in soils and the aquifer.

Fluoride concentrations in surface and ground water ranged from 0.10 to 1.5 mg/L (table 4). Hem (1985, p. 120) noted that fluoride concentrations in most natural water are less than 1.0

Table 4.--Water-quality data

[Site locations in figure 10; --, no data available; <, less than]

| Site location | Date | Time (24-hour) | Water temper ature (°C) | - | Alkal (mg/L as Field | | Dissolved oxygen (mg/L) | Percent saturation | Solids, dissolved (mg/L) |
|--------------------|----------|-------------------|----------------------------------|------|----------------------------|-----|-------------------------------|-----------------------|--------------------------------|
| | | | Sur | face | Water | | | | |
| Big Wood River | 11- 4-86 | 1545 | 7.0 | 8.3 | 98 | 98 | 10.4 | 106 | 125 |
| above Ketchum | 3- 3-87 | 1615 | 3.5 | 8.4 | 102 | 102 | 10.7 | | 120 |
| Warm Springs Creek | 11- 5-86 | 1300 | 9.5 | 8.6 | 105 | 105 | 10.2 | 111 | 151 |
| at golf course | 3- 4-87 | 1600 | 9.5 | 8.8 | 110 | 112 | 9.4 | | 147 |
| Trail Creek | 11- 6-86 | 1200 | 5.0 | 8.5 | 188 | 192 | 11.2 | 110 | 242 |
| at Ketchum | 3- 5-87 | 1130 | 1.5 | 8.6 | 193 | 192 | 9.5 | | 254 |
| Big Wood River | 11- 3-86 | 1630 | 7.0 | 8.2 | 114 | 115 | 10.1 | 102 | 146 |
| below Trail Creek | 3- 4-87 | 1300 | 5.0 | 8.6 | 117 | 116 | 11.0 | | 144 |
| East Fork Big Wood | 11- 6-86 | 0800 | 2.5 | 8.2 | 150 | 151 | 11.1 | 101 | 219 |
| River near mouth | 3- 5-87 | 1000 | .0 | 8.5 | 168 | 165 | 11.3 | | 260 |
| Big Wood River | 11- 3-86 | 1400 | 7.5 | 8.7 | 132 | 129 | 11.3 | 114 | 173 |
| below Hailey | 3- 4-87 | 1030 | 3.5 | 8.5 | 137 | 133 | 11.7 | | 171 |
| Big Wood River | 11- 3-86 | 1130 | 7.0 | 8.6 | 135 | 135 | 11.1 | 110 | 175 |
| at Glendale Road | 3- 3-87 | 1130 | 4.0 | 8.7 | 136 | 137 | 11.5 | | 175 |

з

| Site location | Date | Time (24-hour) | Specific conductance (µS/cm) | | Nitrite, dissolved | Nitrite + nitrate, dissolved | Ortho- phosphate, dissolved | Fluoride, dissolved |
|--------------------|----------|-------------------|------------------------------------|---------|-----------------------|------------------------------------|-----------------------------------|------------------------|
| | | | Field | Lab | (mg/L as N) | (mg/L as N) | (mg/L as P) | (mg/L as F) |
| | | | Surface | e Water | Continued | | | |
| Big Wood River | 11- 4-86 | 1545 | 211 | 209 | <0.010 | <0.100 | <0.010 | 0.20 |
| above Ketchum | 3- 3-87 | 1615 | 209 | 194 | <.010 | <.100 | <.010 | .20 |
| Warm Springs Creek | 11- 5-86 | 1300 | 238 | 236 | <.010 | <.100 | <.010 | 1.5 |
| at golf course | 3- 4-87 | 1600 | 228 | 245 | <.010 | <.100 | <.010 | 1.4 |
| Trail Creek | 11- 6-86 | 1200 | 409 | 411 | <.010 | <.100 | <.010 | .10 |
| at Ketchum | 3- 5-87 | 1130 | 418 | 434 | <.010 | <.100 | <.010 | .20 |
| Big Wood River | 11- 3-86 | 1630 | 234 | 246 | <.010 | <.100 | <.010 | .40 |
| below Trail Creek | 3- 4-87 | 1300 | 234 | 253 | <.010 | <.100 | <.010 | .60 |
| East Fork Big Wood | 11- 6-86 | 0800 | 354 | 357 | <.010 | <.100 | <.010 | .10 |
| River near mouth | 3- 5-87 | 1000 | 403 | 426 | <.010 | <.100 | <.010 | .10 |
| Big Wood River | 11- 3-86 | 1400 | 286 | 280 | <.010 | <.100 | .010 | .40 |
| below Hailey | 3- 4-87 | 1030 | 282 | 299 | <.010 | .230 | .021 | .40 |
| Big Wood River at | 11- 3-86 | 1130 | 294 | 290 | <.010 | <.100 | <.010 | .40 |
| Glendale Road | 3- 3-87 | 1130 | 290 | 305 | <.010 | .190 | <.010 | .40 |

Table 4.--Water-quality data--Continued

27

| | Site location | Date | Time (24-hour) | Chloride, dissolved (mg/L as Cl) | Sulfate, dissolved (mg/L as SO ₄) | Cadmium, dissolved (µg/L as Cd) | Lead, dissolved (µg/L as Pb) | Zinc, dissolved (µg/L as Zn) | | | |
|----|--|---------------------|-------------------|--|---|---------------------------------------|------------------------------------|------------------------------------|--|--|--|
| | Surface WaterContinued | | | | | | | | | | |
| | Big Wood River above Ketchum | 11- 4-86 3- 3-87 | 1545 1615 | 0.80 1.2 | 10 13 | <1 | <5 | 8 | | | |
| 28 | Warm Springs Creek at golf course | 11- 5-86 3- 4-87 | 1300 1600 | 2.0 2.1 | 12 15 | <1 | <5 | 4 | | | |
| | Trail Creek at Ketchum | 11- 6-86 3- 5-87 | 1200 1130 | 1.5 2.6 | 46 52 | <1 | 8 | 10 | | | |
| | Big Wood River below Trail Creek | 11- 3-86 3- 4-87 | 1630 1300 | 1.2 1.5 | 14 17 | <1 | <5 | 8 | | | |
| | East Fork Big Wood River near mouth | 11- 6-86 3- 5-87 | 0800 1000 | 1.52.2 | 43 68 | <1 | <5 | 9 | | | |
| | Big Wood River below Hailey | 11- 3-86 3- 4-87 | 1400 1030 | 1.9 2.7 | 19 22 | <1 | 5 | 17 | | | |
| | Big Wood River at Glendale Road | 11- 3-86 3- 3-87 | 1130 1130 | 1.8 2.9 | 20 23 | <1 | <5 | <u> 6</u> | | | |

Table 4.--Water-quality data--Continued

| | | Time | Water temperature | | Alkal: (mg/L as | CaCO ₃) | Solids dissolved |
|---------------|----------|-----------|----------------------|-----|--------------------|---------------------|---------------------|
| Site location | Date | (24-hour) | (°C) | рН | Field | Lab | (mg/L) |
| | | | Ground Water | | | <u> </u> | |
| 4N-17E-12ADB1 | 11- 5-86 | 0845 | 9.0 | 7.6 | 122 | 121 | 151 |
| | 3- 3-87 | 1545 | 7.0 | 7.8 | 117 | 117 | 137 |
| | 8- 5-87 | 1510 | 9.0 | | | | |
| 4N-18E-19DCD1 | 11- 5-86 | 1100 | 8.5 | 7.8 | 153 | 150 | 196 |
| | 3- 4-87 | 1520 | 4.5 | 7.8 | 150 | 149 | 187 |
| 2N-18E- 4CBB1 | 11- 4-86 | 1400 | 12.0 | 7.6 | 166 | 168 | 205 |
| | 3- 3-87 | 1430 | 9.5 | 7.8 | 165 | 163 | 193 |
| | 8- 5-87 | 1420 | 10.5 | | | | |
| 2N-18E-15BCB1 | 11- 4-86 | 1220 | 11.0 | 7.6 | 174 | 173 | 219 |
| | 3- 4-87 | 0945 | 10.0 | 7.6 | 184 | 181 | 213 |
| | 8- 5-87 | 1150 | 12.0 | | | | |
| 2N-18E-26ABA1 | 11- 4-86 | 0900 | 10.0 | 7.6 | 189 | 188 | 230 |
| | 3- 4-87 | 0900 | 11.0 | 7.7 | 184 | 182 | 210 |
| | 8- 5-87 | 1130 | 10.0 | | | | |
| 1N-18E- 1ABC1 | 11- 4-86 | 1030 | 12.5 | 7.6 | 140 | 140 | 170 |
| | 3- 3-87 | 1300 | 4.0 | 7.9 | 135 | 134 | 167 |
| | 8- 5-87 | 1345 | 12.0 | | | | |

Table 4.--Water-quality data--Continued

| Site location | Date | Time (24-hour) | Spec conduc (µS/ Field | tance | Nitrite, dissolved (mg/L as N) | Nitrite + nitrate, dissolved (mg/L as N) | Ortho- phosphate, dissolved (mg/L as P) | Fluoride, dissolved (mg/L as F) |
|---------------|--------------------------------|----------------------|---------------------------------|----------------|--------------------------------------|---|--|---------------------------------------|
| | | | Gr | ound Wa | terContinued | ,, , | | |
| 4N-17E-12ADB1 | 11- 5-86 3- 3-87 8- 5-87 | 0845 1545 1510 | 234 241 239 | 248 246 | <0.010 <.10 | 0.110 .140 | <0.010 <.010 | 0.20 .20 |
| 4N-18E-19DCD1 | 11- 5-86 3- 4-87 | 1100 1520 | 326 325 | 332 334 | <.010 <.010 | .250 .240 | .010 <.010 | .30 .40 |
| 2N-18E- 4CBB1 | 11- 4-87 3- 3-87 8- 5-87 | 1400 1430 1420 | 333 330 341 | 348 348 | <.010 <.010 | .450 .460 | <.010 <.010 | .30 .30 |
| 2N-18E-15BCB1 | 11- 4-86 3- 4-87 8- 5-87 | 1220 0945 1150 | 366 358 370 | 365 373 | <.010 <.010 | .970 .530 | .021 <.010 | .30 .30 |
| 2N-18E-26ABA1 | 11- 4-86 3- 4-87 8- 5-87 | 0900 0900 1130 | 381 358 372 | 388 374 | <.010 <.010 | 1.40 .750 | .021 .010 | .20 .20 |
| 1N-18E- 1ABC1 | 11- 4-86 3- 3-87 8- 5-87 | 1030 1300 1345 | 295 277 287 | 300 301 | <.010 <.010 | .171 .300 | .010 <.010 | .30 .30 |

Table 4.--Water-quality data--Continued

| Site location | Date | Time (24-hour) | Chloride, dissolved (mg/L as Cl) | Sulfate, dissolved (mg/L as SO ₄) | Cadmium, dissolved (µg/L as Cd) | Lead, dissolved (µg/L as Pb) | Zinc, dissolved (µg/L as Zn |
|---------------|---|-------------------|--|---|---------------------------------------|------------------------------------|-----------------------------------|
| | Mark Milling , / / / / / / / / / / / / / / | | Ground Wat | cerContinued | | | |
| 4N-17E-12ADB1 | 11- 5-86 | 0845 | 0.80 | 10 | <1 | <5 | 56 |
| | 3- 3-87 | 1545 | 1.0 | 13 | | | |
| | 8- 5-87 | 1510 | | | | | 20 |
| 4N-18E-19DCD1 | 11- 5-86 | 1100 | 1.6 | 25 | <1 | 5 | 5 |
| | 3- 4-87 | 1520 | 1.9 | 27 | | | |
| 2N-18E- 4CBB1 | 11- 4-86 | 1400 | 1.8 | 15 | <1 | <5 | 26 |
| | 3- 3-87 | 1430 | 2.5 | 19 | | | |
| | 8- 5-87 | 1420 | | | | | 20 |
| 2N-18E-15BCB1 | 11- 4-86 | 1220 | 3.7 | 17 | 1 | 5 | 219 |
| | 3- 4-87 | 0945 | 3.1 | 18 | | | |
| | 8- 5-87 | 1150 | | | | | 120 |
| 2N-18E-26ABA1 | 11- 4-86 | 0900 | 2.7 | 15 | <1 | <5 | 120 |
| | 3- 4-87 | 0900 | 2.6 | 17 | | | |
| | 8- 5-87 | 1130 | | | | | 100 |
| 1N-18E- 1ABC1 | 11- 4-86 | 1030 | 1.8 | 17 | <1 | <5 | 430 |
| | 3- 3-87 | 1300 | 2.4 | 21 | | | |
| | 8- 5-87 | 1345 | | | | | 80 |

Table 4.--Water-quality data--Continued

mg/L. Warm Springs Creek was the only site where fluoride concentrations were greater than 0.60 mg/L. Fluoride concentrations as high as 16 mg/L were reported by Young and Mitchell (1973, p. 23) in thermal water from Guyer Hot Springs. Thermal water flowing from Guyer Hot Springs into Warm Springs Creek probably is the source for elevated fluoride concentrations.

Many constituents sampled were in concentrations less than analytical detection levels. Nutrient concentrations in surface water were near or below detection levels (table 4), which indicates insignificant changes in water quality due to upstream urban development and sewage disposal. Cadmium and lead concentrations were generally below detection levels, but zinc The drinking concentrations were as high as 430 μ g/L (table 4). water standard for zinc is 5,000 μ g/L (U.S. Environmental The two highest zinc concentrations Protection Agency, 1986). were detected in ground water immediately downgradient from Hailey and Bellevue during November 1986. Most ground-water quality sites were resampled in August 1987 to confirm previous analyses of zinc concentrations. The length of time wells were pumped prior to sample collection was approximately tripled from the Zinc concentrations were lower in August, November sampling. possibly because of the increased pumping time, which reduces the chance of contamination of the sample from contact with the well casing or with any galvanized pipe in the discharge line.

Ranges of nutrient data collected during this and previous studies are presented in table 5. Data from these reports and this study show that nutrient levels in the upper Big Wood River basin have not changed substantially during the past 30 years and that water quality is adequate for drinking and agricultural uses.

WATER YIELD

Water is supplied to the study area by precipitation and is discharged from the area by ET (evapotranspiration), by surface water in the Big Wood River and canals, by ground-water underflow, and by consumptive domestic uses. Yield is used in this report to represent the quantity of water leaving the upper Big Wood River basin or tributary and does not include ET from the mountainous areas. Yield was estimated by using the water-budget method as follows:

$$Y = ETR + ETC + ETP + SW + GW + CU$$
(3)

where

| ETR | = | ET from nonirrigated rangeland, |
|-----|---|---|
| ETC | = | ET from irrigated crops, |
| ETP | = | ET from phreatophytes, |
| SW | = | discharge of the Big Wood River and canals, |
| GW | = | ground-water discharge (underflow), and |
| CU | = | consumptive use by domestic water users. |

Table 5.--Ranges of nutrient concentrations, 1959-87

[--, no data available; <, less than]

| | | Nitrate a | as N (mg/L) | Orthophosphate as P (mg/L) | | |
|-------------|------------------------------|--------------|---------------------------------------|----------------------------|---------------|--|
| | Source | Ground water | Surface water | Ground water | Surface water | |
| - ω ω | | | · · · · · · · · · · · · · · · · · · · | | | |
| ω | Smith (1959) | <0.1 - 3.0 | 0.4 - 0.6 | | | |
| | Castelin and Winner (1975) | .1 - 1.4 | <.12 | | | |
| | Manuel and others (1978) | | .14 | | <0.01 - 0.10 | |
| | Luttrell and Brockway (1984) | .1 - 2.2 | .37 | <0.01 - 0.06 | <.0106 | |
| | 1986 to 1987 | .1 - 1.4 | <.12 | <.0102 | <.0102 | |
| | | | | | | |

ω ω Water-budget components were calculated for each year from 1940 to 1979; the average annual yield is shown in table 6.

Previous studies were examined to determine appropriate ET rates for the water budget. Smith (1959, p. 22) used the following ET rates in his water budget for the Big Wood River: irrigated crops, 1.8 ft/yr; nonirrigated lands, 1.0 ft/yr; and phreatophytes, 3.5 ft/yr. Meyers (1962, p. 91) estimated that evaporation from small streams in the Snake River basin was about 2.7 to 2.9 ft/yr. Williams and Young (1982, p. 18) estimated ET rates of 1.0 to 1.3 ft/yr for several basins in southern Idaho where mean annual precipitation is similar to that on the Big Wood River basin floor. For this study, the following ET rates were assigned: irrigated crops, 1.8 ft/yr; nonirrigated rangeland, 1.0 ft/yr; and phreatophyptes, 2.5 to 3.5 ft/yr.

An empirical method of estimating yield was developed by Langbein (Nace and others, 1961, p. 36-47). This method is based on relations between (1) altitude and temperature, (2) temperature and potential ET, and (3) the ratio of potential ET to precipitation and the ratio of yield to potential ET. То calibrate this method for the upper Big Wood River basin, the temperature-altitude equation was adjusted to result in the correct mean annual temperature at Hailey. Langbein (Nace and others, 1961, p. 46) noted that yield is not entirely explained by climatic variables and the method needs to be tested by comparing results with local measurements of yield and, if necessary, adjusting the coefficients in the yield equation. For this study, the coefficient by which potential ET was multiplied was determined by comparing calculated average yields with mean annual discharges for the Big Wood River near Ketchum and Warm Springs Creek at Guyer Hot Springs for their respective periods of record. The equations as adapted for conditions in the upper Big Wood River area are:

> t = -0.0035 (altitude) + 62 (4) PET = 0.73 (t) -12.25Y = 0.75 (P) -0.59 (PET)

where

t = mean annual temperature, in degrees Fahrenheit; PET = potential evapotranspiration, in inches; Y = annual water yield, in inches; and P = annual precipitation, in inches.

To convert yield in inches to acre-feet, multiply by the basin area (in acres) and divide by 12.

Basin areas and mean altitudes were determined for North Fork Big Wood River, Warm Springs Creek, Trail Creek, and East Fork Big Wood River basin. Basin area and mean altitude for the Big Wood River near Ketchum were obtained from a report by Kjelstrom and

Table 6.--Ranges of water-yield estimates based on water years 1940-79

| | Hailey | | | Q | Glendale Road | | | |
|---------------------------|-----------|---------|---------|---------|---------------|---------|--|--|
| Water-budget component | Low | Average | High | Low | Average | High | | |
| ETR | 18,000 | 21,000 | 24,000 | 24,000 | 27,000 | 30,000 | | |
| ETC | 2,800 | 3,200 | 3,600 | 6,700 | 7,300 | 7,900 | | |
| ETP | 5,000 | 6,000 | 7,000 | 8,500 | 10,000 | 12,000 | | |
| SW | 320,000 | 360,000 | 400,000 | 280,000 | 310,000 | 340,000 | | |
| GW | 5,900 | 13,000 | 25,000 | 22,000 | 59,000 | 120,000 | | |
| CU | 100 | 200 | 400 | 150 | 250 | 450 | | |
| Total | . 350,000 | 400,000 | 460,000 | 340,000 | 410,000 | 510,000 | | |

[Values, in acre-feet per year, are rounded]

ETR = ET from nonirrigated rangelands, 16,000 acres (Hailey), 20,000 acres (Glendale Road).

Low estimate: -1/2 standard deviation from average estimate. High estimate: +1/2 standard deviation from average estimate.

ETC = ET from irrigated crops, determined by subtracting the quantity of diversions that bypass a reach from total diversions above the reach and multiplying by 0.1 to account for return flows and nonirrigation diversions included in the total.

Low estimate: -1/2 standard deviation from average estimate. High estimate: +1/2 standard deviation from average estimate.

ETP = ET from phreatophytes, 2,000 acres (Hailey), 3,400 acres (Glendale Road).

Low estimate: 2.5 acre-ft/acre. Average estimate: 3.0 acre-ft/acre. 3.5 acre-ft/acre. High estimate:

SW

= Discharge of the Big Wood River (gaged at Hailey) and canals. Average at Glendale Road estimated by adding SW, ETC, ETP, and GW at Hailey and subtracting ETC, ETP, and GW at Glendale Road.

Low estimate: -10 percent of average estimate. High estimate: +10 percent of average estimate.

GW = Ground-water discharge based on the following characteristics:

| | Low | Average | High |
|------------------|---|---|---|
| Hailey | K = 150 ft/d A = 820,000 ft ² h = 30 ft/mi f = 90 degrees | 300 ft/d 820,000 ft ² 33 ft/mi 90 degrees | 500 ft/d 820,000 ft ² 38 ft/mi 90 degrees |
| Glendale Road | K = 150 ft/d $A = 3,300,000 \text{ ft}^2$ h = 33 ft/mi f = 60 degrees | 300 ft/d 3,300,000 ft ² 43 ft/mi 60 degrees | 500 ft/d 3,300,000 ft ² 51 ft/mi 60 degrees |

K = Hydraulic conductivity,

A = cross-sectional area of the aquifer,

h = hydraulic gradient, and

f = angle of flow through cross section.

= Consumptive use by domestic water users. Estimates based on consumptive use of water withdrawn for domestic and commercial use in Idaho (Solley CII and others, 1988, p. 17).

Moffatt (1981, p. 96). Basin areas and mean altitudes for other areas not listed above were determined but not separated other than to identify them as either above Hailey or between Hailey and Glendale Road. Basin areas, mean altitudes, and mean annual precipitation are shown in table 7.

Yield was calculated for the basin above Hailey and for the basin above Glendale Road. Yields at Hailey estimated by the water-budget method are compared graphically with gaged surfacewater discharge at Hailey (fig. 11), which provides a useful measure for examining the reliability of estimated yields. Variations in surface-water discharge and estimated yield are similar because surface-water discharge is much larger than any other component included in yield estimates (fig. 12). Mean annual yield at Hailey, estimated using the water-budget method, was about 400,000 acre-ft and, using the Langbein method, was about 420,000 acre-ft (table 8). Mean annual surface-water discharge at Hailey, including diversions that bypass the gage, for the same period was 360,000 acre-ft. Mean annual yield at Glendale Road, estimated using the water-budget method, was 410,000 acre-ft and, using the Langbein method, was 460,000 acreft (table 8).

Average yield for 1940-79, estimated using the Langbein method, was greater than the average value of the water-budget method but was less than the high value shown in table 6. The results verify the Langbein method and indicate that it could be used if data for a water budget were not available. The waterbudget method is probably more accurate because a large percentage of the water budget is surface water, which is measured rather than estimated.

The Langbein method is based on average climatic conditions and can be expected to produce reasonable results for years when climatic conditions are near average or over a long time period. When precipitation is extreme (low or high), this method does not produce reasonable results, such as in 1987 when precipitation was about half of average and was reflected by the subsequent low runoff (fig. 13).

During 1986, precipitation in the basin was about 7 in. (26 percent) above average. Yield for the basin above Glendale Road during 1986, estimated using the water-budget method, was 580,000 acre-ft and, using the Langbein method, was 660,000 acre-ft. Yield during 1987, estimated using the water-budget method, was 230,000 acre-ft and, using the Langbein method, was 94,000 acre-ft.

Tributary Yield

Yields were estimated for three major tributary basins in the study area. Few historical discharge data were available for

| Drainage | Area (square miles) | Mean altitude (feet above sea level) | Mean annual precipitation (inches) |
|-----------------------------|------------------------|--|--|
| Big Wood River near Ketchum | 137 | 8,120 | 31 |
| North Fork Big Wood River | 40 | 8,630 | 33 |
| Trail Creek | 65 | 8,120 | 31 |
| Warm Springs Creek | 96 | 7,660 | 28 |
| East Fork Big Wood River | 85 | 7,870 | 29 |
| Valley floor | 36 | 5,800 | 17 |
| Other | 177 | 7,120 | 25 |
| Total above Hailey | 636 | 7,640 | 28 |
| Hailey to Glendale Road | 105 | 6,500 | 22 |
| South valley floor | 11 | 5,100 | 15 |
| Total above Glendale Road | 752 | 7,440 | 27 |

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Table 7.--Drainage areas, mean altitudes, and mean annual precipitation for various parts of the upper Big Wood River basin

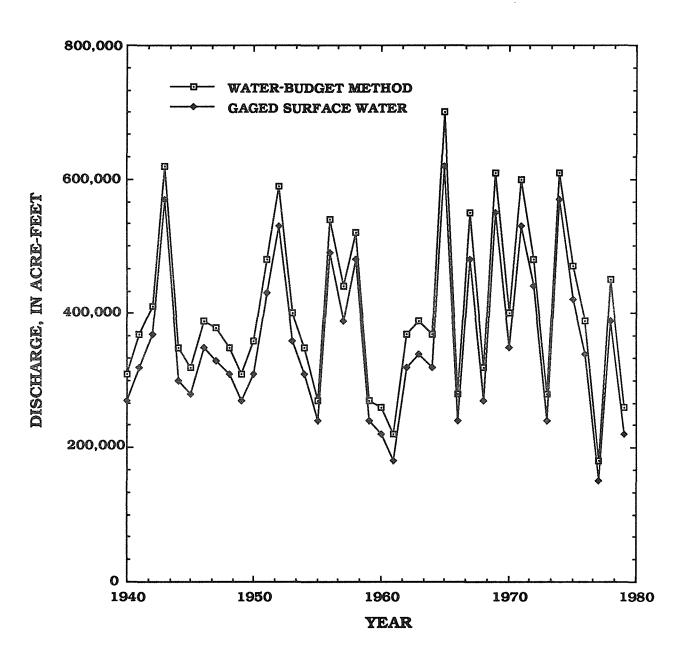
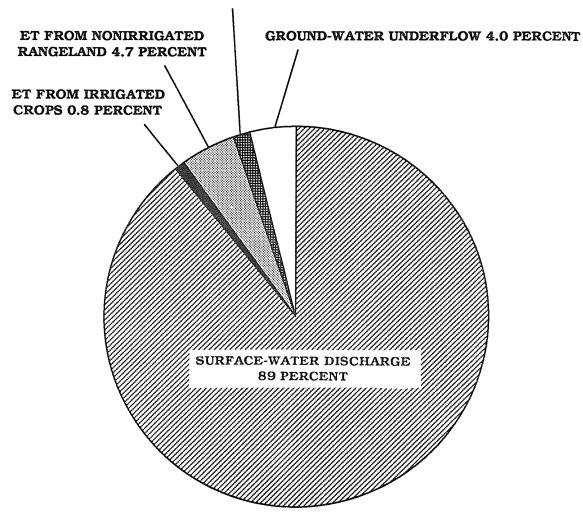


Figure 11.--Yield estimated by water-budget method and gaged surface-water discharge at Hailey, 1940-79.



ET FROM PHREATOPHYTES 1.5 PERCENT

Figure 12.--Relative percentage of water-budget components for yield from basin above Hailey.

| Location and period of estimate | Water-budget method (acre-feet) | Langbein (1961) method (acre-feet) |
|------------------------------------|---------------------------------------|--|
| Above Hailey | | |
| 1940-79 | 400,000 | 420,000 |
| Standard deviation | 120,000 | 100,000 |
| 1986 | 560,000 | 590,000 |
| 1987 | 220,000 | 110,000 |
| Above Glendale Road | | |
| 1940-79 | 410,000 | 460,000 |
| Standard deviation | 120,000 | 120,000 |
| 1986 | 580,000 | 660,000 |
| 1987 | 230,000 | 94,000 |

Table 8.--Estimated water yield and standard deviation of average estimates

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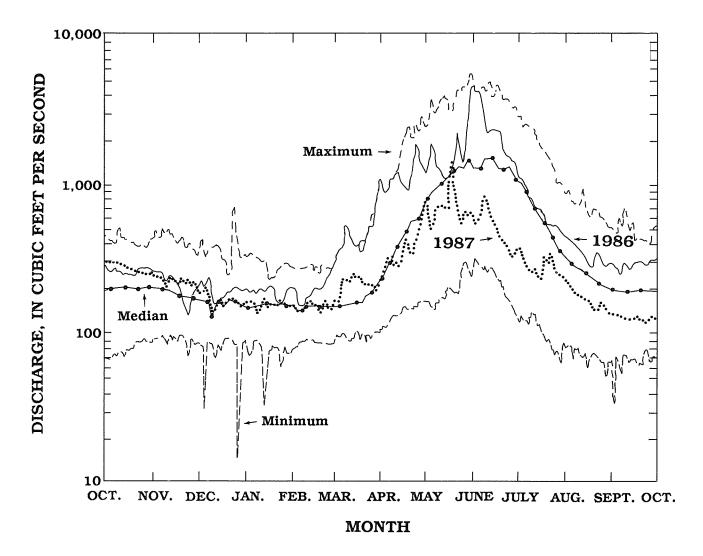


Figure 13.--Maximum, median, and minimum mean daily discharge of the Big Wood River at Hailey, water years 1915-86, compared with mean daily discharge during water years 1986 and 1987.

Trail Creek and East Fork Big Wood River; a continuous record of discharge for Warm Springs Creek was collected from 1940 to 1958. During 1986 and 1987, tributary basin yields were calculated from monthly discharge measurements. The Riggs (1969) method correlates monthly discharge measurements on ungaged streams to mean daily discharge on gaged streams for the date of the discharge measurement. The ratio of daily discharges on ungaged and gaged streams is used to calculate monthly mean discharge for the ungaged stream from the monthly mean discharge of the gaged Monthly mean discharges are summed for the year and stream. divided by 12 to give the mean annual surface-water discharge. The mean annual surface-water discharge from a basin is equal to the basin yield where ground-water underflow is insignificant. Ground-water underflow from Trail Creek, Warm Springs Creek, and East Fork Big Wood River is probably small. Smith (1960, p. 34) estimated that underflow at the Warm Springs Creek gaging station was less than 1 percent of the yield.

Gaging stations used in the Riggs method of calculating yield for Warm Springs Creek, Trail Creek, and East Fork Big Wood River were Big Wood River at Hailey and North Fork Big Lost River at Wild Horse. Accuracy of the Riggs method depends on the hydrologic similarity of gaged and ungaged basins. The North Fork Big Lost River basin (114 mi²) is adjacent to the headwaters of Trail Creek and has a mean altitude of 8,540 ft.

Tributary yields were calculated for the 1986 and 1987 water years and are shown in table 9. In 1986, the yields from Trail Creek, Warm Springs Creek, and East Fork Big Wood River were about 61,000, 83,000, and 60,000 acre-ft, respectively. In 1987, the yields were about 26,000, 32,000, and 28,000 acre-ft. The average annual yield from the tributaries was estimated from the 1986 and 1987 yields and the percentage of average precipitation during those water years. The average annual yields (reported to 1 significant figure) from Trail Creek, Warm Springs Creek, and East Fork Big Wood River were about 50,000, 60,000, and 50,000 acre-ft, respectively.

SUMMARY

The water resources of the upper Big Wood River basin were studied to provide water planners and managers with tools to evaluate their present water-use policies and to help make future water-management decisions.

Availability of surface and ground water varies seasonally; the greatest quantity is available during spring snowmelt, and the least is available during mid- to late winter. Results of a seepage study conducted during August 1986 showed that the Big Wood River gained water from the ground-water system from Ketchum to below Hailey and lost water to the ground-water system from below Hailey to Glendale Road.

Table 9.--Estimated water yield and precipitation for upper Big Wood River basin tributaries during 1986 and 1987

[Yield in acre-feet per year; precipitation in inches]

| | Trail Creek | Warm Springs Creek | East Fork Big Wood River |
|--|----------------------------|----------------------------|-----------------------------|
| | | <u>1986</u> | |
| Riggs (1969) method (¹) (²) Average | 60,000 64,000 61,000 | 78,000 88,000 83,000 | 56,000 64,000 60,000 |
| Precipitation Percentage of 1940-79 ³ | 38 123 | 35 125 | 36 124 |
| | | <u>1987</u> | |
| Riggs (1969) method (¹) (²) Average | 25,000 26,000 26,000 | 30,000 35,000 32,000 | 27,000 28,000 28,000 |
| Precipitation Percentage of 1940-79 ³ | 18 58 | 15 54 | 16 55 |

¹Correlated using streamflow data from Big Wood River at Hailey. ²Correlated using streamflow data from Big Lost River at Wildhorse. ³Estimated from snow course data and precipitation-altitude relation shown in figure 4.

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Water-quality data showed that nutrient concentrations in surface and ground water were near or below detection levels, which indicated negligible changes in water quality due to upstream urban development and sewage disposal. Fluoride concentrations were elevated in Warm Springs Creek, probably due to inflow of thermal water from Guyer Hot Springs.

Mean annual water yield for the upper Big Wood River basin above Glendale Road, estimated by using a water-budget method, was 410,000 acre-ft and, by using an empirical method, was 460,000 acre-ft. Yield estimated by using the water-budget method is probably more accurate because a large percentage of the water budget is surface water, which is measured rather than estimated. Yield estimated by using the water-budget method was 580,000 acreft during 1986 and 230,000 acre-ft during 1987.

During 1986 and 1987, yields from tributary basins were calculated on the basis of monthly discharge measurements. Yields during 1986 for Trail Creek, Warm Springs Creek, and East Fork Big Wood River were 61,000, 83,000, and 60,000 acre-ft; and during 1987, were 26,000, 32,000, and 28,000 acre-ft for the respective basins. Mean annual yields for Trail Creek, Warm Springs Creek, and East Fork Big Wood River, estimated using 1986 and 1987 yields and the percentage of average precipitation during those water years, were 50,000, 60,000, and 50,000 acre-ft, respectively.

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